

**Research Report 181**

**AN APPROACH  
TO THE  
CONSOLIDATION OF SNOW**

by  
E. D. Feldt  
and  
G. E. H. Ballard

DECEMBER 1965

U.S. ARMY MATERIEL COMMAND  
COLD REGIONS RESEARCH & ENGINEERING LABORATORY  
HANOVER, NEW HAMPSHIRE

DA Task IVO14501B52A02



Distribution of this document is unlimited

PREFACE

This report was prepared by SP4 E. D. Feldt and Dr. G. E. H. Ballard, for the Materials Research Branch, Research Division, USA CRREL.

USA CRREL is an Army Materiel Command laboratory.

DA Task IV014501B52A02

## CONTENTS

	Page
Preface-----	ii
Summary -----	iv
Introduction-----	1
Consolidation theory-----	1
Coefficient of viscosity-----	4
Porosity time relationship-----	6
Unit deformation-----	8
Densification of natural snow cover-----	10
Discussion of parameters-----	11
References-----	12

## ILLUSTRATIONS

## Figure

1. Theoretical compressive viscosity compared with empirical relationship-----	5
2. Theoretical compressive viscosity compared with empirical relationship-----	5
3. Theoretical compressive viscosity compared with the experimentally determined viscosity curve of Ramseier and Pavlak and the empirical relationship of Kojima-----	6
4. Theoretical porosity-time curve-----	7
5. Linearized time-porosity equation compared with data from Ballard and Feldt-----	7
6. Arrhenius-type relationship for an activation energy of 16 kcal/mole compared with data of Ballard and Feldt-----	8
7. Comparison of theoretical unit deformation equation with power function approximation-----	9
8. Theoretical depth-porosity curve compared with data and depth-porosity curve of Kojima-----	11

## TABLES

## Table

I. Summation of regression analysis of porosity-time data according to eq 15-----	7
II. Values of $\eta/\nu$ predicted from Landauer's creep curves---	9
III. Summation of regression analysis on creep data of Ramseier and Pavlak according to equation 18-----	10
IV. Estimated values of the parameter $\nu$ -----	12

## SUMMARY

A consolidation theory is developed for an age-hardened snow under uniaxial stress in the porosity range of 35 to 55% by considering one mechanism, viz., viscous flow of interparticle bonds. For a uniaxial stress  $\sigma$ , the differential equation for porosity  $n$  in terms of time  $t$  is shown to be

$$\frac{1}{(1-n)} \frac{dn}{dt} = -\frac{\nu \sigma n}{\eta(1-an)}$$

where  $a$  and  $\nu$  are structural parameters and  $\eta$  is the coefficient of viscosity of ice. Comparison of this equation and the integrated form with existing data predicts consistent and reasonable values for  $a$ . The predicted values of  $\eta/\nu$  range from  $10^{-2}$  to  $10^2$  times the published values for  $\eta$ , which may indicate that  $\nu$ , and hence the consolidation rate, is greatly affected by the diagenetic history of the snow and the conditions of experimentation.

# AN APPROACH TO THE CONSOLIDATION OF SNOW

by

E. D. Feldt and G. E. H. Ballard

## Introduction

Previous work on the deformation and consolidation of snow has concentrated on the macroscopic rheological behavior and has resulted in the introduction of macroscopic rheological parameters that are snow-type, temperature, and density dependent.

Extensive experimental work has been done to investigate small deformations under low stress conditions. Landauer (1955) and Ramseier and Pavlak (1964) empirically expressed the time-dependent component of the deformation, for a given constant stress, as a simple power law in terms of time. Other researchers (including Ramseier and Pavlak) compared experimental results with the equations of certain rheological models: Bucher (1948) discussed the use of the Maxwell model; and DeQuervain (1946), Yosida et al. (1956), and Ramseier and Pavlak (1964) employed the Maxwell-Voigt model. It was found that the power law and the rheological equations agreed quite well with experimental data; however, these investigators showed that the macroscopic elasticity and viscosity coefficients as well as the experimental parameters in the power law are definite functions of at least temperature and density. Application of these equations to a consolidation process in which there is a significant density change necessitates knowing the functions relating the viscosity coefficient or the parameters in the power law to density and temperature.

The following investigators have advanced simple, yet very different, empirical equations for the macroscopic coefficient of viscosity of snow as a function of density: Landauer (1955), Kojima (1956, 1957, 1958), Bader (1962), and Mellor and Hendrickson (1965).

Examining recent densification theories one finds that Costes (1962) circumvented the problem of an explicit viscosity-density-temperature relationship by developing a rather complicated empirical equation, involving several parameters, for the rate of densification. Bader (1962) used the empirical viscosity-density equation of Kojima, and modified it by arbitrarily introducing a function which satisfied certain boundary conditions. Kojima (1964) showed that Bader's modified equation was approximately of the same form as his original equation for a large density range, and used the original in the analysis of his densification studies in the Antarctic.

In order to gain further insight into the process of snow consolidation and to allow formulation of a theoretical equation describing the density-dependent viscous behavior of snow, it is suggested that the theory should originate on the microscopic level by considering the actual phenomena occurring in the grains and grain bonds.

In this way the properties and behavior of ice are immediately incorporated into the theory. By considering the snow mass to be composed of a finite number of ice particles joined together by a finite number of ice bonds one can introduce parameters related to grain and pore space geometry. Then introducing the macroscopic variable porosity, which is a measure of the mass of ice in an elemental volume, the density dependence is incorporated and a transition to the phenomenological level of interest is achieved.

## Consolidation theory

The theory of consolidation is developed for a laterally confined cylindrical snow mass subjected to an axial load. The lateral stresses which develop are

considered negligible.\* Shear components of this axial force in the grain bonds produce a viscous flow of the ice composing the bonds, and pore space is decreased by the relative movement of the individual snow particles as they slide along intergrain boundaries into a closer configuration. Consolidation is considered to proceed with little change in the shape and size of the snow grains until the closest possible arrangement of the particles is reached. This closest configuration corresponds to a bulk porosity in the range of 36 to 43% (Benson, 1962) and further consolidation can only continue by mutual intrusion of the particles, which results in a marked transition in the rate of consolidation.

It is assumed that the given snow mass is statistically homogeneous, and contains a large number of particles joined together by  $\underline{K}$  bonds. The total volume of the voids,  $V_v$ , in the mass is imagined to be partitioned into  $\underline{K}$  equal volume elements with a common dimension  $\underline{r}$ ; i. e., the elemental volume is represented by

$$\frac{V_v}{\underline{K}} = \underline{a}r^3 \quad (1)$$

where the proportionality constant  $\underline{a}$  may be considered to be a volume shape factor.

Let  $\delta\epsilon_i$  denote the small shear strain which occurs in the bonds when  $V_v$  is decreased by a small amount  $\delta V_v$ . It is assumed that there exist  $\underline{K}$  geometrical parameters  $\lambda_i$  which enable one to approximate the change in the geometrically complicated pore volume as

$$-\delta V_v = \sum_{i=1}^{\underline{K}} \underline{a}r^3 \lambda_i \delta\epsilon_i \quad (2)$$

Then from eq 1 and 2 the unit change in pore volume is

$$\frac{-\delta V_v}{V_v} = \frac{1}{\underline{K}} \sum_{i=1}^{\underline{K}} \lambda_i \delta\epsilon_i \quad (3)$$

It has been found experimentally that the rheological behavior of ice is simple Newtonian at low stresses, i. e., the relationship between shear stress and strain rate is linear. Jellinek and Brill (1956) report this linearity to exist for the stress range of  $3.4 \times 10^5$  to  $2.3 \times 10^6$  dynes/cm<sup>2</sup> and Butkovich and Landauer (1960) found the linear relationship in the stress range of approximately  $10^4$  to  $10^5$  dynes/cm<sup>2</sup>. In this paper the forces of consolidation are considered small enough that the grain bond in the snow mass will exhibit this linear Newtonian behavior.

Let  $\tau_i$  represent the shearing stress acting in a grain bond which produces the strain  $\delta\epsilon_i$  in time  $\delta t$ . Then

$$\delta\epsilon_i = \frac{\tau_i \delta t}{\eta}$$

where  $\eta$  is the coefficient of viscosity for ice. Equation 3 becomes

$$\frac{-\delta V_v}{V_v} = \frac{\delta t}{\eta \underline{K}} \sum_{i=1}^{\underline{K}} \lambda_i \tau_i \quad (4)$$

---

\*Landauer (1957b) showed that lateral stresses which develop under uniaxial load are small.

For the confined snow mass let  $\underline{P}$  be the axial force and define a surface  $S$ , in general perpendicular to  $\underline{P}$ , which intersects only grain bonds in the planes of  $\tau_i$ . Defining the number of bonds intersected by  $S$  to be  $\ell$ ; the area of each bond cross-section to be  $A_i$ , and the angle between the normal to  $A_i$  and the direction of  $\underline{P}$  to be  $\theta_i$ , then

$$\tau_i = \frac{P \cos \theta_i \sin \theta_i}{\sum_{i=1}^{\ell} A_i \cos \theta_i}$$

It is now assumed that the "two dimensional porosity" of the surface  $S$  projected on a plane perpendicular to  $\underline{P}$  is identical to the effective porosity  $n_f$  of a potential failure surface as defined by Ballard and McGaw (1965). If  $\underline{A}$  is the right cross-sectional area of the mass then

$$n_f = \frac{A - \sum_{i=1}^{\ell} A_i \cos \theta_i}{A}$$

and

$$\tau_i = \frac{\sigma \sin \theta_i \cos \theta_i}{1 - n_f} \quad (5)$$

where  $\sigma$  is the axial external stress  $P/A$ . Substituting eq 5 in 4

$$\frac{-\delta V_v}{V_v \delta t} = \frac{\sigma}{\eta(1-n_f)K} \sum_{i=1}^K \lambda_i \sin \theta_i \cos \theta_i.$$

Allowing  $\delta t$  to approach zero

$$\frac{-dV_v}{V_v dt} = \frac{\sigma}{\eta(1-n_f)K} \sum_{i=1}^K \lambda_i \sin \theta_i \cos \theta_i. \quad (6)$$

If  $\underline{V}$  represents the bulk volume of the snow mass with bulk porosity  $n$ , then the insignificant compressibility of ice allows the substitution of  $dV$  for  $dV_v$ ,  $nV$  for  $V_v$ , and  $dn/(1-n)$  for  $dV/V$ . Substituting these relationships in eq 6

$$\frac{(1-n_f)}{n(1-n)} \frac{dn}{dt} = \frac{-\sigma}{\eta K} \sum_{i=1}^K \lambda_i \sin \theta_i \cos \theta_i. \quad (7)$$

The dependence of  $n_f$  and  $\frac{1}{K} \sum_{i=1}^K \lambda_i \sin \theta_i \cos \theta_i$  on  $\underline{n}$  will now be discussed.

According to Ballard and McGaw (1965)  $n_f$  for an age-hardened snow can be represented by  $\underline{an}$  where  $\underline{a}$  is the reciprocal of the limiting porosity  $n_\theta$ . In the summation

$\underline{K}$  increases as consolidation progresses and the quantities  $\lambda_i$  and  $\theta_i$  will in general change as  $\underline{n}$  decreases; however, if the separate distributions of the values of  $\lambda_i$  and  $\theta_i$  are invariant with porosity for  $\underline{K}$  infinite, then, when  $\underline{K}$  is large,

$\frac{1}{\underline{K}} \sum_{i=1}^{\underline{K}} \lambda_i \sin \theta_i \cos \theta_i$  will not change appreciably with porosity.

There is very little evidence in the literature to substantiate the invariance of the distributions of  $\theta_i$  and  $\lambda_i$ . Certainly a porosity-dependent distribution of  $\theta_i$  would require a preferred orientation of the bonds in a naturally consolidating snow mass, a condition which to date has not been observed. The exact physical significance of the geometrical parameters  $\lambda_i$  is not yet clearly visualized; however, if the geometry of pore space remains similar for some range of  $\underline{n}$  as  $\underline{n}$  decreases, then it seems reasonable to assume that the distribution of the values of  $\lambda_i$  is independent of  $\underline{n}$  for this range of  $\underline{n}$ .

Replacing  $\frac{1}{\underline{K}} \sum_{i=1}^{\underline{K}} \lambda_i \sin \theta_i \cos \theta_i$  by a constant  $\nu$  and  $\underline{n}_f$  by  $\underline{an}$  in eq 7 produces

$$\frac{(1-an)}{n(1-n)} \frac{dn}{dt} = \frac{-\nu\sigma}{\eta} \quad (8)$$

which is now restricted to age-hardened snow.

Representing the height of the snow mass by  $\underline{z}$ , then since

$$\frac{1}{(1-n)} \frac{dn}{dt} = \frac{1}{\underline{z}} \frac{dz}{dt} \quad (9)$$

eq 8 may be rewritten as

$$\frac{1}{\underline{z}} \frac{dz}{dt} = \frac{-\nu}{\eta} \left( \frac{n}{1-an} \right) \sigma \quad (10)$$

to give the expression for the rate of consolidation.

#### Coefficient of viscosity

The term  $(\eta/\nu) [(1-an)/n]$ , eq 10, is the macroscopic coefficient of compressive viscosity for the conditions specified in the development: the confining stresses are negligible; the macroscopic stress condition is uniaxial; and the porosity is such that consolidation can occur through particle rearrangement, but is less than  $1/a$ . Denoting this macroscopic coefficient of compressive viscosity as  $\eta_c$ , then

$$\eta_c = \frac{\eta}{\nu} \left( \frac{1-an}{n} \right). \quad (11)$$

The dependence of  $\eta_c$  on temperature, snow-type, and porosity is immediately apparent: temperature dependence is inherent in the temperature-dependent coefficient of viscosity for ice,  $\eta$ , and variation with different snow-types is introduced by the parameters  $\nu$  and  $\underline{a}$ .

Equation 11 was compared with the viscosity data of Mellor and Hendrickson (1965) from confined creep tests at Byrd Station, Antarctica. The porosity range of this data,  $0.35 < n < 0.55$ , is within the range of applicability. Making the substitution

$$X = \frac{1}{n} - a$$

reduces eq 11 to a linearized equation through the origin, viz.,

$$\eta_c = \frac{\eta}{\nu} X. \tag{12}$$

A series of regression analyses of  $\eta_c$  on  $X$  for  $1.70 \leq a \leq 1.80$  in increments of 0.01 showed a maximum correlation coefficient of 0.940 for an  $a$  of 1.78. The reciprocal of this value of  $a$  predicts a limiting porosity  $n_l$  of 0.561, which agrees very well with the values found by Ballard and McGaw. The corresponding value of the slope  $\eta/\nu$  was  $1.23 \times 10^{15}$  poises. Figure 1 shows a comparison of the theoretical equation developed here with the empirical equation of Mellor and Hendrickson for their Byrd Station data.

Haefeli (Bader et al., 1939) showed that the effect of lateral confinement is small for unit deformations up to several percent; hence eq 11 should be applicable to unconfined consolidation for small deformations. From viscosity experiments (unconfined case) Landauer (Bader et al., 1955) found that the compressive viscosity of snow varied as  $\exp(-4.4e')$ , where  $e'$  is the void ratio. From eq 11

$$\eta_c \propto \frac{1-e'(a-1)}{e'} = f(e'). \tag{13}$$

The function  $f(e')$  is well represented by an equation of the form  $\exp(-4.4e')$  for  $a = 1.82$  (or  $n_l = 0.566$ ) in the porosity range of 38 to 53% (Fig. 2).

Equation 11 is also compared in Figure 3 with the experimentally determined viscosity curve of Ramseier and Pavlak (1964) and the empirical relationship of Kojima (1964),  $\eta_c \propto e^{20(1-n)}$ , which was derived from depth-density data. In general  $d\eta_c/dn$  for the theoretical curve is inconsistent with the slopes of these other curves.

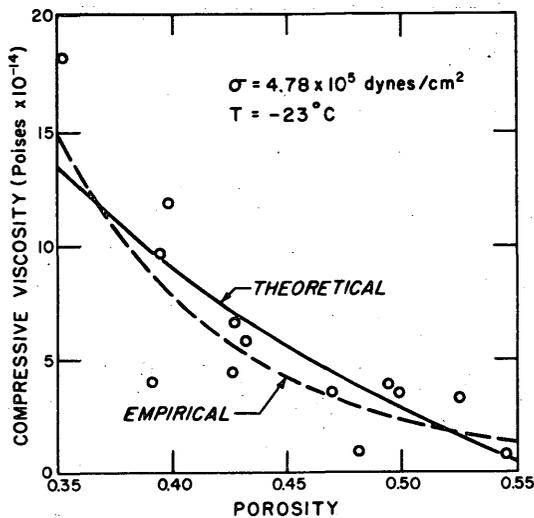


Figure 1. Theoretical compressive viscosity  $\eta_c = (\eta/\nu) [(1-an)/n]$ , for  $a = 1.78$ , compared with empirical relationship  $\eta_c = 2.27 \times 10^{11} [(1-n)/n]^{3.03}$  for Byrd Station data (Mellor and Hendrickson, 1965).

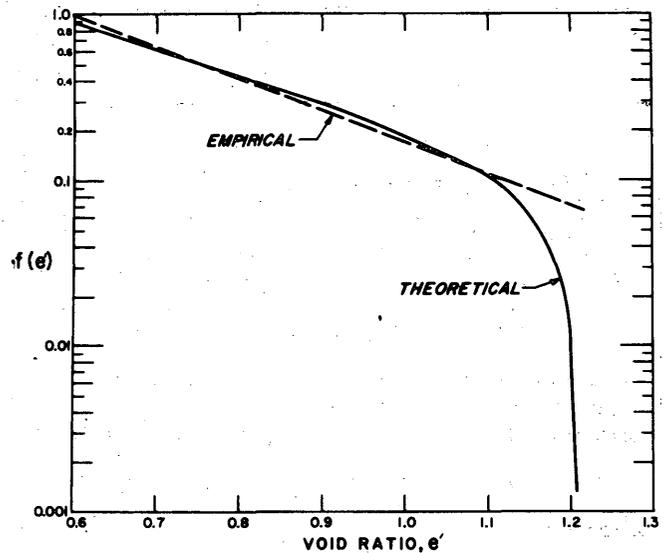


Figure 2. Theoretical compressive viscosity  $\eta_c \propto f(e') = (1-e')(a-1)/e'$ , for  $a = 1.82$ , compared with empirical relationship  $\eta_c \propto \exp(-4.4e')$  of Landauer (Bader et al., 1955).

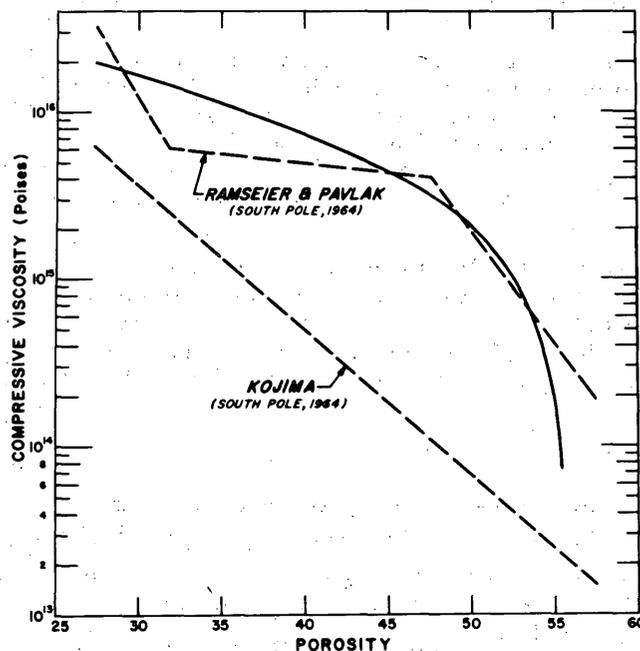


Figure 3. Theoretical compressive viscosity  $\eta_c = (\eta/\nu) [(1-an)/n]$ , for  $a = 1.8$ , compared with the experimentally determined viscosity curve of Ramseier and Pavlak and the empirical relationship of Kojima

$$\eta_c \propto e^{20(1-n)}$$

### Porosity-time relationship

Equation 8 can be integrated for a constant value of  $\sigma$  to give

$$n \left[ \left( \frac{1-n_0}{1-n} \right)^{a-1} \left( \frac{n_0}{n} \right) \right] = \frac{\nu\sigma}{\eta} t \quad (14)$$

where  $n_0$  is the value of  $n$  at  $t = 0$ . Figure 4 is a graph of equation 14 in units of  $\nu\sigma/\eta$  for  $a = 1.8$  and  $n_0 = 0.555$ . To investigate the validity of eq 14, porosity-time data may be analyzed statistically by using the linearized form,

$$Y = MX + B \quad (15)$$

where

$$Y = \frac{1}{t} \ln \left( \frac{1-n}{1-n_0} \right), \quad X = \frac{1}{t} \ln \left( \frac{n_0}{n} \right), \quad B = \frac{-\nu\sigma}{\eta(a-1)}, \quad M = \frac{1}{a-1}$$

Data from Ballard and Feldt (1965) were analyzed according to eq 15 by regressing  $Y$  on  $X$ . The results are summarized in Table I and a typical example is shown in Figure 5. Ballard and Feldt reported data for a large series of tests, but only the data for the lower axial loads appeared to be explained by eq 14.

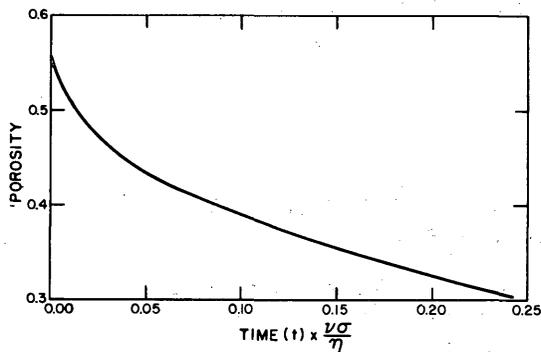


Figure 4. Theoretical porosity-time curve

$$\ln \left[ \left( \frac{1-n}{1-n_0} \right)^{a-1} \left( \frac{n_0}{n} \right) \right] = \frac{v\sigma}{\eta} t \text{ for } a = 1.80 \text{ and } n_0 = 0.555.$$

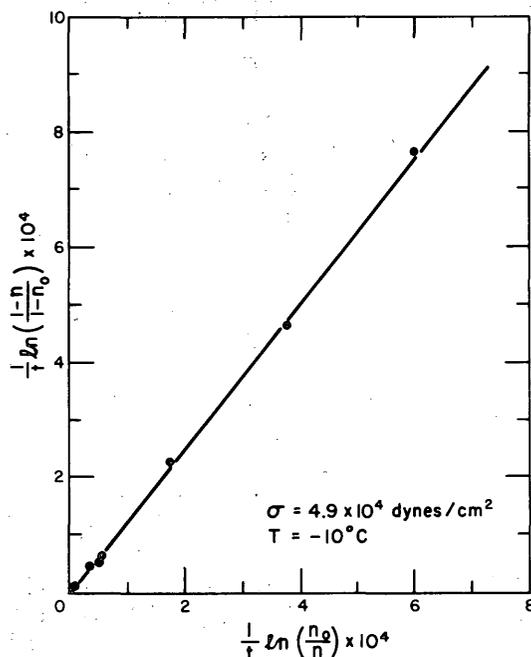


Figure 5. Linearized time-porosity equation compared with data from Ballard and Feldt (1965).

Table I. Summation of regression analysis of porosity-time data according to eq 15.

T (°C)	σ (dynes/cm <sup>2</sup> )10 <sup>-4</sup>	M	B (sec <sup>-1</sup> )10 <sup>8</sup>	Correlation coefficient	1/a = n <sub>l</sub>	η/v (poises)10 <sup>-12</sup>
-3.3	0.98	1.35	1.62	0.9989	0.575	0.82
	1.96	1.26	3.79	0.9997	0.557	0.65
-6.7	0.98	1.31	0.82	0.9986	0.567	1.56
	1.96	1.27	2.10	0.9990	0.559	1.19
	4.90	1.23	6.47	0.9998	0.551	0.93
-10	0.98	1.50	2.89	0.9994	0.601	0.51
	1.96	1.23	0.13	0.9993	0.551	18.1
	4.90	1.24	0.78	0.9999	0.554	7.79

The consistently high correlation coefficients and the narrow range of values of the limiting porosity, with a mean of 0.564, support the validity of eq 14. Values of η/v are plotted against the reciprocal of absolute temperature in Figure 6. An Arrhenius-type relationship for an activation energy of 16 kcal/mole appears to fit the data very well. This agrees with Jelinek and Brill (1956) who found that the variation of the coefficient of viscosity of polycrystalline ice with temperature predicted an activation energy for creep of 16.1 kcal/mole. It therefore appears that v is indeed constant for the particular type of snow used by Ballard and Feldt.

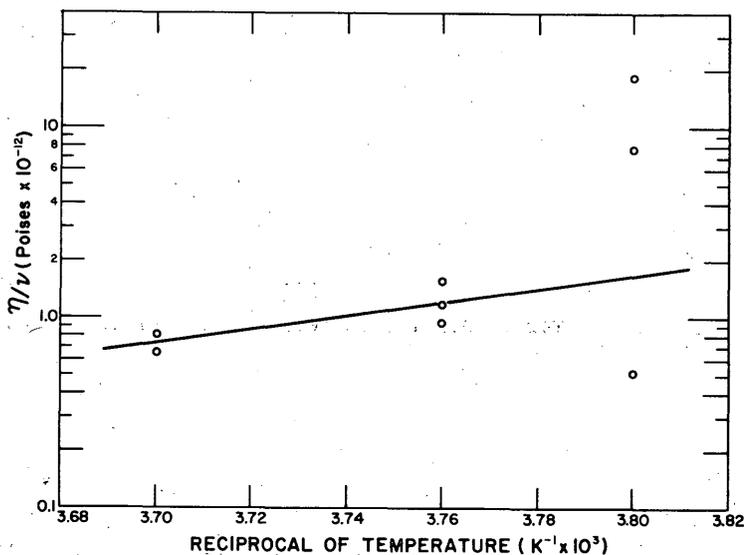


Figure 6. Arrhenius-type relationship for an activation energy of 16 kcal/mole compared with data of Ballard and Feldt (1965).

#### Unit deformation

Representing the height of the snow mass at time  $t = 0$  and  $t$  by  $z_0$  and  $z_0 - \Delta z$  respectively and making the substitution

$$\frac{1-n_0}{1-n} = \frac{z}{z_0}$$

and

$$\frac{n_0}{n} = \frac{n_0(1 - \Delta z/z_0)}{n_0 - (\Delta z/z_0)}$$

then eq 14 may be written in terms of the unit deformation  $\Delta z/z_0$  as

$$\ln \left[ \frac{n_0(1 - \Delta z/z_0)^a}{n_0 - (\Delta z/z_0)} \right] = \frac{\nu \sigma}{\eta} t. \quad (16)$$

Equation 16 was checked against the creep curves in Landauer (1955). Choosing  $a = 1.80$  (a value which is consistent with previous predictions) and using  $n_0 = 0.542$  (Landauer's initial porosity), a logarithmic plot (Fig. 7) was made of the left side of eq 16, designated as  $F(\Delta z/z_0)$  against  $\Delta z/z_0$ . Landauer's creep curves (1955, Fig. 6) can be represented by an equation of the form  $t = b(\Delta z/z_0)^{1.25}$  where  $b$  varies with  $\sigma$ . This empirical relationship is a very good approximation to eq 16 in the range  $0.001 < \Delta z/z_0 < 0.1$ , as can be seen in Figure 7 where the straight line is the power function  $0.179(\Delta z/z_0)^{1.25}$ . Replacing  $F(\Delta z/z_0)$  by this approximation one has

$$t = 0.179 \frac{\eta}{\nu \sigma} \left( \frac{\Delta z}{z_0} \right)^{1.25} \quad (17)$$

which requires  $0.179 \eta/\nu \sigma = b$ . Values of  $b$  from Landauer's curves and the calculated values of  $\eta/\nu$  are shown in Table II.

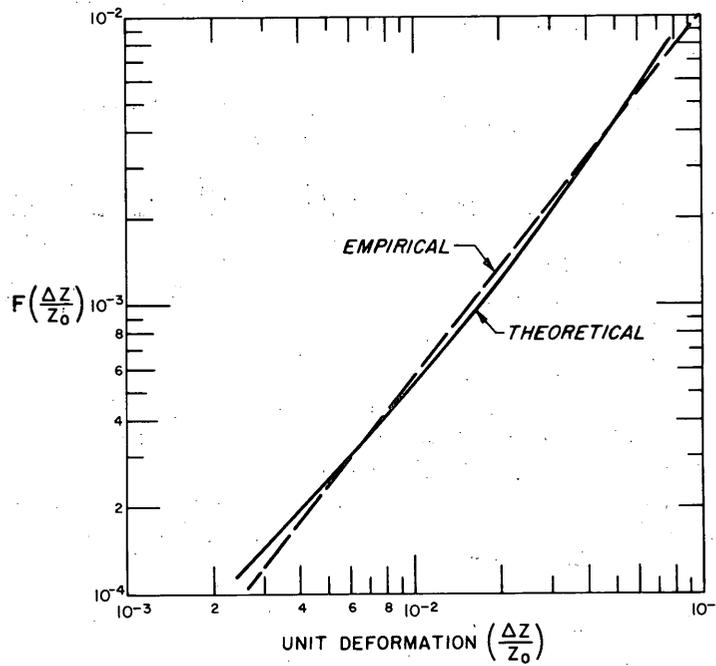


Figure 7. Comparison of theoretical unit deformation

$$F(\Delta z/z_0) = \ln \left[ \frac{n_0(1-\Delta z/z_0)^a}{n_0 - \Delta z/z_0} \right] =$$

$$\frac{\nu \sigma}{\eta} t, \text{ for } a = 1.80 \text{ and } n_0 = 0.542, \text{ with power}$$

$$\text{function approximation } F(\Delta z/z_0) = 0.179 (\Delta z/z_0)^{1.25}.$$

Table II. Values of  $\eta/\nu$  predicted from Landauer's creep curves.

$\sigma$ (dynes/cm <sup>2</sup> )	b (secs)	$\eta/\nu$ (poises)
$8.0 \times 10^4$	$2.73 \times 10^7$	$1.25 \times 10^{13}$
$4.31 \times 10^4$	$7.05 \times 10^7$	$1.73 \times 10^{13}$
$2.41 \times 10^4$	$11.5 \times 10^7$	$1.58 \times 10^{13}$

Equation 16 was also compared with the data from Ramseier and Pavlak (1964, Fig. 1) by using the linearized form of the equation

$$Y = aX + d \tag{18}$$

where

$$Y = \frac{1}{t} \ln \left( 1 - \frac{\Delta z}{n_0 z_0} \right)$$

$$X = \frac{1}{t} \ln \left( 1 - \frac{\Delta z}{z_0} \right)$$

$$d = \frac{-\nu \sigma}{\eta}.$$

A regression of Y on X produced the results shown in Table III.

Although widely separated areas are represented, the values of  $n_t$  are considerably lower than previously predicted.

Table III. Summation of regression analysis on creep data of Ramseier and Pavlak according to equation 18.

Location	T (°C)	$\sigma$ (dynes/cm <sup>2</sup> )10 <sup>-5</sup>	1/a= $n_t$	d (sec <sup>-1</sup> )10 <sup>11</sup>	Correlation coefficient	$\eta/\nu$ (poises)10 <sup>-16</sup>
South Pole	-48.0	0.847	0.49	-423	1.0000	200
Camp Century	-22.5	1.78	0.50	-1.19	.9999	1.5
Byrd Station	-25.0	2.10	0.50	-1.05	1.0000	2.0

#### Densification of natural snow cover

Finally, application of the result of this theory to densification of a natural snow cover should indicate whether the imposed conditions used in the development of the theory are applicable to in situ consolidation.

Assuming that the snow is accumulating at a constant rate A, then a snow layer which fell at time  $t = 0$  will be subject to a vertical stress  $\sigma = At$  at time  $t$ , and for the given snow layer eq 8 becomes

$$\frac{(1-an)}{n(1-n)} \frac{dn}{dt} = \frac{-\nu At}{\eta} \quad (19)$$

Integrating gives

$$t = \sqrt{\frac{2\eta}{A\nu}} \sqrt{\ln \left[ \left( \frac{1-n_0}{1-n} \right)^{a-1} \frac{n_0}{n} \right]} \quad (20)$$

where  $n_0$  is now the surface snow porosity.

Denoting the depth as  $h$ , the density of the snow as  $\gamma$ , and the density of ice as  $\gamma_i$ , then from Sorge's Law (Bader, 1954)

$$\frac{A}{\gamma^2} \frac{d\gamma}{dh} = \frac{1}{\gamma} \frac{d\gamma}{dt}$$

or in terms of  $n$

$$\frac{A}{\gamma_i(1-n)^2} \frac{dn}{dh} = \frac{1}{(1-n)} \frac{dn}{dt} \quad (21)$$

Substituting from eq 19 and 20 in 21 and integrating from the surface to depth  $h$  produces the depth-porosity curve for a constant temperature,

$$h = \frac{-1}{\gamma_i} \sqrt{\frac{A\eta}{2\nu}} \int_{n_0}^n \frac{(1-an) dn}{n(1-n)^2 \sqrt{\ln \left[ \left[ \frac{(1-n_0)}{(1-n)} \right]^{a-1} \left( \frac{n_0}{n} \right) \right]}} \quad (22)$$

A depth-porosity curve from Kojima (1964, Fig. 14, BH58) was selected as representative for snow with a low surface porosity for comparison with eq 22. Estimating  $n_0 = 0.525$  and choosing  $a = 1.80$ , the integral in eq 22 was evaluated numerically by changing the lower limit to 0.5249 to avoid the point  $n=n_0$  where the integrand becomes infinite. Then a choice of

$$\frac{1}{\gamma_i} \sqrt{\frac{\eta A}{2\nu}} = 430$$

produced the depth-porosity curve shown in Figure 8. The curve expresses the data quite well down to a depth of about 450 cm, where the porosity is just within the range indicated by Benson (1962) for close packing. A value of  $\eta/\nu = 4.25 \times 10^{13}$  poises was calculated from Kojima's estimated accumulation rate.

#### Discussion of parameters

Two parameters,  $a$  and  $\nu$ , were introduced in the development of the consolidation theory. The reciprocal of the first parameter,  $1/a$ , was assumed to be equivalent to the limiting porosity  $n_0$  as defined by Ballard and McGaw (1965). Comparison of the theory with consolidation data from several different sources has predicted values of  $1/a$  that agree very closely with the values of  $n_0$  predicted by Ballard and McGaw from strength data.

The parameter  $\nu$  defined by

$$\nu = \frac{1}{K} \sum_{i=1}^K \lambda_i \sin \theta_i \cos \theta_i \quad (23)$$

is not directly related to any quantity that has been previously defined in snow mechanics. It was introduced to relate the combined individual infinitesimal displacements in the structure of the snow mass to the total change in pore volume. Its value cannot be predicted precisely from consolidation data, but rather the quotient  $\eta/\nu$ . A knowledge of the value of  $\eta$  for a particular temperature allows an estimation of  $\nu$ . Jellinek and Brill found that  $\eta$  for polycrystalline ice could be represented by

$$\eta = 7.5 e^{16.1/RT} \quad (\text{poises}) \quad (24)$$

where  $R$  is the ideal gas constant in kcal/mole - deg Kelvin and  $T$  is the absolute temperature. Using eq 24 and the values of  $\eta/\nu$  predicted in this paper, the values of  $\nu$  shown in Table IV were calculated. It is seen that the order of magnitude of  $\nu$  ranges from  $10^{-2}$  to  $10^2$ . This inconsistency in the values of  $\nu$  as predicted from the data of different investigators may indicate that the value of  $\nu$  is greatly affected by the diagenetic history of the snow and the specific conditions of the experiment. The magnitude of  $\nu$  (eq 23) is equal to the mean value of the term  $\lambda_i \sin \theta_i \cos \theta_i$ . From eq 2 the magnitude of  $\lambda_i$  should be of the order of 1; and if  $\theta_i$  can assume all possible values between 0 and  $\pi/2$ , then the average value of  $\sin \theta_i \cos \theta_i$  is  $1/\pi$ . Therefore, the magnitude of  $\nu$  should be of the order of 1. Only the data of Mellor and Hendrickson predict a value of  $\nu$  of this magnitude (Table IV). It may be noted, however, that their experiment was the only one which actually satisfied the conditions of the theory; viz., the samples were fully age-hardened snow and were confined during the tests.

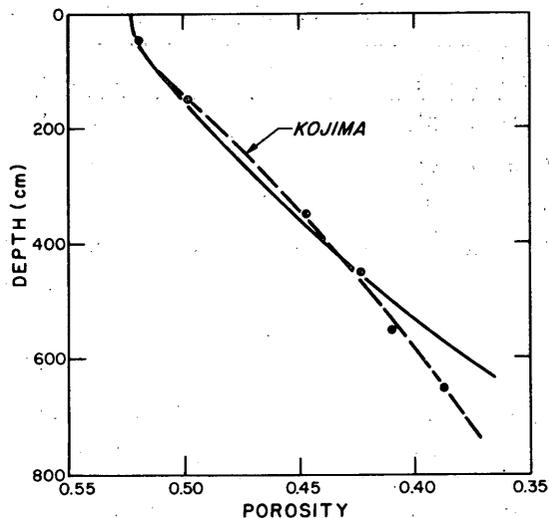


Figure 8. Theoretical depth-porosity curve compared with data and depth-porosity curve of Kojima (1964).

Table IV. Estimated values of the parameter  $\nu$ .

$\eta/\nu$ (poises)	T (°C)	$\eta$ (poises)	$\nu$	References
$8.19 \times 10^{11}$	-3	$7.2 \times 10^{13}$	88	Ballard and Feldt (1965)
$6.51 \times 10^{11}$	-3	$7.2 \times 10^{13}$	111	
$1.56 \times 10^{12}$	-7	$1.1 \times 10^{14}$	71	
$1.19 \times 10^{12}$	-7	$1.1 \times 10^{14}$	93	
$9.31 \times 10^{11}$	-7	$1.1 \times 10^{14}$	118	
$5.1 \times 10^{11}$	-10	$1.6 \times 10^{14}$	314	
$1.81 \times 10^{13}$	-10	$1.6 \times 10^{14}$	8.85	
$7.79 \times 10^{12}$	-10	$1.6 \times 10^{14}$	20.5	
$4.25 \times 10^{13}$	-26	$1.25 \times 10^{15}$	29.4	Kojima (1964)
$1.25 \times 10^{13}$	-10	$1.6 \times 10^{14}$	12.8	Landauer (Bader <i>et al.</i> , 1955)
$1.73 \times 10^{13}$	-10		9.3	Bader <i>et al.</i>
$1.58 \times 10^{13}$	-10		10.1	
$1.23 \times 10^{15}$	-23	$8.5 \times 10^{14}$	0.69	Mellor and Hendrickson (1965)
$2 \times 10^{16}$	-23	$8.5 \times 10^{14}$	0.0424	Ramseier and Pavlak (1964)
$1.5 \times 10^{16}$	-25	$1.2 \times 10^{15}$	0.08	
$2 \times 10^{18}$	-48	$3.5 \times 10^{16}$	0.0175	

## REFERENCES

- Bader, H. (1954) Sorge's Law of densification of snow on high polar glaciers, Journal of Glaciology, 2, 319-323.
- (1962) Theory of densification of dry snow on high polar glaciers, II, U. S. Army Cold Regions Research and Engineering Laboratory (USA CRREL) Research Report 108.
- ; Haefeli, R.; Bucher, E.; Neher, J.; Eckel, O.; and Thams, Chr. (1939) Der Schnee und seine Metamorphose (Snow and its metamorphism), Beiträge zur Geologie der Schweiz, Geotechnische Serie, Hydrologie, Lieferung 3. U. S. Army Snow, Ice and Permafrost Research Establishment (USA SIPRE) Translation 14, 1954.
- ; Waterhouse, R. W.; Landauer, J. K.; Hansen, B. L.; Bender, J. A.; and Butkovich, T. R. (1955) Excavations and installations at SIPRE test site, Site 2, Greenland, USA SIPRE Report 20, p. 24-26.
- Ballard, G. E. H.; Feldt, E. D. and Toth, S. R. (1965) Direct shear data on snow, USA CRREL Special Report 92.
- , and McGaw, R. W. (1965) A theory of snow failure; USA CRREL Research Report 137.
- Benson, C. S. (1962) Stratigraphic studies in the snow and firn of the Greenland Ice Sheet, USA SIPRE Research Report 70.

## REFERENCES (Cont'd)

- Bucher, E. (1948) Beiträge zu den theoretischen Grundlagen des Lawinenverbaus (Contribution to the theoretical foundations of avalanche defense construction). Beiträge zur Geologie der Schweiz, Geotechnische Serie, Hydrologie, Lieferung 6. USA SIPRE Translation 18, 1956.
- Butkovich, T. R. and Landauer, J. K. (1960) Creep of ice at low stresses, USA SIPRE Research Report 72.
- Costes, N. C. (1963) "Confined compression tests in dry snow," in Ice and snow, properties, processes, and applications (W. D. Kingery, editor). Cambridge, Mass.: M.I.T. Press.
- DeQuervain, M. (1946) Kristallplastische Vorgänge im Schneeaggregat II (Crystalloplastic phenomena in the snow aggregate), Mitteilungen aus dem eidg. Institut für Schnee- und Lawinenforschung.
- Jellinek, H. H. G. and Brill, R. (1956) Viscoelastic properties of ice, Journal of Applied Physics, vol. 27, no. 10, p. 1198-1209.
- Kojima, K. (1956) Sekisetsuso no nensei asshuku, IV. (Viscous compression of natural snow layers, IV), Low Temperature Science, Series A, vol. 15.
- \_\_\_\_\_ (1957) Sekisetsuso no nensei asshuku, IV (Viscous compression of natural snow layers, IV), Low Temperature Science, Series A, vol. 16, p. 167-196 (text in Japanese).
- \_\_\_\_\_ (1958) Sekisetsuso no nensei asshuku, IV (Viscous compression of natural snow layers, IV), Low Temperature Science, Series A, vol. 17, p. 53-64 (text in Japanese).
- \_\_\_\_\_ (1964) Densification of snow in Antarctica, Antarctic Research Series, vol. 2, p. 157-218.
- Landauer, J. K. (1955) Stress-strain relations in snow under uniaxial compression, USA SIPRE Research Report 12, 9p.
- \_\_\_\_\_ (1957a) Creep of snow under combined stress, USA SIPRE Research Report 41.
- \_\_\_\_\_ (1957b) On the deformation of excavations in the Greenland névé, USA SIPRE Research Report 30.
- Mellor, M. and Hendrickson, G. (1965) Confined creep tests on polar snow, USA CRREL Research Report 138.
- Ramseier, R. O. and Pavlak, T. L. (1964) Unconfined creep tests of polar snow, Journal of Glaciology, vol. 5, no. 39.
- Yosida, Z. et al., (1956) Physical studies on deposited snow II. Mechanical properties (1), Contribution no 307, Institute of Low Temperature Science, Hokkaido University, Japan, no. 9, p. 1-81.

DOCUMENT CONTROL DATA - R&D

(Security classification of title, body of abstract and indexing annotation must be entered when the overall report is classified)

1. ORIGINATING ACTIVITY (Corporate author) U. S. Army Cold Regions Research and Engineering Laboratory, Hanover, N. H.		2a. REPORT SECURITY CLASSIFICATION Unclassified	
		2b. GROUP	
3. REPORT TITLE AN APPROACH TO THE CONSOLIDATION OF SNOW			
4. DESCRIPTIVE NOTES (Type of report and inclusive dates) Research Report			
5. AUTHOR(S) (Last name, first name, initial) Feldt, E. D. and Ballard, G. E. H.			
6. REPORT DATE Dec 1965		7a. TOTAL NO. OF PAGES 16	7b. NO. OF REFS 22
8a. CONTRACT OR GRANT NO.  b. PROJECT NO.  c. DA Task IV014501B52A02  d.		9a. ORIGINATOR'S REPORT NUMBER(S) Research Report 181	
		9b. OTHER REPORT NO(S) (Any other numbers that may be assigned this report)	
10. AVAILABILITY/LIMITATION NOTICES Distribution of this document is unlimited			
11. SUPPLEMENTARY NOTES		12. SPONSORING MILITARY ACTIVITY U. S. Army Cold Regions Research and Engineering Laboratory	
13. ABSTRACT A consolidation theory is developed for an age-hardened snow under uniaxial stress in the porosity range of 35 to 55% by considering one mechanism, viz., viscous flow of interparticle bonds. For a uniaxial stress $\sigma$ , the differential equation for porosity $n$ in terms of time $t$ is shown to be $1/(1-n) dn/dt = \nu\sigma n/\eta(1-an)$ where $a$ and $\nu$ are structural parameters and $\eta$ is the coefficient of viscosity of ice. Comparison of this equation and the integrated form with existing data predicts consistent and reasonable values for $a$ . The predicted values of $\eta/\nu$ range from $10^{-2}$ to $10^2$ times the published values for $\eta$ , which may indicate that $\nu$ , and hence the consolidation rate, is greatly affected by the diagenetic history of the snow and the conditions of experimentation.			

14. KEY WORDS	LINK A		LINK B		LINK C	
	ROLE	WT	ROLE	WT	ROLE	WT
Snow--Consolidation Snow cover--Subsidence Snow cover--Theoretical Analysis						

**INSTRUCTIONS**

**1. ORIGINATING ACTIVITY:** Enter the name and address of the contractor, subcontractor, grantee, Department of Defense activity or other organization (*corporate author*) issuing the report.

**2a. REPORT SECURITY CLASSIFICATION:** Enter the overall security classification of the report. Indicate whether "Restricted Data" is included. Marking is to be in accordance with appropriate security regulations.

**2b. GROUP:** Automatic downgrading is specified in DoD Directive 5200.10 and Armed Forces Industrial Manual. Enter the group number. Also, when applicable, show that optional markings have been used for Group 3 and Group 4 as authorized.

**3. REPORT TITLE:** Enter the complete report title in all capital letters. Titles in all cases should be unclassified. If a meaningful title cannot be selected without classification, show title classification in all capitals in parenthesis immediately following the title.

**4. DESCRIPTIVE NOTES:** If appropriate, enter the type of report, e.g., interim, progress, summary, annual, or final. Give the inclusive dates when a specific reporting period is covered.

**5. AUTHOR(S):** Enter the name(s) of author(s) as shown on or in the report. Enter last name, first name, middle initial. If military, show rank and branch of service. The name of the principal author is an absolute minimum requirement.

**6. REPORT DATE:** Enter the date of the report as day, month, year, or month, year. If more than one date appears on the report, use date of publication.

**7a. TOTAL NUMBER OF PAGES:** The total page count should follow normal pagination procedures, i.e., enter the number of pages containing information.

**7b. NUMBER OF REFERENCES:** Enter the total number of references cited in the report.

**8a. CONTRACT OR GRANT NUMBER:** If appropriate, enter the applicable number of the contract or grant under which the report was written.

**8b, 8c, & 8d. PROJECT NUMBER:** Enter the appropriate military department identification, such as project number, subproject number, system numbers, task number, etc.

**9a. ORIGINATOR'S REPORT NUMBER(S):** Enter the official report number by which the document will be identified and controlled by the originating activity. This number must be unique to this report.

**9b. OTHER REPORT NUMBER(S):** If the report has been assigned any other report numbers (*either by the originator or by the sponsor*), also enter this number(s).

**10. AVAILABILITY/LIMITATION NOTICES:** Enter any limitations on further dissemination of the report, other than those imposed by security classification, using standard statements such as:

- (1) "Qualified requesters may obtain copies of this report from DDC."
- (2) "Foreign announcement and dissemination of this report by DDC is not authorized."
- (3) "U. S. Government agencies may obtain copies of this report directly from DDC. Other qualified DDC users shall request through \_\_\_\_\_."
- (4) "U. S. military agencies may obtain copies of this report directly from DDC. Other qualified users shall request through \_\_\_\_\_."
- (5) "All distribution of this report is controlled. Qualified DDC users shall request through \_\_\_\_\_."

If the report has been furnished to the Office of Technical Services, Department of Commerce, for sale to the public, indicate this fact and enter the price, if known.

**11. SUPPLEMENTARY NOTES:** Use for additional explanatory notes.

**12. SPONSORING MILITARY ACTIVITY:** Enter the name of the departmental project office or laboratory sponsoring (*paying for*) the research and development. Include address.

**13. ABSTRACT:** Enter an abstract giving a brief and factual summary of the document indicative of the report, even though it may also appear elsewhere in the body of the technical report. If additional space is required, a continuation sheet shall be attached.

It is highly desirable that the abstract of classified reports be unclassified. Each paragraph of the abstract shall end with an indication of the military security classification of the information in the paragraph, represented as (TS), (S), (C), or (U).

There is no limitation on the length of the abstract. However, the suggested length is from 150 to 225 words.

**14. KEY WORDS:** Key words are technically meaningful terms or short phrases that characterize a report and may be used as index entries for cataloging the report. Key words must be selected so that no security classification is required. Identifiers, such as equipment model designation, trade name, military project code name, geographic location, may be used as key words but will be followed by an indication of technical context. The assignment of links, rules, and weights is optional.