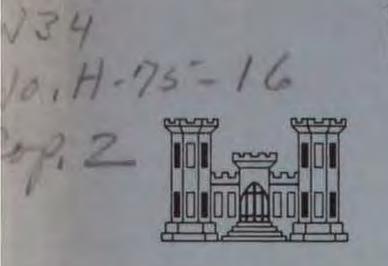
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TECHNICAL REPORT H-75-16

SHORE EFFECT MODEL, ATLANTIC GENERATING STATION

Hydraulic Model Investigation

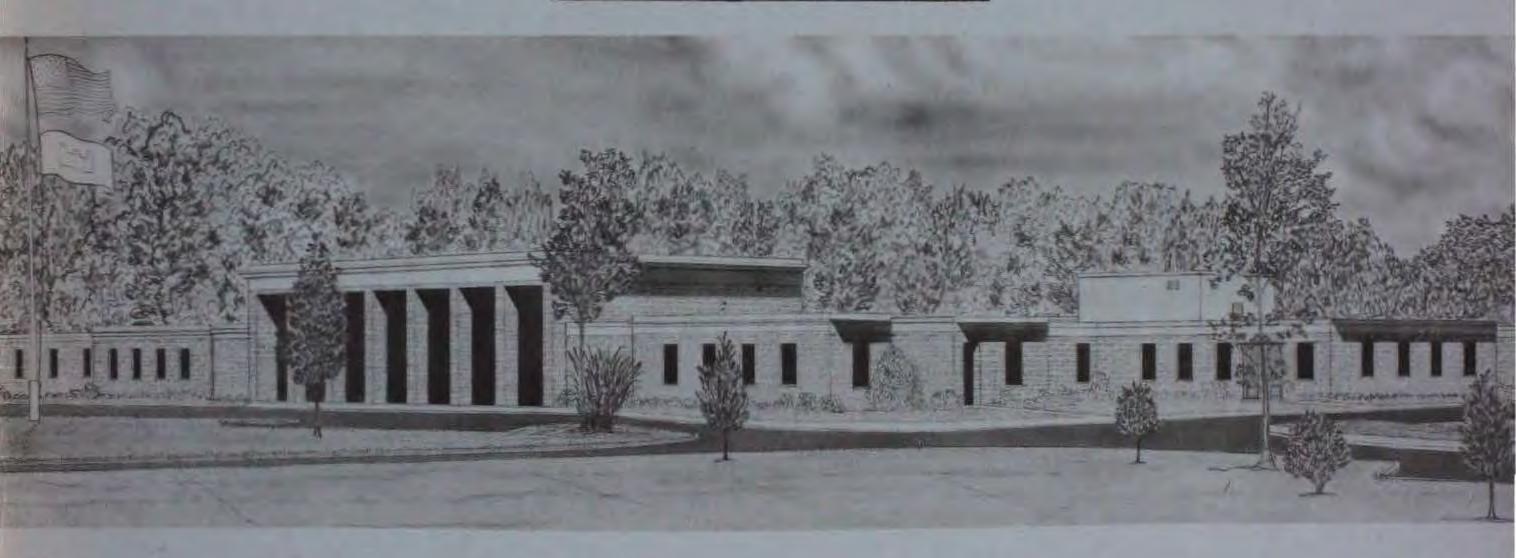
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November 1975 Final Report

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Prepared for Public Service Electric and Gas Company Newark, New Jersey 07101

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A distorted-scale hydraulic model investigation was performed to determine the potential effect, if any, of a proposed offshore nuclear power plant on shoreline evolution. Model measurements of current patterns with and without the breakwater were directly compared and measurements of breaking wave characteristics (height, depth, and angle to shoreline) with and without the breakwater were used to calculate and compare longshore transport rates in the potentially affected areas. It was concluded that the proposed construction would have a negligible effect on future shoreline evolution.

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PREFACE

The model investigation reported herein was requested by Public Service Electric and Gas Company (PSE&G) in a letter to the U. S. Army Engineer Waterways Experiment Station (WES) dated 29 June 1972. The investigation was authorized by the Office, Chief of Engineers (OCE), U. S. Army, in the 1st indorsement dated 20 July 1972 to WES letter dated 11 July 1972 and extended in the 1st indorsement dated 5 June 1974 to WES letter dated 16 May 1974. The tests were conducted during the period October 1973 to December 1974 by personnel of the Hydraulics Laboratory (HL), WES, under the general direction of Mr. H. B. Simmons, Chief of HL, and Dr. R. W. Whalin, Chief of the Wave Dynamics Division. The research on the morphology of the inlets was conducted by 1LT J. H. Barwis, and the model tests were conducted by Mr. R. D. Carver, Research Hydraulic Engineer, with the assistance of Messrs. C. Lewis and W. G. Dubose, Engineering Technicians, under the immediate supervision of Mr. D. D. Davidson, Chief of the Wave Research Branch. This report was prepared by Messrs. Carver and Davidson, and Dr. Whalin. 1LT Barwis prepared Appendix A.

Directors of WES during this investigation and the preparation and publication of this report were BG E. D. Peixotto, CE, and COL G. H. Hilt, CE. Technical Director was Mr. F. R. Brown.

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CONVERSION' FACTORS, U. S. CUSTOMARY TO METRIC (SI) UNITS OF MEASUREMENT

U. S. customary units of measurement used in this report can be converted to metric (SI) units as follows:

| Multiply | By | To Obtain |
|------------------------------|------------|---------------------------|
| inches | 2.54 | centimetres |
| feet | 0.3048 | metres |
| miles (U. S. statute) | 1.609344 | kilometres |
| square feet | 0.09290304 | square metres |
| square miles (U. S. statute) | 2.589988 | square kilometres |
| cubic yards | 0.7645549 | cubic metres |
| pounds (mass) per cubic foot | 16.01846 | kilograms per cubic metre |
| foot-pounds (force) | 1.355818 | joules |
| feet per second | 0.3048 | metres per second |
| miles per hour | 1.609344 | kilometres per hour |
| degrees (angle) | 0.01745329 | radians |
| | | |

SHORE EFFECT MODEL, ATLANTIC GENERATING STATION Hydraulic Model Investigation

PART I: INTRODUCTION

The Problem

1. A nuclear power plant is proposed to be located approximately 3 miles* seaward of Little Egg Inlet, New Jersey, at longitude 74°15'20" W and latitude 39°28'20" N (New Jersey coordinate of N 232, 959 ft and E 2, 116, 060 ft). A concern is the effect, if any, of this offshore structure on shoreline evolution in the vicinity of the inlet. Will the breakwater used to protect the power plant alter wave conditions (breaking locations, heights, and angles) near the shoreline, thereby producing a change in the longshore transport rates and causing erosion or accretion of the shoreline? This is a difficult question to answer. It is impossible to answer by purely analytical techniques due to the complicated dynamics of wave, tide, and sediment interaction. Some factors which must be considered are: the existence of caustics in the local wave refraction patterns, the diffraction of wave energy around the breakwater and along the wave crests, and the nonlinear interaction of wave-induced currents and tidal flows.

Geomorphological Evaluation of the Prototype

2. The Beach Haven-Little Egg Inlet area has, since the existence of records, undergone dynamic changes as a result of tidal and wave interaction with the regional longshore transport. It is realized that any type of study to show that the construction of an offshore structure would cause morphology changes over and above those presently being

^{*} A table of factors for converting U. S. customary units of measurement to metric (SI) units is presented on page 4.

experienced is very difficult. To emphasize the historical configurational changes, a brief morphology study of the inlets was conducted and is presented in Appendix A as background information.

Feasibility Investigation

- 3. Since all the dynamic problems involved could not be determined analytically, it was felt that the only realistic way to evaluate the potential effects of the proposed power plant was to conduct a distorted-scale hydraulic model investigation. Even a distorted hydraulic model of these phenomena is a state-of-the-art investigation and requires special feasibility considerations. Whalin and Hudson address the feasibility of this model in detail, whereas the next few paragraphs of this report contain only the highlights of the factors affecting the model feasibility. Factors considered in determining the feasibility of such an investigation were:
 - a. Wave height attenuation due to viscous friction.
 - b. Wave refraction.
 - c. Wave diffraction.
 - d. Wave reflection.
 - e. Wave breaking location and angle to shoreline.
 - f. Simulation of tidal flow velocities.
- 4. Due to the large area of relatively shallow water encompassed by the model, the viscous dissipation of energy at the bottom became an important consideration. If the model had been constructed to an undistorted scale, this excessive energy dissipation would probably have prevented accurate reproduction of wave phenomena. The selection of a horizontal-scale ratio which was numerically larger than the vertical-scale ratio and the scaling of model wave heights and periods by the vertical-scale ratio resulted in a reduction in the energy dissipation due to the relatively shorter propagation distance of the test waves.
- 5. In a distorted-scale model investigation it is impossible for both wave refraction and diffraction to be properly scaled

simultaneously. Refraction is a function of the relative depth (d/L)* only; therefore, if the wavelength is scaled according to the vertical scale, refraction patterns will be modeled correctly. Diffraction is a function of the ratio of a horizontal distance to the wavelength (X/L); consequently, if the wavelength is scaled according to the horizontal scale, diffraction will be properly modeled. In the investigation under consideration, diffraction around the breakwater is an important effect in the immediate area of the power plant; however, the closer to shore the wave progresses, the less important diffraction effects are and the more important refraction becomes. Since attention was focused on current patterns and wave characteristics near the shoreline, it was most advantageous to model refraction correctly (test waves were modeled on the vertical scale). Even though this induced some errors in the diffraction patterns around the breakwater, construction of diffraction diagrams revealed these errors to be minimal near the shoreline.

- 6. Two types of wave reflection merited consideration: cumulative reflection from bottom slopes as waves propagated from the area of the power plant to the shoreline, and reflection from the sloping breakwater. Calculations using the theory of M. Rosseau² revealed that excess bottom slope reflections for horizontal-scale ratios up to five times numerically larger than the vertical-scale ratio were only one to two percent of the incident wave height. The magnitude of bottom-slope reflections in this model (distortion 4:1) can be considered negligible. However, reflections from the relatively steep breakwater slopes (1:2) were considered a problem. It was decided that two-dimensional (2-D) flume tests should be conducted to determine optimum construction materials and techniques for the three-dimensional (3-D) model breakwater.
- 7. Scaling test waves by the vertical-scale ratio resulted in proper similitude of relative wave heights (H/d) and relative wave steepness (H/L); therefore, proper breaking depth was assured. Similitude of

^{*} For convenience, symbols and unusual abbreviations are listed and defined in the Notation (Appendix C).

refraction and consequently similitude of angle of wave crests relative to the shoreline also were assured by this scaling technique.

8. An important part of the model study was the interaction of tidal and wave-induced currents. Based on the study of requirements to reproduce the entire tidal cycle (reproduction of a large tidal prism, artificial roughness, extensive prototype surveys, etc.), it was decided the model could use steady-state ebb and flood flows produced by a manifold system.

Object and Approach

9. The objective of the model study was to determine qualitatively the effect, if any, of the proposed offshore nuclear power plant breakwater on shoreline evolution. Model measurements to be made across and along the shoreline north and south of the inlet, with and without the proposed breakwater, consisted of current patterns and breaking wave characteristics such as height, depth, and angle to the shoreline. Current patterns and calculated longshore transport rates with and without the proposed breakwater would then be compared. From these comparisons a judgment would be made as to the effect, if any, of the proposed breakwater on shoreline evolution.

Description of the Model

structed to a distorted scale of 1:75 vertically and 1:300 horizontally, model to prototype. The model was molded in cement mortar (fixed-bed) and an artificial transition was constructed from the -40 ft mean sea level (msl) contour to the wave generator pit (-69.2 ft msl). The model was approximately 113 by 115 ft and covered a total area of 9800 sq ft, of which about 6600 sq ft was contoured area. This reproduced, in nature, 34,000 ft of coastline and the bathymetry for a seaward distance of 18,000 ft. The model was operated in accordance with Froude's model law. Scale relations used in the transference from model to prototype were as follows:

| Characteristics | Dimensions* | Model:Prototype Scale Relation |
|----------------------|-------------------|-----------------------------------|
| Horizontal distance | L | $X_r = 1:300$ |
| Vertical distance | L | $Y_{r} = 1:75$ |
| Volume | r ₃ | $Vol_r = x_r y_r^2 = 1:1,687,500$ |
| Time | T | $T_r = Y_r^{1/2} = 1:8.66$ |
| Velocity | L/T | $Vel_r = Y_r^{1/2} = 1:8.66$ |
| Volumetric flow rate | L ³ /T | $Q_r = x_r Y_r^{3/2} = 1:194,586$ |
| Wave period | T | $Per_r = Y_r^{1/2} = 1:8.66$ |
| Wavelength | L | $L_r = Y_r = 1:75$ |
| Wave height | L | $H_r = Y_r = 1:75$ |

^{*} Dimensions are in terms of length (L) and time (T).

^{11.} A pump and manifold system were used to reproduce tidal currents. A differential manometer was installed in the discharge line of the pump and was used in conjunction with a control valve and pipe

arrangement to regulate both the flood and ebb volumetric flow rates through the inlet. The pipe system around the inner perimeter of the model was fitted with a series of openings; each opening was equipped with a sliding metal sleeve which could be used to vary the effective area of the opening. This system allowed the reproduction of a quite variable combination of flow rates.

Design of Model Breakwater

12. During the construction phase of the 3-D model, large-scale 2-D flume tests were conducted to determine reflection coefficients of the proposed breakwater at an undistorted scale. A representative range of wave periods and heights were tested with the incident and reflected wave heights being measured by a mobile wave gage (Photo 3) for each test wave. This information was used to calculate reflection coefficients representative of the prototype structure. By using these data it was determined, by a trial and error procedure, that a distorted structure composed of wire mesh covered with fibrous wave absorber (rubberized hair) would reflect about the same amount of wave energy as the prototype structure.

Test Equipment

13. A vertical-displacement, 60-ft-long wave generator was used to produce the model waves (Photo 2). The vertical motion of the plunger produced a periodic oscillation of the water normal to it. Test waves of the required characteristics were generated by varying the frequency and amplitude of the plunger motion. The wave generator was equipped with retractable jacks and wheels which enabled it to be positioned to generate waves from various wave directions. Changes in watersurface elevation as a function of time were measured by electrical wave-height gages at selected locations in the model and recorded on chart paper by an electrically operated oscillograph (Photo 4). The

electrical output of each wave gage was directly proportional to the submergence depth of the gage.

14. A gravity-feed dye injection system was used to inject a tracer for measuring current patterns. The system consisted of an elevated well connected by flexible tubing to portable injection stands. This arrangement allowed simultaneous injection at a variety of locations across the inlet and along the coastline. Two 16mm motion picture cameras were mounted above the model and used to record current patterns and wave motion. A still-picture camera also was used to obtain instantaneous current pattern and wave motion records.

Verification of Tidal Velocities

15. Prototype tidal velocity data, collected and furnished by E. G. and G. International, Environmental Services Division, were used to calibrate the model manifold system. A trial and error procedure was employed during which various combinations of control valve settings and sliding collar positions were tested. For each trial, tidal velocities were measured using weighted surface floats and a stopwatch at stations selected across the inlet to correspond with the given prototype data. Tests were conducted until settings were obtained which adequately reproduced mean steady-state flood and ebb tide flows through the inlet.

PART III: TEST CONDITIONS AND PROCEDURES

Wave Dimensions and Directions

- 16. In planning a test program for a model investigation involving wave action, it is necessary to select dimensions and directions for test waves that will allow the model to accurately reproduce the prototype wave climate. Surface-wind waves are generated by the tangential shear force of the wind blowing along the water surface and the normal force of the wind against the wave crests. Selection of test wave conditions entails evaluation of such factors as:
 - a. The frequency and duration of waves of different periods from different directions.
 - b. The refraction of waves caused by depth differentials.
 - c. The dissipation of wave energy due to viscous friction.
- 17. Wave refraction occurs when waves propagate over water of variable depth (provided the depth is less than about one-half the deepwater wavelength). Changes take place in all wave characteristics except wave period. The most important changes affecting test wave characteristics are the alteration of wave height and direction of travel. Changes in wave height and direction can be obtained by calculating refraction coefficients and plotting refraction diagrams. The diagrams are constructed by plotting orthogonals (lines drawn perpendicular to wave crests). Linear wave refraction theory assumes the waves do not break and there is no lateral flow of energy between wave orthogonals. The ratio between the wave height in deep water (Ho) and the wave height in shallow water (H) will be inversely proportional to the square root of the ratio of the corresponding orthogonal spacings (b and b) or $H/H_o = K(b_o/b)^{1/2}$ where K is the shoaling coefficient and $(b_o/b)^{1/2}$ is the refraction coefficient. Therefore, the quantity $K(b_o/b)^{1/2}$ serves as a conversion factor for transforming deepwater wave heights to shallow-water wave heights. The shoaling coefficient, a function of wavelength and water depth, can be obtained from Reference 6.

- 18. Wave refraction diagrams were prepared for selected wave directions and periods. Two sets of diagrams were prepared from the wave generator pit to the shoreline. In the first set the natural contours were used and in the second set the model contours with the sloping transition to the wave generator pit were substituted. A comparison of the diagrams showed the model accurately reproduced wave fronts near the shoreline. Diagrams for the southeast wave direction are presented in Appendix B.
- 19. Even though the model was built to a distorted scale, the large area of extremely shallow water reproduced by it made the excessive dissipation of energy at the bottom a problem worthy of correction. The effect of this energy dissipation on wave height is given by 7

$$- \left[\frac{5\pi (\pi \nu T)^{1/2}}{L^2 \left(\sinh \frac{4\pi d}{L} + \frac{4\pi d}{L} \right)} \right] \Delta X$$

$$H_2 = H_1 e$$

where

 H_{2} = the wave height after the wave has propagated a distance ΔX

H, = the incident wave height

v = kinematic viscosity

T = wave period

d = water depth

L = wavelength

 ΔX = an incremental distance

Energy dissipation was calculated along orthogonals from the wave generator to the breaker zone; wave heights at the wave generator were increased by an appropriate amount to compensate for the viscous-friction scale effects.

20. Model test wave conditions were selected from wave hindcast data obtained by A. H. Glenn and Associates (Table 1). These data represent an estimated yearly wave climate in terms of magnitude and duration of waves approaching the proposed Atlantic Generating Station from the various directions.

Test Series I

21. Model measurements, with and without the proposed breakwater, consisted of measuring currents at selected locations across the mouth of the inlet and along the north and south coastline (test series I), breaking wave characteristics (test series II), and average longshore currents (test series III). Selected test conditions for test series I are presented in Table 2. Velocity stations (Plate 2) were positioned across the inlet and along the shoreline both north and south. For each test condition, the currents were allowed to develop, dye was injected as a tracer, and the current and wave patterns were recorded on motion picture film. Still photos also were taken to give an instantaneous record of current and wave patterns.

Test Series II

22. The breaking wave characteristic tests (test series II) involved measuring the height and depth of breaking and the angle of breaking relative to the shoreline. Two longshore transport zones were selected, one north and one south of the inlet, in which the measurements were taken. These zones and baselines for referencing the angle of breaking are shown in Plate 3. Selected test conditions are presented in Table 3. Breaking-wave heights were obtained by placing electrical wave gages across the zones at the breaker line. Uneven breaking of the wave front within a selected zone required the placement of up to four wave gages to adequately define the wave front. The depth of breaking was obtained directly from the model using an engineer's level. The angle of breaking relative to the assumed baseline was obtained from visual observation, still photos, and the motion picture film gathered in test series I.

Test Series III

23. Average longshore current measurements (test series III) were

made by injecting a line of dye perpendicular to the assumed baseline of the selected zone (Plate 3). The currents were allowed to develop; the general direction of the dye was observed and its rate of travel timed with a stopwatch. Selected conditions for test series III are given in Table 4. These average current measurements were taken at the same time as the data in test series II, simply to augment the current data collected in test series I and to provide an overall look at the current regime within the selected zones rather than at specific stations as measured in test series I.

PART IV: DATA ANALYSES AND DISCUSSION OF RESULTS

Test Series I

- 24. The motion picture film obtained for each test condition was analyzed with the aid of a stop-action movie projector. Current velocities and directions were extracted from the film for sta 1A-4B for the south wave direction, 2A-6B for the southeast wave direction, and 4A-7B for the east wave direction (see Plate 2 for stations). Photos 5-22 illustrate model current patterns for selected test conditions.
- 25. All current data obtained in test series I are given in Table 5. In some instances, an azimuth or both a velocity and azimuth value may be left blank. These omissions resulted from either the current pattern having such a broad range of flow directions that a pronounced direction was not definable or the complete loss of the data at a station due to some mechanical malfunction. Plates 4-29 present the data from Table 5 in a comparative graphical form. Careful scrutiny of these plates reveals some changes in current patterns with the breakwater installed; however, the majority of the data indicate no predominant trends either in decrease or increase of velocity or shift of direction. It is felt that most of the differences shown are reasonably within the limits of experimental error. Repeat tests of selected wave conditions indicated current velocities were reproducible within ±10 percent on a comparative basis.
- 26. Since the data presented in Plates 4-29 are quite detailed, it was believed averaging the data would result in a clearer picture of the overall current measurement results. Table 6 presents average current velocities and directions for a given wave period. To obtain this table, the values of velocity and azimuth for all wave heights at a given station for a given period, wave direction, and tidal condition (Table 5) were averaged. The data from Table 6 also are presented in a graphical manner in Plates 30-56. These data again fail to indicate any significant changes in current patterns (velocity or direction).

Test Series II

- 27. Data obtained from the breaking-wave height tests are presented in Tables 7 through 18. Photos 23-32 illustrate the simultaneous measurement of breaking-wave heights and longshore currents (test series III) for selected wave conditions.
- 28. Extensive correlation of model and prototype wave and sediment transport data by other researchers has yielded several longshore transport equations. In all these studies, the transport rate is some function of the breaking-wave characteristics. Three of the more common equations relating breaking-wave characteristics to the longshore transport rate, $Q_{\rm L}$, are:

$$Q_{L} = 118.9E'_{L} (CERC)^{6}$$
 (1)

$$Q_{L} = 210E_{L}^{0.8} (Caldwell)^{9}$$
 (2)

$$Q_{L} = 548\overline{H}_{b}^{2} (Galvin)^{10}$$
(3)

where

 E_{L}^{\prime} = total longshore energy per foot of beach per day

H = average breaking-wave height for all waves considered

29. In order to use Equations 1 and 2, the total longshore energy per foot of beach per wave must be calculated and the total number of waves per day approaching the coastline under consideration must be known. The total longshore energy per foot of beach per wave is given by

$$E_{L} = \frac{\gamma H_{b}^{2} L_{b}}{8} \left[1 - \frac{\pi^{2}}{2 \tanh^{2} \left(\frac{2\pi d_{b}}{L_{b}} \right) \left(\frac{H_{b}^{2}}{L_{b}^{2}} \right) \sin \alpha \cos \alpha \right]$$
(4)

where

γ = specific weight of water

H_b = wave height at breaking

Lb = wavelength at breaking

d, = depth of water a wave breaks in, ft

α = angle between breaking-wave crest and shoreline

To determine the total number of waves per day the wave hindcast data
(Table 1) were regrouped to make the selected test waves representative
of the average wave climate. Tables 19-21 illustrate this regrouping
procedure for waves approaching the south zone. The same objective is
accomplished for the north zone in Tables 22 and 23. Since the original
wave climate was only divided into 45-deg wave direction groups and tests
were conducted at selected 22.5-deg intervals, it became necessary to redistribute the wave occurrence frequencies. To accomplish this, it was
assumed that each 22.5-deg interval would receive 25 percent of the
total waves from each of the two major directions adjacent to it.
Tables 24, 25, and 26 illustrate this final regrouping procedure.

- 30. The information required to calculate transport rates in the two longshore transport zones is summarized in Tables 27 and 28. The "Breaking Height Squared" column is the average height at breaking, squared, for all wave gages considered for a particular test wave. The "Transport Direction" column was determined by the orientation of the breaking-wave crest relative to the assumed baseline. The "Longshore Energy per Foot of Beach per Wave" was obtained by applying the longshore energy Equation 4 to the measured breaking-wave characteristics at each of the gages in a zone (Tables 7 through 19) and then averaging the individual longshore energy calculated for each test wave. The "Longshore Energy per Foot of Beach per Wave per Day" was determined by multiplying the longshore energy per wave by the number of waves per day.
- 31. Table 29 lists calculated transport rates, with and without the proposed breakwater, for all wave directions considered in test series II. It should be mentioned that the "Average Breaking Height Squared" column was obtained by taking a weighted average of the breaking heights (Tables 27 and 28) for a particular wave direction and tidal condition. The weighted average was obtained by multiplying the individual values of \overline{H}_b^2 by their respective occurrences in waves per day and dividing by the total number of waves per day from a given test

direction. This procedure can best be illustrated by an example. The data from Table 27 for the northeast wave direction for the case with the structure out can be used to obtain \overline{H}_{b}^{2} as follows:

$$\begin{aligned} \overline{H}_b^2 &= \left[(11.50)(209) + (30.91)(115) + (98.19)(17) + (22.85)(137) \right. \\ &+ 128.24(83) + 59.19(11) + 197.411(23) \right] \div (209 + 115) \\ &+ 17 + 137 + 33 + 11 + 23) \\ \overline{H}_b^2 &= \frac{26.593.27}{595} = 44.69 \text{ ft}^2 \end{aligned}$$

The same procedure was followed to obtain values of \overline{H}_b^2 for the other test directions.

Table 30 presents calculated transport rates for the major transport directions (north and south). When more than one tidal condition per wave direction (south, southeast, and east) was tested it was assumed that slack tide occurred 50 percent of the time and flood and ebb tide 25 percent each. It should be observed that all the calculated longshore transport rate changes are 7 percent or less except for a 19 percent change obtained by applying Galvin's equation to the south zone. In this particular case, the relatively small reduction in wave height (approximately 9.5 percent) is amplified because Galvin's method only considers wave height squared rather than wave height, breaking depth, and breaking angle to the shoreline as used in the energy calculations. It should be emphasized that the most important consideration in the present investigation is not the absolute value of the predicted transport rates or the relative merits of the different equations, but the comparative predicted transport rates (with and without the breakwater). The three equations considered give widely different predicted transport rates; however, they are all similar in that they indicated little change with the proposed breakwater installed. When one considers the small experimental error involved in obtaining such data, the differences become even more minimal. Repeat tests of selected wave conditions indicated breaking characteristics (height,

depth, and angle) to be reproducible to the extent that calculated transport rates on a comparative basis have an accuracy of +8 percent.

Test Series III

33. Comparative average current velocities and directions of flow are given in Table 31. These data indicate little difference in velocity and no directional changes with the proposed breakwater installed. These data are not presented graphically since they are of an auxiliary nature and were obtained only to give an overall view of the current regime within a general area.

PART V: CONCLUSIONS

- 34. Based on the results of the hydraulic model study described herein, it appears that:
 - a. The construction of the proposed power plant will not:
 - (1) Significantly alter current patterns shoreward of it.
 - (2) Significantly alter longshore current velocities or transport rates north and south of the inlet.
 - (3) Have a detrimental effect on shoreline evolution in the area under consideration.
 - b. The Little Egg Inlet area is historically one of very dynamic geomorphological change and any changes produced by the construction of the breakwater protecting the offshore nuclear power plant would certainly be masked by the natural changes at the inlet.
 - c. The distorted-scale model provided adequate information to reach the conclusions set forth in this investigation.

PART VI: GENERAL KNOWLEDGE GAINED AND FUTURE APPLICATIONS

35. Results of this investigation have an extremely wide application. The present energy crisis makes it a virtual certainty that offshore nuclear power plants, offshore deepwater oil terminals, and perhaps entire offshore energy-related industrial complexes will be constructed. The impact of this construction on coastal evolution must be reliably evaluated. The methodology developed in this investigation can be very beneficial in evaluating possible effects of other proposed offshore structures.

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Table 1
Estimated Magnitude and Duration of Waves Approaching Proposed Atlantic
Generating Station from the Indicated Directions

| Wave Period | | | | | Perce | entage o | of Total | Wave Cl | imate per | r Wave H | eight Gr | oup, ft | | | | |
|-----------------------|------|------|------|------|-------|----------------------|----------|--------------|-----------|----------|----------|---------|-------|-------|------|-------|
| sec | 0-1 | 1-3 | 3-5 | 5-7 | 7-9 | 9-11 | 11-13 | 13-15 | 15-17 | 17-19 | 19-21 | 21-23 | 23-25 | 25-27 | >27 | Total |
| | | | | | | | | Sout | th_ | | | | | | | |
| 0-5 5-7 | 1.20 | 1.50 | 0.80 | 0.30 | 0 | 0.04 | 0.04 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3.80 |
| 7-9 9-11 | 0.30 | 0.70 | 0.80 | 0.60 | 0.45 | 0.11 | 0.04 | 0.05 | 0.04 | 0.03 | 0.02 | 0.01 | 0.01 | 0.01 | 0 | 3.15 |
| 11-13 13-15 | 0.02 | 0.10 | 0.16 | 0.16 | 0.18 | 0.19 | 0.10 | 0.10 | 0.05 | 0.05 | 0.03 | 0.02 | 0.02 | 0.01 | 0.02 | 0.47 |
| >15 | 0 | 0 | 0 | 0.01 | 0.03 | 0.03 | 0.03 | 0.02 | 0.02 | 0.01 | 0.01 | 0 | 0.01 | 0 | 0.02 | 0.19 |
| Total | 2.90 | 4.20 | 2.79 | 2.01 | 1.22 | 0.73 | 0.40 | 0.25 | 0.18 | 0.14 | 0.09 | 0.05 | 0.05 | 0.03 | 0.06 | 15.10 |
| | | | | 0 | 2 22 | - | | South | | 100 | - | | 5 | | | |
| 0-5 5-7 | 0.30 | 0.75 | 0.40 | 0.08 | 0.02 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2.00 |
| 7-9 9-11 | 0.25 | 0.42 | 0.50 | 0.35 | 0.31 | 0.19 | 0.03 | 0.02 | 0.02 | 0.01 | 0.01 | 0.01 | 0.02 | 0 | 0 | 2.10 |
| 11-13 13-15 >15 | 0.09 | 0.07 | 0.05 | 0.09 | 0.16 | 0.17 0.05 0.02 | 0.08 | 0.03 | 0.02 | 0.02 | 0.01 | 0.02 | 0.03 | 0 | 0 | 0.8 |
| Total | 2.66 | 3.20 | 1.80 | 1.02 | 1.06 | 0.69 | 0.29 | 0.12 | 0.08 | 0.05 | 0.04 | 0.04 | 0.09 | 0 | 0 | 11.1 |
| | | | | | | | | East | <u>t</u> | | | | | | | |
| 0-5 5-7 | 3.18 | 2.10 | 0.42 | 0.18 | 0.08 | 0.06 | 0.02 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5.88 |
| 7-9 9-11 | 0.26 | 0.55 | 0.39 | 0.37 | 0.39 | 0.13 | 0.04 | 0.02 | 0.01 | 0.02 | 0.01 | 0.02 | 0.01 | 0 | 0 | 2.20 |
| 11-13 | 0.04 | 0.07 | 0.09 | 0.11 | 0.16 | 0.15 | 0.12 | 0.05 | 0.04 | 0.02 | 0.02 | 0.01 | 0.04 | 0 | 0 | 0.98 |
| >15 | 0 | 0 | 0 | 0.01 | 0.01 | 0.02 | 0.02 | 0.03 | 0.02 | 0.01 | 0 | 0.01 | 0.01 | 0 | 0 | 0.11 |
| Total | 3.80 | 3.70 | 1.90 | 1.14 | 0.96 | 0.66 | 0.35 | 0,19 | 0.11 | 0.09 | 0.05 | 0.04 | 0.11 | 0 | 0 | 13.10 |
| | | 4 22 | 0.00 | 0.00 | 5 | -8 | .00 | North | | | | ~ | | | | 0.00 |
| 0-5 5-7 | 0.70 | 1.30 | 0.75 | 0.25 | 0.17 | 0.06 | 0.01 | 0.01 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2.50 |
| 7-9 | 0.10 | 0.51 | 0.56 | 0.64 | 0.44 | 0.12 | 0.03 | 0.01 | 0.02 | 0.01 | 0.02 | 0.02 | 0.01 | 0 | 0 | 2.47 |
| 11-13 13-15 | 0.03 | 0.03 | 0.12 | 0.18 | 0.22 | 0.13 | 0.05 | 0.04 | 0.03 | 0.02 | 0.03 | 0.01 | 0.05 | 0 | 0 | 0.93 |
| >15 | 0 | 0 | 0 | 0.02 | 0.02 | 0.02 | 0.02 | 0.01 | 0.01 | 0.01 | 0.06 | 0.01 | 0.02 | 0 | 0 | 12.17 |
| Total | 2.29 | 2.88 | 2.55 | 1.84 | 1.35 | 0.52 | 0.21 | 0.13 Nort | | 0.01 | 0.00 | 0.04 | 21.23 | | | 15.4 |
| 0-5 | 2.39 | 3.97 | 1.93 | 0.23 | 0.02 | 0 | 0 | 0 | 0 | .0 | 0 | 0 | 0 | 0 | 0 | 8.54 |
| 5-7 7-9 | 0.41 | 0.43 | 0.36 | 0.44 | 0.15 | 0.03 | 0.01 | 0.01 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1.83 |
| >9 | 0 | 0 | 0 | 0 | 0.02 | 0.03 | 0.01 | 0.01 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.07 |
| Total | 2.80 | 4.40 | 2.30 | 0.77 | 0.25 | 0.13 | 0.03 | 0.02 | 0 | 0 | 0 | 0 | 0 | .0 | 0 | 10.70 |
| | | | | | | 2.22 | | North | - | 4 | | | | Ā | | 10.07 |
| 0-5 | 3.79 | 5.42 | 0.94 | 0.06 | 0.03 | 0.01 | 0.01 | 0.01 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 10.27 |
| Total | 4.00 | 5.85 | 1.33 | 0.12 | 0.05 | 0.02 | 0.01 | 0.01 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 11.39 |
| | | | | | | | | West | <u>t</u> | | | | | | | |
| 0-5 | 4.47 | 1.34 | 0.58 | 0.76 | 0.77 | 0.57 | 0.29 | 0.11 | 0.03 | 0.01 | 0 | 0 | 0 | 0 | 0 | 8.93 |
| Total | 4.70 | 1.80 | 0.90 | 0.80 | 0.78 | 0.57 | 0.29 | 0.11 | 0.03 | 0.02 | 0 | 0 | 0 | 0 | 0 | 10.00 |
| | | | | | | | | South | vest | | | | 2 | | | 23 43 |
| 0-5 5-7 | 2.96 | 5.24 | 3.30 | 1.05 | 0.05 | 0.06 | 0,01 | 0.01 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12,60 |
| 7-9 9-11 | 0.11 | 0.51 | 0.56 | 0.64 | 0.44 | 0.12 | 0.03 | 0.01 | 0.02 | 0.01 | 0.02 | 0.02 | 0.01 | 0 | 0 | 2.48 |
| 11-13 | 0.03 | 0.03 | 0.12 | 0.18 | 0.22 | 0.13 | 0.05 | 0.04 | 0.03 | 0.02 | 0.03 | 0.01 | 0.05 | 0 | 0 | 0.93 |
| >15 | 0 | 0 | 0 | 0.02 | 0.02 | 0.02 | 0.02 | 0.01 | 0.01 | 0.01 | 0 | 0.01 | 0.02 | 0 | 0 | 0.14 |
| Total | 5.13 | 6.19 | 4.47 | 2.64 | 1.40 | 0.52 | 0.21 | 0.13 | 0.10 | 0.07 | 0.06 | 0.04 | 0.13 | 0 | 0 | 21.09 |

Table 2

<u>Selected Conditions for Test Series I</u>

Stillwater Level = 0.0 (msl)

| | | Wave Di | rection | | |
|-----------------------|-----------------------------|-----------------------|-----------------------------|-----------------------|----------------------|
| Ea | st | South | neast | So | uth |
| Wave Period sec | Wave Height <u>ft</u> | Wave Period sec | Wave Height <u>ft</u> | Wave Period sec | Wave Height ft |
| 6 | 2 | 6 | 2 | 6 | 2 |
| 6 | 4 | 6 | 4 | 6 | 4 |
| 6 | 7 | 6 | 7 | 6 | 7 |
| 6 | 10 | 6 | 10 | 6 | 10 |
| 10 |) 4 | | 4 | 10 | 4 |
| 10 | 10 | 10 | 10 | 10 | 10 |
| 10 | 14 | 10 | 14 | 10 | 14 |
| 10 | 18 | 10 | 18 | 10 | 18 |
| 14 | 4 | 14 | 4 | 14 | 4 |
| 14 | 10 | 14 | 10 | 14 | 10 |
| 14 | 14 | 14 | 14 | 14 | 14 |
| 14 | 18 | 14 | 18 | 14 | 18 |

Note: All wave conditions for all wave directions conducted for slack, flood, and ebb tide with and without proposed breakwater in place.

Table 3

<u>Selected Conditions for Test Series II</u>

Stillwater Level = 0.0 (msl)

| | | | | | | ition an | d wave L | irection | 1 | 011 | 707 7 | 3 777 7 | m. a |
|-----------------------|-----------------------------|-----------------------|----------------------|-----------------------|----------------------|-----------------------|----------------------|-----------------------|----------------------|-----------------------|----------------------|-----------------------|----------------|
| NT | A. a. a.b. | TOO | 2.5°N | Slack T | .5°S | Court | heast | FOC | .5°E | | Flood, | | |
| | theast | _ | | | | | | | | | st | Sou | |
| Wave Period sec | Wave Height <u>ft</u> | Wave Period sec | Wave Height ft | Wave Period sec | Wave Height |
| | | | | | | South | Zone* | | | | | | |
| 6 6 | 4 7 10 | 6 6 | 4 7 10 | 6 6 | 4 7 10 | 6 6 | 4 7 10 | | | 6 6 | 4 7 10 | | |
| 10 10 | 4 10 | 10 10 | 4 10 | 10 10 | 10 10 | 10 10 | 4 10 | | | 10 10 | 10 | | |
| 14 14 | 10 | 14 14 | 4 10 | 14 14 | 4 10 | 14 14 | 10 | | | 14 14 | 10 | | |
| | | | | | | North | Zone* | | | | | | |
| | | | | | | 6 | 10 | 6 | 10 | | | 6 | 10 |
| | | | | | | 10 10 | 10 14 | 10 10 | 10 14 | | | 10 10 | 10 |
| | | | | | | 14 14 | 10 14 | 14 | 10 14 | | | 14 | 10 14 |

^{*} Zones are defined in Plate 3.

Table 4

Selected Conditions for Test Series III, Slack Tide

Stillwater Level = 0.0 (msl)

| | | | | Wave Di | rection | | | | |
|-----------------------|----------------------|-----------------------|----------------------|-----------------------|----------------------|-----------------------|----------------------|-----------------------|----------------------|
| North | east | E22. | 5°N | E22. | 5°S | South | east | S22. | 5°E |
| Wave Period sec | Wave Height ft |
| | | | | South | Zone* | | | | |
| 6 | 4 | 6 | 4 | 6 | 4 | 6 | 4 | | |
| 6 | 7 | 6 | 7 | 6 | 7 | 6 | 7 | | |
| 6 | 10 | 6 | 10 | 6 | 10 | 6 | 10 | | |
| 10 | 4 | 10 | 4 | 10 | 14 | 10 | 4 | | |
| 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | | |
| 14 | 24 | 14 | 14 | 14 | 14 | 14 | 4 | | |
| 14 | 10 | 14 | 10 | 14 | 10 | 14 | 10 | | |
| | | | | North | Zone* | | | | |
| | | | | | | 6 | 10 | 6 | 10 |
| | | | | | | 10 | 10 | 10 | 10 |
| | | | | | | 10 | 14 | 10 | 14 |
| | | | | | | 14 | 10 | 14 | 10 |
| | | | | | | 14 | 14 | 14 | 14 |

^{*} Zones are defined in Plate 3.

Table 5 Comparison of Test Series I Current Measurements Current Velocities in fps and Direction* at Indicated Stations**

| Wave Period | od Height Breakwater 1A 1B | | | | | | | | | | | 3A3B | | | | A | 4B | | |
|----------------|----------------------------|-----------------|--------|------------|------------|------------|--------------|------------|--------|------------|--------------|------------|------|------------|--------------|------------|------|------------|--|
| sec | ft | Status | Vel | Az | <u>Vel</u> | Az - | Vel | Az | Vel | Az | Vel_ | Az | Vel_ | Az | Vel. | Az | Vel_ | B Az | |
| | | | | | | Sou | th Wave | Direct | ionSl | ack Tid | <u>é</u> | | | | | | | | |
| 6 | 2 | Without With | 0.38 | 240 | 0.57 | 165 165 | 0.34 | 30 30 | 0.51 | 90 60 | 0.88 | 330 330 | 0.34 | 330 | 0.43 | 315 | 0.32 | 60 | |
| 6 | 4 | Without With | 0.33 | 135 | 0.58 | 180 150 | 0.44 | | 0.83 | 90 90 | 1.72 | 300 285 | 0.96 | 60 75 | 0.53 | | 0.73 | 60 90 | |
| 6 | 7 | Without With | 0.38 | 180 | 0.49 | 150 | 0.57 | 105 90 | 1.01 | 75 75 | 2.12 | 315 315 | 1.19 | 30 15 | 1.26 | 60 30 | | | |
| 6. | 10 | Without | | | 0.38 | 45 | 0.67 | 120 | 1.83 | 60 | 1.50 | 315 | 0.67 | 315 | 0.91 | 0 | 0.96 | 60 90 | |
| 10 | 4 | With Without | 0.69 | 75 | 0.57 | 75 195 | 0.94 | 120 210 | 0.37 | 60 | 1.80 | 330 345 | 0.67 | 315 0 | 0.91 | 45 315 | 0.87 | 90 45 | |
| 10 | 10 | With Without | 0.97 | 45 75 | 0.66 | 75 45 | 0.57 | 30 60 | 2.00 | 60 60 | 2.48 | 345 315 | 0.94 | 330 | 0.58 | 60 | 0.87 | 60 90 | |
| 10 | 14 | With Without | 1.15 | 60 | 0.81 | 60 45 | 3.24 | 105 | 1.74 | 60 45 | 2.53 | 315 330 | 0.78 | 315 330 | 0.90 | 60 45 | 0.76 | 90 120 | |
| 10 | 18 | With Without | 2.71 | 345 | 0.87 | 90 60 | 2.43 | 315 15 | 1.73 | 45 | 1.64 | 15 | 0.89 | 60 | 0.90 | 60 | 0.68 | 120 | |
| | 1 | With | 2.11 | 135 | 1.86 | 60 | 2.55 | 15 | 2.45 | 75 60 | 2.38 | 270 285 | 0.57 | 300 315 | 0.64 | 75 45 | 0.67 | 135 105 | |
| 14 | 4 | Without With | 0.91 | 60 60 | 0.49 | 60 | 0.74 | 60 30 | 1.56 | 60 60 | 2.01 | 0 345 | 1.05 | 30 | 0.69 | 30 | 0.99 | 75 60 | |
| 14 | 10 | Without With | 0.87 | 120 60 | 1.03 | 75 60 | 0.80 | 0 345 | 2.43 | 60 45 | 1.79 2.44 | 285 0 | 0.46 | 315 0 | 1.01 | 30 0 | 0.68 | 150 105 | |
| 14 | 14 | Without With | | | 2.27 | 45 60 | 1.08 | 60 210 | 1.88 | 75 45 | 2.00 | 270 345 | 1.16 | 180 | 0.80 | 90 30 | 1.39 | 105 120 | |
| 14 | 18 | Without With | 1.76 | 60 90 | 1.73 | 45 45 | 0.68 | 60 | 1.44 | 60 75 | 2.04 | 315 0 | 1.03 | 315 | 0.65 | 0 45 | 0.41 | 120 | |
| | | | | | | Sou | th Wave | Direct | ionFl | ood Tid | e | | | | | | | | |
| 6 | 2 | Without With | 0.87 | 225 | 1.61 | 210 | 1.66 | 255 | 2.39 | 240 | 3.41 | 315 | 2.77 | 315 | 4.06 | 270 270 | 2.26 | 315 315 | |
| 6 | 4 | Without With | 0.66 | 210 225 | 1.35 | 210 | 1.48 | 255 225 | 2.68 | 240 240 | 4.32 | 315 315 | 2.63 | 330 330 | 3.19 | 285 285 | 2.88 | 315 315 | |
| 6 | 7 | Without With | 0.58 | 225 | 1.22 | 210 | 1.19 | 225 255 | 1.68 | 240 | 4.44 | 315 315 | 3.65 | 330 330 | 2.46 | 300 | 2.68 | 315 315 | |
| 6 | 10 | Without | 0.60 | 180 | 1.01 | 180 | 1.16 | 255 | 1.75 | 240 | 4.25 | 330 | 3.02 | 315 | 2.65 | 285 | 2.64 | 315 | |
| 10 | 4 | With Without | 0.56 | 195 210 | 1.21 | 195 210 | 1.07 | 240 255 | 2.26 | 240 | 5.16 | 330 315 | 3.45 | 330 330 | 2.72 | 300 285 | 2.47 | 315 | |
| 10 | 10 | With Without | 0.70 | 225 | 1.50 | 210 | 1.63 | 255 | 2.26 | 240 60 | 3.80 | 315 330 | 2.77 | 330 315 | 2.67 | 285 285 | 2.47 | 315 315 | |
| 10 | 14 | With Without | 0.79 | 0 | 0.71 | 180 | 2.07 | 255 315 | 2.80 | 60 240 | 4.58 3.44 | 330 315 | 2.49 | 330 315 | 2.19 | 285 | 2.68 | 315 | |
| 10 | 18 | With Without | 0.95 | 60 150 | 0.38 | 150 | 1.84 | 315 | 2.56 | 240 | 3.63 | 330 | 2.47 | 315 300 | 2,32 | 285 270 | 2.08 | 315 | |
| | | With | 2.01 | 180 | 1.35 | 135 | 1.43 | 255 | 2.31 | 240 | 3.67 | 315 | 0.75 | 190-1 | 3.41 | 270 | 2.53 | 315 | |
| 14 | 4 | Without With | 0.22 | | 0.55 | 195 210 | 0.96 | 255 255 | 1.00 | 240 | 4.86 | 330 315 | 2.93 | 330 330 | 3.38 | 300 | 2.80 | 315 315 | |
| 14 | 10 | Without With | 0.26 | 165 | 1.43 | 75 105 | 1.25 | 225 180 | 0.39 | 75 | 5.02 | 330 345 | 3.13 | 330 | 2.64 3.13 | 300 285 | 2.46 | 315 315 | |
| 14 | 14 | Without With | 1.18 | 60 180 | 1.36 | 75 45 | 1.19 0.86 | 255 255 | 1.73 | 240 240 | 5.00 4.12 | 315 330 | 2.23 | 315 315 | 2.61 3.00 | 285 285 | 2.26 | 300 | |
| 14 | 18 | Without With | 1.26 | 60 180 | 0.91 | 60 90 | 1.70 1.72 | 180 165 | 2.43 | 240 240 | 5.00 4.46 | 330 330 | 2.24 | 315 315 | 2.32 | 285 300 | 2.56 | 315 315 | |
| | | | | | | So | uth Wav | e Direc | tion-E | bb Tide | 2 | | | | | | | | |
| 6 | 2 | Without With | 0.65 | 60 | 0.43 | 180 180 | 0.90 | 120 180 | 1.05 | 45 | 1.83 | 75 90 | 2.32 | 135 150 | 3.14 2.58 | 120 120 | 4.31 | 135 135 | |
| 6 | 4 | Without With | 0.68 | 195 120 | 1.02 | 195 180 | 0.85 | 120 | 0.53 | 240 270 | 1.83 | 60 15 | 2.29 | 165 135 | 2.43 | 120 135 | 3.26 | 120 135 | |
| 6 | 7 | Without | 0.21 | 120 | 0.68 | 180 | 0.43 | 45 | 0.75 | 240 | 2.05 | 75 60 | 1.79 | 150 135 | 2.99 | 105 | 4.41 | 120 | |
| 6 | 10 | With Without | 1.32 | 90 | 0.68 | 180 | 1.73 | 90 | 0.54 | 240 60 | 1.89 | 60 | 1.45 | 180 | 2,49 | 90 | 3.92 | 120 | |
| 10 | 4 | With Without | 0.42 | 135 | 0.42 | 180 180 | 0.74 | 120 | 1.27 | 60 105 | 2.32 | 60 30 | 2.03 | 150 300 | 2.49 | 90 105 | 2.85 | 135 | |
| | 10 | With Without | 0.53 | 180 | 0.53 | 180 60 | 0.42 | 210 60 | 2.47 | 105 60 | 2.11 | 105 210 | 2.08 | 135 165 | 2.61 | 150 90 | 2.85 | 135 135 | |
| 10 | | With | , 125c | 86 | 0.61 | 60 | 2.13 | | 2.14 | 60 120 | 1.36 | 210 | 2.04 | 150 165 | 2.26 | 120 135 | 3.64 | 135 150 | |
| 10 | 14 | Without With | 1.72 | 30 | 1.15 | 90 120 | 2.51 | 30 30 | 1.73 | 105 | 1.37 | 60 | 2.31 | 150 | 2.63 | 120 | 3.43 | 150 | |

^{*} Direction in the azimuth measured clockwise from New Jersey grid north.

** Station locations given in Plate 2.

† Without means breakwater is not installed. With means breakwater is installed.

| Period sec | Height ft | Breakwater Status | Vel | 1A A | 2 | Vel_ | Az | Ve) | ZA A | 2 | Vel_ | Az | Ve: | 3A | 12 | Vel_ | Az Az | V€ | 4A | An | Vel | AZ AZ |
|---------------|-----------|----------------------|-------|------------|---------|--------------|------------|------------|--------|------------|--------|-----------|--------|------------|----------|------|------------|------------|-------|---------|--------------|----------|
| | | | | | | 5 | outh W | ave D | irecti | onE | bb Tid | e (Co | ntinue | d) | | | | | | | | |
| 10 | 18 | Without With | 2.07 | | | 1.38 | 60 30 | 4.5 | | 5 | 2.31 | 90 60 | 3.3 | | 30 | 2.71 | 195 180 | | | 105 | 3.67 | 135 |
| 14 | 4 | Without With | 0.80 | 18 | 30 | 1.38 | 165 195 | 1.6 | 6 12 | 0 | 1.11 | 60 90 | 2.0 | 7 | 45 75 | 1.43 | 165 | 2. | 98 | 105 | 3.14 | 135 |
| 14 | 10 | Without With | | | | 1.59 | 75 120 | 2.6 | 8 6 | 0 | 3.13 | 90 60 | 2.5 | 7 8 | 25 | 3.13 | 180 | | 85 1 | 105 | 3.96 | 135 |
| 14 | 14 | Without With | 0.89 | | 12. | 2.32 | 45 135 | 2,2 | | 5 | 1.28 | 75 90 | 1.8 | - | 90 | | | | | 90 | 3.92 | 135 |
| 14 | 18 | Without With | | | | 3.90 1.73 | 30 60 | 2.0 | | | 2.56 | 75 135 | 2.3 | | 30 45 | | | 3. | 33. 1 | 20 | 4,16 3.74 | 135 |
| | | | Vel | A Az | Vel Vel | B Az | 3. Vel | A Az | Vel 3 | | Vel. | | Vel | B Az | Vel S | A Az | Vel Vel | B Az | Vel | A Az | Vel | B Az |
| | | | | | | | South | neast | Wave I | lrect | ion | Slack | Tide | | | | | | | | | |
| 6 | 2 | Without With | 0.35 | | 0.61 | 120 | 1.73 | 0 | 0,52 | 330 | 0.35 | | 0.35 | | 0.26 | | 0.26 | | 0.61 | 270 | 0.61 | 165 |
| 6 | 14 | Without With | 0.20 | | 0.78 | | | 285 | 0.78 | | | 330 | 1.05 | 330 345 | | | 0.26 | | 2.52 | | | |
| 6 | 7 | Without With | 0.95 | 180 | | 60 | | 300 270 | 0.95 | | 0.78 | 75 60 | 1.47 | 315 | 0.52 | 180 | | 150 135 | 1.99 | 285 | 1.47 | 180 |
| 6 | 10 | Without With | 1.47 | | 2.25 | | 3.12 | | 1.04 | 300 | 1.56 | 60 | | 300 | 0.52 | | 0.52 | 150 | 2.77 | 285 | 1.47 | 180 |
| 10 | 4 | Without With | 0.78 | | 1.39 | | | 270 | 0.61 | 0 | 1.04 | 211 | 0.78 | | 0.43 | | 0.43 | 135 | | 285 | 1.04 | 180 |
| 10 | 10 | Without With | 2.25 | | 3.03 | 60 60 | | - | 0.52 | 30 | | 300 | | 120 | 1,13 | 180 | 0.96 | | 1.47 | 240 | 1.73 | 180 |
| 10 | 14 | Without With | 2.60 | | 2.42 | 10000 | | 285 | 0.61 | 15 | 0.69 | 330 | 0.87 | 120 | 1.21 | 180 | 1.13 | 150 | 2,77 | 255 | 2.34 | 180 |
| 10 | 18 | Without With | 3.38 | | 1.99 | 60 60 | 2.94 | 285 255 | 0.69 | | 1.30 | | 1.39 | 150 | 1.13 | 180 | 1.21 | 150 | 3.12 | 255 | 2.25 | 180 |
| 14 | 4 | Without With | 0.87 | 150 135 | 2.77 | 60 75 | 3.12 | 300 | 0.78 | 300 | 2.08 | 45 | | 180 | 0.52 | 180 | 0.52 | | | 270 | 2.08 | 195 |
| 14 | 10 | Without With | 1.39 | | 5.11 | | 1.56 | 300 | 1.39 | 315 | | | | 165 | 1.73 | 180 | | 165 | 3.12 | | 3.46 | 195 |
| 14 | 14 | Without With | 1.73 | | 3.98 | 60 60 | 3.20 | 270 | 1.21 | 315 330 | 0.69 | 345 | 1.30 | 165 | 1,73 | 180 | 1.47 | 150 | 3.98 | 240 | 3.55 | 195 |
| 14 | 18 | Without With | 2.08 | 30 30 | 3.64 | 60 60 | 2.68 | | 1.30 | 45 | 0.87 | 285 | 1.04 | 165 | 1.39 | 195 | 1.39 | 165 | 3.46 | 240 | 2.86 | 105 |
| | | | | | | | South | east V | | | | | | | | | | | -000 | | | -64 |
| 6. | 2 | Without With | 1.32 | 240 | 2.37 | 240 | 2.96 | 300 | 2.22 | 315 315 | 2.22 | 285 | 2.21 | 315 | 1.44 | | 1.52 | | | | 1.44 | 15 15 |
| 6 | 4 | Without With | 1.38 | | 2.27 | 240 | 3.57 | 300 | 2.27 | 315 | 1.92 | 285 | 2.29 | 300 | 1.66 | 330 | 1.60 | 315 | 1.60 | 3/15 | 0.58 | 15 |
| 6 | 7 | Without With | 1.21 | 225 | 1.02 | 75 75 | 3.91 | 300 | 2.81 | 315 | 1.36 | 315 | 2.29 | 315 | | | 1.60 | | | | | |
| 6 | 10 | Without With | 1.41 | 240 | 1.56 | 60 60 | 4.37 | 285 270 | 2.68 | 300 | 1 58 | ann | 1 81 | 3918 | 1 65 | 27.5 | 7 70 | 79.0 | 8 to | - No | 2 | 200 |
| 10 | | Without With | 1.54 | 255 | 2,15 | 240 | 4.22 | 300 | 3.12 | 315 | 2.55 | 285 | 2.44 | 375 | 2-02 | 215 | 1 00 | 216 | 0.00 | 'n | 2 62 | 24 |
| 10 | | Without With | 1.77 | 185 | 3.08 | 60 | 3.63 | 300 | 2.31 | 315 | 1.35 | 0 | 2.06 | 315 | 1.38 | 300 | 1.07 | 200 | 0.00 | DEE | 1 90 | 305 |
| 10 | | Without With | 3.62 | 345 | 2.07 | 45 | 3.58 | 330 | 2.46 | 315 | 1.73 | 300 | 1.78 | 315 | 0.97 | 240 | 0.93 | 300 | 1 05 | nic | 1 6E | 700 |
| 10 | | Without With | 3.15 | 345 | 1.77 | 45 | 1.31 | 15 | 2.05 | 315 | 2.05 | 285 | | | | | 0.65 | | | | | |
| 14 | | Without With | 0.60 | 345 | 0.36 | | 5.78 | 315 | 2.88 | 315 | 2.62 | 300 | 1.96 | 315 | 1:51 | 330 | 7 07 | 220 | 1 70 | 200 | 0.00 | 105 |
| 14 | | Without With | 1.42 | 540 | 3.46 | 60 | 4.19 | 300 | 2.97 | 315 | 3.98 | 285 | 1.54 | 315 | | | 0.87 | | | | | |
| 14 | | Without With | - 1 - | 300 | 3,83 | 45 | 4.33 | 315 | 2.98 | 315 | 3.36 | 285 | 1.35 | 315 | 0.94 | 255 | 0.77 | 300 | 1.49 | 270 | 2.20 | 195 |
| 14 | | Without With | 2.80 | 0 | 1.89 | 60 | 5.18 | 300 | 2.65 | 315 | 3.48 | 285 | 1.53 | 315 | 1.11 | 285 | 1.09 | 300 | 3.50 | alin | 9 08 | 180 |

| Wave Period sec | Wave Height ft | Breakwater Status | ZA Vel | | 2B Vel | Az | 3A Vel | | 3B Vel | | Vel | | Vel 4B | | Vel 5/ | | 5E Vel | | 6A Vel | | 6B Vel | |
|-----------------------|----------------------|----------------------|--------------|------------|--------------|----------|--------------|------------|--------------|------------|--------------|------------|--------------|------------|--------|--------------|------------|------------|--------------|------------|--------------|------------|
| | | | - | | | | Southea | | | | | | | | | - | | | | | | |
| 6 | 2 | Without With | 0.85 | 180 | 0.62 | 90 | 3.48 | 120 135 | 5.63 2.79 | 135 | 2.76 | 120 135 | 3.42 | 150 135 | 1.07 | 165 165 | 1.09 | 135 150 | 0.36 | | 0.54 | 195 |
| 6 | 4 | Without With | 1.19 | 120 45 | 1.26 | 60 75 | | 90 150 | | | | | 3.97 | | | | | | | | 1.23 | |
| 6 | 7 | Without With | 1.97 | 195 | 2.21 | 45 | 1.28 | 15 90 | 3.36 | | | 1 1000 | 1.07 | | | | | | 1.17 | 100000 | 1.70 | |
| 6 | 10 | Without With | 1.80 | | 2.13 | | 2.44 | | | | | | 5.41 3.53 | | | | 1.29 | | 2.18 | | 2.70 | |
| 10 | 4 | Without With | 0.95 | 120 45 | 0.86 | | 2.18 | | | | | | 5.09 5.15 | | | | | | | | 1.10 | |
| 10 | 10 | Without With | 3.12 | 15 15 | 5.45 5.28 | 100 | 1.48 | | 2.91 5.00 | | 2.33 | 135 | 3.99 | | | | | | | | 3.47 2.63 | |
| 10 | 14 | Without With | 3.53 | 330 330 | 3.89 | 45 | 1.75 2.73 | 300 75 | 2.01 | 120 135 | 1.75 | | 4.46 | | 2.68 | | 1.62 | 165 165 | | | 3.68 1.75 | - |
| 10 | 18 | Without With | 3.72 4.16 | 45 60 | 5.77 1.87 | | 2.57 2,16 | | 2.95 5.53 | | | | | | 3.99 | | 2.14 | 165 150 | 5.08 4.34 | 210 210 | 4.16 | |
| 14 | 4 | Without With | 2.10 | 120 60 | 2.98 | 75 45 | 2.65 | 30 90 | 3.83 6.30 | | 0.67 | | 4.88 | | | | 1.49 | | 2.82 | | 3.00 | |
| 14 | 10 | Without With | 1.24 | 30 | 3.90 4.68 | 30.50 | 1.55 | | 2.97 5.20 | | 1.86 | | 4.81 | | | | 1.70 | | 3.68 | | 3.53 3.53 | |
| 14 | 14 | Without With | 2.36 | 0 15 | 5.46 | | 0.68 | | | | 0.68 | | 4.77 | | | | 1.82 | | 4.74 | | | |
| 14 | 18 | Without With | 3.04 | 30 | 4.38 | 60 | 2,00 | 270 | 3.77 | 135 | 0.66 | | 4.13 | 150 165 | 2,87 | 180 180 | 1.86 | 165 165 | 4.08 | 210 210 | 3.98 | 195 195 |
| | | | Vel | Az | Ve. | 4B | Az | | A Az | v | 5B | Az | Vel | A Az | | 6B | Az | Vel | 7A Az | | 7B Vel | Az |
| | | | | | | | East | . Wave | Direc | tion- | -Slac | k Tide | | | | | | | | | | |
| 6 | 2 | Without With | 1.01 | 270 | 0.0 | - | 165 | 0.69 | 300 | | 30 | | 0.50 | | | 0.89 | 165 120 | 0.3 | | | 0.75 | 0 |
| 6 | .4 | Without With | 0.93 | 285 300 | 0. | 55 | 135 | 0.62 | | | .80 | 300 | 1.56 | 31 | 5 (| 0.69 | 30 15 | 0.4 | 3 3 | | 0.26 | 195 |
| 6 | 7 | Without With | 0.61 | 30 60 | | - | 180 330 | 0.43 | | C | .52 | 300 | 1.99 | | | 0.95 | 15 15 | 0.5 | 2 10 | 5 | 1.13 | 165 165 |
| 6 | 10 | Without With | 1.92 | 75 45 | 1. | 42 | 150 300 | 0.43 | 195 | | .80 | 135 | 4.33 | 28 | 5 | 1.13 | 195 195 | 2.0 | | | 1.48 | 180 195 |
| 10 | 4 | Without With | 0.51 | 7.5 60 | 1. | 13 | 105 135 | 0.43 | 300 | 0 | 1.44 | 315 | 0.87 | 18 | 0 | L.09 | 165 15 | 0.6 | 0 4 | 5 | 0.74 | 180 |
| 10 | 10 | Without With | 2.04 | 90 | 1. | 75 | 270 285 | 0.75 | 300 |) (| 1.43 | | 2.62 | 24 | | 2.84 | 195 210 | 2.3 | | 5 | 1,78 | 195 |
| 10 | 14 | Without With | 1.76 | 60 60 | 0. | 92 | 300 | 1.39 | 315 | 1 | .11 | 315 | 2.44 | | | 1.26 | 195 | 2.2 | 7 24 | 0 | 1.21 | 180 |
| 10 | 18 | Without With | 1.91 | 45 | 0.1 | 61 | 165 150 | 0.35 | | | 1.61 | 135 135 | 2.66 | 24 | | 1.65 | 180 180 | 1.3 | | | 1.73 | 195 180 |
| 14 | 4 | Without With | 1.30 | 45 | 1. | 47 | 105 | 0.95 | | |).96).36 | 15 | 3.98 | 27 | 0 | L.13 L.24 | 0 195 | 0.7 | | 5 | 1.21 | 180 180 |
| 14 | 10 | Without With | 2.34 | 45 | 2. | 80 | 165 150 | 0.61 | | 1 | .01 | 330 | 2,25 | 28 | 5 | L.04 L.39 | 180 | 2.5 | 9 21 | 0 | 1.99 | 195 210 |
| 14 | 14 | Without With | 1.09 | 60 | 0. | 61 | 195 | 1.24 | 315 | 1 | .07 | 315 | 3.06 | 28 | 5 | 2.64 | 180 180 | 1.3 | 9 19 | 5 | 1.51 | 165 180 |
| 14 | 18 | Without With | 1.79 | 75 90 | 1. | 14 | 240 285 | 1.12 | 315 | C |).35).35 | | 2.86 | 25 | 5 (| 3.18 | 180 180 | 1.5 | 0 16 | 5 | 2.42 | 195 210 |
| | | | | | | | Ea | st Wa | ve Dir | ectio | nEbb | Tide | | | | | | | | | | |
| 6 | 2 | Without With | 1.28 | 135 120 | | | 135 135 | 1.82 | | | .91 | 135 150 | 0.94 | | | 0.68 | 180 | 0.9 | 1 24 | Ó | 0.73 | 195 195 |
| 6 | 4 | Without With | 1.69 3.09 | 135 120 | 1000 | | 135 135 | 1.64 | | | .52 | 150 150 | 2.26 | | | 0.96 L.21 | 15 0 | 0.79 | 2 27 | Q | 0.90 | 180 210 |
| 6 | 7 | Without With | 1.65 | 150 105 | | | 150 150 | 1.77 | | | .16 | 165 165 | 2.17 | | | 0.52 | 15 | 0.9 | | | 2.81 | 180 195 |
| 6 | 10 | Without With | 2.85 | 105 | 100 | | 150 150 | 1.54 | | | .13 | 135 135 | 3.27 4.08 | | | 0.97 | 195 195 | 2.42 | | | 2.03 | 195 210 |
| 10 | 4 | Without With | 3.78 2.61 | 105 | | 00 19 | 135 135 | 2.13 | 150 |)] | .31 | 150 135 | 2.07 | | | 2.69 | 180 210 | 0.9 | | | 1.64 | 195 195 |
| | | | | | | | | | (Cont | inued | 1) | | | | | | | | | She | et 3 p | f 4) |

| Wave | Wave Height | Breakwater | 4A | 1 | 4B | | 5A | - | 5B | | 6A | | бв | | 7A | | 78 | |
|------|----------------|-----------------|--------------|------------|--------------|------------|--------------|------------|---------|-------------|--------------|------------|--------------|------------|--------------|------------|------|----|
| sec | _ft_ | Status | <u>Vel</u> | Az | Vel | Az | Vel | Az | Vel | Az | Vel | Az | Vel | Az | Vel | Az | Vel | Az |
| | | | | | | East We | ve Dire | ction- | Ebb Tid | (Cont | inued) | | | | | | | |
| 70 | 10 | Without With | 2.20 | 90 90 | 3.65 | 150 135 | 1.42 | 180 150 | 1.08 | 135 | 2.92 | 225 225 | 1.25 | 180 195 | 2.71 | 225 | 2.26 | 21 |
| 10 | 14 | Without With | 3.05 | 90 90 | 4.15 | 150 150 | 1.59 | 180 180 | 1.01 | 150 135 | 2.42 | 240 240 | 1.67 | 180 195 | 2.90 3.47 | 225 | 2.60 | 21 |
| 10 | 18 | Without With | 1.61 | 90 105 | 3.62 | 150 150 | 1.62 | 180 | 1.16 | 150 150 | 5.13 | 255 270 | 2.30 | 195 195 | 2.57 | 225 | 2.57 | 2 |
| 14 | 4 | Without With | 1.75 | 105 120 | 4.35 | 135 150 | 1.42 | 180 | 1.48 | 150 150 | 3.94 | 270 240 | 1.32 | 210 210 | 1.13 | 225 | 2.28 | 2 |
| 14 | 10 | Without With | 3.32 | 105 90 | 4.03 | 150 150 | 1.25 | 180 | 0.93 | 135 150 | 3.08 | 225 225 | 0.84 | 180 195 | 2.95 | 210 | 2.37 | 2 |
| 14 | 14 | Without With | 2.21 | 75 90 | 4.14 | 150 150 | 1.76 | 150 150 | 1.03 | 135 | 2.94 | 240 | 2.12 | 195 195 | 2.12 | 210 225 | 2.23 | 5 |
| 14 | 1.8 | Without With | 1.72 | 90 135 | 4.33 5.05 | 150 135 | 1.75 | 180 | 1.21 | 150 | 3.79 | 225 | 2.20 | 195 195 | 2.35 | 210 | 2.24 | 2 |
| | | | | | | Ea | st Wave | Direct | ionFlo | od Tid | e | | | | | | | |
| 6 | 2 | Without With | 4.07 | 285 285 | 3.55 | 315 315 | 2.42 | 315 315 | 2.42 | 315 315 | 2.25 | 345 345 | 2.60 | 15 15 | 1.04 | 30 | 0.69 | 7 |
| 6 | 4 | Without With | 2.77 | 285 285 | 2.77 | 315 315 | 1.91 | 315 315 | 2.08 | 315 315 | 1.73 | 330 330 | 1.73 | 15 15 | 0.61 | 15 15 | 0.52 | |
| 6 | 7 | Without With | 2.68 3.12 | 315 285 | 2.17 | 270 315 | 2.34 | 315 315 | 1.47 | 315 315 | 2.42 | 300 330 | 1.56 | 15 15 | 0.52 | 45 60 | 0.52 | 10 |
| 6 | 10 | Without With | 2.42 | 300 300 | 1.82 3.12 | 300 315 | 2.08 | 330 330 | 2.08 | 315 315 | 1.91 2.51 | 300 300 | 1.65 | 15 15 | 0.52 | 240 | 0.61 | 1 |
| 10 | 14 | Without With | 3.38 | 285 285 | 2.77 | 315 315 | 1.99 | 315 315 | 2.51 | 315 315 | 2.17 | 345 330 | 2.42 | 15 15 | 0.87 | 15 15 | 0.43 | |
| 10 | 10 | Without With | 2.77 | 315 300 | 3.12 | 300 315 | 1.91 2.17 | 330 315 | 2.51 | 315 330 | 3.38 | 300 300 | 1.82 | 15 15 | 1.13 | 225 240 | 1.04 | 18 |
| 10 | 14 | Without With | 1.39 | 345 330 | 2.25 | 315 315 | 2.08 | 315 330 | 2.08 | 315 315 | 2.68 | 270 270 | 0.69 | 195 | 1.47 | 270 | 1.65 | 13 |
| 10 | 18 | Without With | 1.73 | 330 315 | 2.08 | 330 315 | 1.82 | 315 330 | 1.56 | 330 330 | 2.42 | 285 | 1.04 | 15 | 1.65 2.08 | 180 225 | 1.56 | 19 |
| 14 | 4 | Without With | 2.17 | 285 300 | 2.34 | 315 315 | 1.82 | 315 315 | 1.47 | 330 315 | 2.08 | 300 | 3.64 2.51 | 0 | 0.52 | | 0.87 | 15 |
| 14 | 10 | Without With | 1.65 | 345 345 | 2.17 | 315 330 | 2.60 | 330 330 | 2.34 | 330 330 | 2.25 | 300 315 | 1.04 | 180 180 | 1.39 | 195 180 | 1.65 | 19 |
| 14 | 14 | With | 1.82 | 330 330 | 2.17 | 315 315 | 2.17 | 315 315 | 1.91 | 31.5 330 | 2.51 | 300 270 | 0.61 | 195 210 | 1.21 | 180 210 | 1.56 | 19 |
| 14 | 18 | Without With | 1.21 | 360 45 | 2.08 | 315 315 | 1.91 | 330 330 | 1.65 | 330 330 | 3.03 | 300 270 | 1.13 | 195 180 | 1.04 | 195 210 | 2.08 | 19 |

Table 6

Average Current Velocities Within a Wave Period, Test Series I

| 20000 | | Breakwater Out | | Breakwater In | | | 5 |
|-------------------------|--------------|----------------------|-------------|----------------------|----------|--------------------------|------------------|
| Tidal Condi- tion | Sta- tion | Veloc- ity fps | Azimuth* | Veloc- ity fps | Azimuth* | Δ Veloc- ity** fps | Δ Veloc- ity; |
| | | Sout | h Wave Dire | ection, 6 | Sec Wave | Period | |
| Slack | 1A | 0.36 | †† | 0.46 | †† | +0.10 | +28 |
| | 1B | 0.51 | 130 | 0.53 | 130 | +0.02 | +4 |
| | 2A | 0.51 | 113 | 0.82 | 105 | +0.31 | +61 |
| | 2B | 1.05 | 79 | 1.16 | 71 | +0.11 | +10 |
| | 3A | 1.56 | 315 | 1.83 | 315 | +0.27 | +17 |
| | 3B | 0.79 | 15 | 0.90 | 15 | +0.11 | +14 |
| | 4A | 0.78 | 30 | 0.82 | 38 | +0.04 | +5 |
| | 4B | 0.70 | 75 | 0.87 | 90 | +0.17 | +24 |
| Flood | 1A | 0.61 | 205 | 0.57 | 210 | -0.04 | -7 |
| | 1B | 1.19 | 200 | 1.35 | 205 | +0.16 | +13 |
| | 2A | 1.28 | 255 | 1.30 | 250 | +0.02 | +2 |
| | 2B | 2.06 | 240 | 1.85 | 240 | -0.21 | -10 |
| | 3A | 4.34 | 320 | 4.68 | 320 | +0.34 | +8 |
| | 3B | 3.10 | 325 | 2.95 | 330 | -0.15 | -5 |
| | 4A | 3.09 | 285 | 2.86 | 289 | -0.23 | -7 |
| | 4B | 2.62 | 315 | 3.00 | 315 | +0.38 | +15 |
| Ebb | 1A | 0.72 | †† | 0.95 | †† | +0.23 | +32 |
| | 1B | 0.77 | 184 | 1.09 | 180 | +0.32 | +42 |
| | 2A | 0.98 | 110 | 0.84 | 105 | -0.14 | -14 |
| | 2B | 0.96 | 240 | 0.82 | 255 | -0.14 | -15 |
| | 3A | 1.90 | 68 | 2.16 | 56 | +0.26 | +14 |
| | 3B | 1.96 | 158 | 2.11 | 143 | +0.15 | +8 |
| | 4A | 2.76 | 109 | 2.52 | 109 | -0.24 | -9 |
| | 4B | 4.05 | 124 | 3.48 | 131 | -0.57 | -14 |

(Continued)

Note: Station locations given in Plate 2, velocities and azimuths are average values obtained from all test waves within the designated wave periods.

^{*} Azimuth is measured clockwise from New Jersey grid north.

^{**} A velocity (fps) = velocity - velocity out .

[†] Δ velocity (%) = (velocity - velocity out /velocity out) (100).

⁺⁺ No predominant direction can be defined. (Sheet 1 of 8)

| | | Breakt | vater Out | Breakw | rater In | | |
|-------------------------|--|--|--|--|--|--|--|
| Tidal Condi- tion | Sta- tion | Veloc- ity fps | Azimuth deg | Veloc- ity fps | Azimuth deg | Δ Veloc- ity fps | Δ Veloc- ity ——————————————————————————————————— |
| | | Sout | h Wave Dire | ection, 1 | O-Sec Wave | Period | |
| Slack | 1A 1B 2A 2B 3A 3B 4A 4B | 1.25 1.20 2.16 1.72 1.65 0.61 0.84 0.73 | 11 86 8 60 315 330 34 98 | 1.41 1.05 1.91 1.97 2.26 0.76 0.79 0.80 | †† 71 345 55 330 330 41 94 | +0.16 -0.15 -0.25 +0.25 +0.61 +0.15 -0.05 +0.07 | +13 -13 -12 +15 +37 +25 -6 +10 |
| Flood | 1A 1B 2A 2B 3A 3B 4A 4B | 1.19 1.12 1.82 2.09 3.97 2.38 2.11 2.40 | 180 180 285 240 319 320 281 311 | 1.36 0.99 1.46 1.99 3.92 2.12 1.98 2.44 | 203 173 275 240 323 325 281 315 | +0.17 -0.13 -0.36 -0.10 -0.05 -0.26 -0.13 +0.04 | +14 -12 -20 -5 -1 -11 -6 +2 |
| Ebb | 1A 1B 2A 2B 3A 3B 4A 4B | Lost 1.01 3.55 1.94 1.91 2.41 2.55 3.45 | Lost 98 45 94 †† 175 109 139 | Lost 0.97 2.50 1.52 1.37 2.41 2.40 3.40 | Lost 98 60 83 ++ 160 131 139 | -0.04 -1.05 -0.42 -0.54 0 -0.15 -0.05 | -4 -30 -22 -28 -0 -6 -1 |
| | | Sout | h Wave Dir | ection, 1 | 4-Sec Wave | Period | |
| Slack | 1A 1B 2A 2B 3A 3B 4A 4B | 1.34 1.38 0.77 1.83 1.94 0.85 0.79 1.02 | 60 55 30 64 290 340 30 110 | 1.53 1.34 1.38 1.88 2.02 0.88 0.83 0.89 | 75 55 8 56 353 10 26 115 | +0.19 -0.04 +0.61 +0.05 +0.08 +0.03 +0.04 -0.13 | +14 -3 +79 +3 +4 +4 +5 |

(Continued)

tt No predominant direction can be defined.

| | | Breakw | ater Out | Breakt | water In | | |
|----------------|--------------|------------|-------------|-------------|----------------|----------------|------------|
| Tidal | C+ - | Veloc- | 1 | Veloc- | A - 5 + 3- | Δ Veloc- | Δ Veloc- |
| Condi- tion | Sta- tion | ity fps | Azimuth deg | ity fps | Azimuth deg | ity fps | ity % |
| <u> </u> | | - | | | | | |
| | Sou | 74 1300 | 450 | 1000 | 200 | d (Continued | <u>1)</u> |
| Flood | lA | 1.22 | 60 | 1.18 | 175 | -0.04 | -3 |
| | 1B | 1.06 | 101 | 1.10 | 112 214 | +0.04 | +4 |
| | 2A 2B | 1.27 | 229 240 | 1.11 | 240 | +0.22 | -13 +13 |
| | 3A | 4.97 | 326 | 4.24 | 330 | -0.73 | -15 |
| | 3B | 2.52 | 323 | 2.64 | 323 | +0.12 | +5 |
| | 4A | 2.51 | 293 | 2.89 | 293 | +0.38 | +15 |
| | 4B | 2.59 | 311 | 2.19 | 315 | -0.40 | -15 |
| Ebb | lA | Lost | Lost | Lost | Lost | | |
| | 1B | 2.30 | 79 | 1.20 | 113 | -1.10 | -48 |
| | 2A | 2.16 | 53 | 2.17 | 86 | +0.01 | 0 |
| | 2B | 2.02 | 75 | 1.58 | 94 | -0.44 | -22 |
| | 3A | 2.20 | 172 | 2.56 | ++ | +0.36 +0.16 | +16 +11 |
| | 3B 4A | 1.43 | 173 105 | 1.59 | †† 116 | -1.42 | <u>-44</u> |
| | 4B | 3.80 | 135 | 3.14 | 135 | -0.66 | -17 |
| | 72 | | ast Wave D | - | | | |
| | | | 4.000 | 11 60 01011 | | | |
| Slack | 2A | 0.87 | 218 | 0.92 | 225 | +0.05 | +6 |
| | 2B | 1.65 | 60 | 1.93 | 70 | +0.28 | +16 |
| | 3A | 2.40 | 295 | 2.57 | 275 | +0.17 | +7 |
| | 3B | 0.92 | 295 | 1.05 | 280 | +0.13 | +14 +14 |
| | 4A | 0.94 | 68 | 1.07 | 75 315 | -0.22 | -18 |
| | 4B | 0.51 | 315 180 | 0.46 | 158 | -0.05 | -10 |
| | 5A 5B | 0.43 | 150 | 0.46 | 143 | +0.03 | +7 |
| | 6A | 2.43 | 285 | 2.80 | 280 | +0.37 | +15 |
| | 6B | 1.30 | 185 | 1.91 | 185 | +0.61 | +47 |
| Flood | 2A | 1.33 | 236 | 1.46 | 236 | +0.13 | +9 |
| | 2B | 1.81 | ++ | 1.82 | ++ | +0.01 | +1 |
| | 3A | 3.70 | 296 | 3.85 | 293 | +0.15 | +4 |
| | 3B | 2.50 | 311 | 2.79 | 307 | +0.29 | +12 |
| | 4A | 1.77 | 296 | 1.68 | 300 | -0.09 | - 5 |
| | 4B | 2.15 | 311 | 1.96 | 315 | -0.19 -0.16 | -9 -10 |
| | 5A | 1.58 | 325 | 1.42 | 325 315 | +0.06 | +4 |
| | 5B | 1.50 | 315 | 1.56 | 320 | +0.03 | +2 |
| | 6A 6B | 1.82 | 325 †† | 1.07 | ++ | -0.06 | -5 |
| | 72 | -1-3 | | | | | |
| | | | | (Continu | ed) | | |

⁺⁺ No predominant direction can be defined.

| | | Breakwa | ater Out | Break | water In | | 2 12 2 |
|-------------------------|--|--|--|--|--|--|---|
| Tidal Condi- tion | Sta- tion | Veloc- ity fps | Azimuth deg | Veloc- ity fps | Azimuth deg | Δ Veloc- ity fps | Δ Veloc- ity ——————————————————————————————————— |
| | Southe | east Wave | Direction | , 6-Sec | Wave Period | (Continued | 1) |
| Ebb | 2A 2B 3A 3B 4A 4B 5A 5B 6A 6B | 1.20 1.56 2.21 4.42 1.90 3.47 1.25 1.17 1.13 | †† 60 116 139 109 143 158 143 235 191 | 0.60 1.70 2.66 3.98 2.37 3.62 1.33 0.99 1.66 1.30 | †† 68 120 135 124 135 165 143 255 200 | -0.60 +0.14 +0.45 -0.44 +0.47 +0.15 +0.08 -0.18 +0.53 -0.24 | -50 +9 +20 -10 +25 +4 +6 -15 +47 -16 |
| | | Southeast | Wave Dire | ection, | 10-Sec Wav | e Period | |
| Slack | 2A 2B 3A 3B 4A 4B 5A 5B 6A 6B | 2.74 2.21 2.96 0.61 0.87 0.98 1.16 0.93 2.69 1.84 | 355 64 278 11 †† 130 180 146 259 180 | 2.83 2.54 2.51 0.59 0.75 1.25 1.04 0.82 2.82 2.23 | 350 64 270 25 305 124 185 155 259 195 | +0.09 +0.33 -0.45 -0.02 -0.12 +0.27 -0.12 -0.11 +0.13 +0.39 | +3 +15 -15 -3 -14 +28 -10 -12 +5 +21 |
| Flood | 2A 2B 3A 3B 4A 4B 5A 5B 6A 6B | 2.31 2.31 3.19 2.49 1.92 2.09 1.46 1.30 1.75 2.23 | †† 50 310 315 290 315 308 305 248 195 | 2.65 2.00 2.89 2.72 2.11 2.15 1.51 1.52 2.50 2.26 | †† 60 295 311 290 315 310 315 265 195 | +0.34 -0.31 -0.30 +0.23 +0.19 +0.06 +0.05 +0.22 +0.75 +0.03 | +15 -13 -9 +9 +10 +3 +17 +43 +1 |

(Continued)

| | | Breakwa | ater Out | Breakw | ater In | | |
|--------|-------|-----------|------------|-----------|-----------|--------------|-----------|
| Tidal | | Veloc- | | Veloc- | | Δ Veloc- | Δ Veloc- |
| Condi- | Sta- | ity | Azimuth | ity | Azimuth | ity | ity |
| tion_ | tion | fps_ | deg | _fps | deg | fps | |
| | South | east Wave | Direction | , 10-Sec | Wave Peri | od (Continue | <u>d)</u> |
| Ebb | 2A | 3.46 | ++ | 3.02 | ++ | -0.44 | -13 |
| | 2B | 3.33 | 56 | 3.07 | 55 | -0.26 | -8 |
| | 3A | 2.08 | 45 | 2.25 | 150 | +0.17 | +8 |
| | 3B | 2.72 | 131 | 4.92 | 135 | +2.20 | +81 |
| | 4A | 1.29 | 158 | 2.67 | 131 | +1.38 | +107 |
| | 4B | 4.37 | 154 | 4.78 | 146 | +0.41 | +9 |
| | 5A | 2.61 | 173 | 1.50 | 173 | -1.11 | -42 |
| | 5B | 1.60 | 158 | 1.26 | 158 | -0.34 | -21 |
| | 6A | 4.31 | 225 | 4.24 | 225 | -0.07 | -2 |
| | 6в | 3.10 | 195 | 2.09 | 195 | -1.01 | -32 |
| | | Southeast | t Wave Dir | ection, 1 | 4-Sec Wav | e Period | |
| Slack | 2A | 1.52 | 28 | 1.75 | 15 | +0.23 | +15 |
| | 2B | 3.88 | 60 | 3.20 | 64 | -0.68 | -18 |
| | 3A | 2.63 | 290 | 2.95 | 290 | +0.32 | +12 |
| | 3B | 1.17 | 353 | 1.19 | 356 | +0.02 | +2 |
| | 4A | 1.21 | ++ | 1.33 | 281 | +0.12 | +10 |
| | 4B | 1.13 | 169 | 1.07 | 143 | -0.06 | -5 |
| | 5A | 1.34 | 185 | 1.11 | 184 | -0.23 | -17 |
| | 5B | 1.19 | 158 | 1.02 | 154 | -0.17 | -14 |
| | 6A | 3.29 | 251 | 2.88 | 255 | -0.41 | -12 |
| | 6в | 2.99 | 195 | 2.45 | 195 | -0.54 | -18 |
| Flood | 2A | 2.21 | ++ | 2.73 | ++ | +0.52 | +24 |
| | 2B | 3.06 | 55 | 3.08 | 55 | +0.02 | +1 |
| | 3A | 4.87 | 308 | 4.53 | 304 | -0.34 | -7 |
| | 3B | 2.87 | 315 | 2.89 | 315 | +0.02 | +1 |
| | 4A | 3.36 | 289 | 3.24 | 289 | -0.12 | -4 |
| | 4B | 1.60 | 315 | 1.56 | 315 | -0.04 | -3 |
| | 5A | 1.19 | 290 | 1.19 | 300 | 0 | 0 |
| | 5B | 0.96 | 310 | 0.93 | 310 | -0.03 | 0 -3 |
| | 6A | 2.23 | 270 | 2.79 | 280 | +0.56 | +25 |
| | 6в | 1.80 | 190 | 1.83 | 195 | +0.03 | +2 |

(Continued)

| | | Breakw | ater Out | Breakw | rater In | | |
|--------|---------|----------|------------|-----------|------------|--------------------------|--------|
| Tidal | | Veloc- | | Veloc- | | Δ Veloc- Δ | Veloc- |
| Condi- | Sta- | ity | Azimuth | ity | Azimuth | ity | ity |
| tion | tion | fps | deg | _fps_ | deg | fps _ | % |
| | Souther | ast Wave | Direction | , 14-Sec | Wave Perio | d (Continued) | |
| Ebb | 2A | 1.90 | 15 | 1.96 | 35 | +0.06 | +3 |
| | 2B | 4.11 | 60 | 3.62 | 50 | -0.49 | -12 |
| | 3A | 1.63 | 38 | 1.61 | 68 | -0.02 | -1 |
| | 3B | 3.67 | 130 | 5.31 | 125 | +1.64 | +44 |
| | 4A | 1.06 | ++ | 1.21 | ++ | +0.15 | +14 |
| | 4B | 4.65 | 169 | 4.62 | 161 | -0.03 | -1 |
| | 5A | 2.63 | 173 | 2.02 | 173 | -0.61 | -23 |
| | 5B | 1.72 | 158 | 1.37 | 158 | -0.35 | -20 |
| | 6A | 3.83 | 220 | 3.48 | 221 | -0.35 | -9 |
| | 6в | 3.48 | 195 | 3.11 | 195 | -0.37 | -11 |
| | | East 1 | Wave Direc | tion, 6-S | ec Wave Pe | eriod | |
| Slack | 4A | 1.15 | ++ | 1.12 | ++ | -0.03 | -3 |
| | 4B | 0.97 | 158 | 0.99 | ++ | +0.02 | +2 |
| | 5A | 0.49 | 263 | 0.45 | 248 | -0.04 | -8 |
| | 5B | 0.71 | ++ | 0.66 | ++ | -0.05 | -7 |
| | 6A | 2.63 | 290 | 2.74 | 290 | +0.11 | +4 |
| | 6В | 0.95 | ++ | 0.95 | ++ | 0 | 0 |
| | 7A | 1.01 | ++ | 1.10 | ++ | +0.09 | +9 |
| | 7B | 1.30 | 173 | 0.90 | 184 | -0.40 | -31 |
| rlood | 4A | 2.79 | 296 | 3.00 | 289 | +0.21 | +8 |
| | 4B | 2.71 | 310 | 3.09 | 315 | +0.38 | +14 |
| | 5A | 2.08 | 319 | 2.19 | 319 | +0.11 | +5 |
| | 5B | 1.91 | 315 | 2.06 | 315 | +0.15 | +8 |
| | 6A | 2.08 | 319 | 2.06 | 326 | -0.02 | -1 |
| | 6В | 1.89 | 15 | 2.19 | 15 | +0.30 | +16 |
| | 7A | 0.72 | 30 | 0.63 | 25 | -0.09 | -13 |
| | 7B | 0.59 | 120 | 0.57 | 128 | -0.02 | -3 |
| Ebb | 4A | 1.94 | 125 | 2.85 | 115 | +0.91 | +47 |
| | 4B | 3.55 | 143 | 5.49 | 143 | +1.94 | +55 |
| | 5A | 1.54 | 161 | 1.71 | 161 | +0.17 | +11 |
| | 5B | 1.11 | 146 | 1.40 | 150 | +0.29 | +26 |
| | 6A | 2.57 | 255 | 2.77 | 265 | +0.20 | +8 |
| | 6B | 0.78 | ++ | 0.85 | †† | +0.07 | +9 |
| | 7A | 1.29 | 240 | 1.32 | 244 | +0.03 | +2 |
| | 7B | 1.65 | 188 | 1.81 | 203 | +0.16 | +10 |
| | | | ((| Continued |) | | |

tt No predominant direction can be defined.

Table 6 (Continued)

| | | Breakw | ater Out | Breakw | ater In | | |
|-------------------------|--------------|----------------------|----------------|----------------------|----------------|------------------------|----------------------|
| Tidal Condi- tion | Sta- tion | Veloc- ity fps | Azimuth deg | Veloc- ity fps | Azimuth deg | Δ Veloc- ity fps | Δ Veloc- ity % |
| | | East | Wave Direc | tion, 10- | Sec Wave | Period | |
| Slack | 4A | 1.56 | 68 | 1.70 | 60 | +0.14 | +9 |
| | 4B | 1.10 | ++ | 1.00 | ++ | -0.10 | -9 |
| | 5A | 0.73 | 305 | 0.74 | 290 | +0.01 | +1 |
| | 5B | 0.49 | ++ | 0.57 | ++ | +0.08 | +16 |
| | 6A | 2.15 | 233 | 2.44 | 248 | +0.29 | +13 |
| | 6B | 1.71 | 184 | 1.42 | 200 | -0.29 | -17 |
| | 7A | 1.00 | ++ | 0.92 | ++ | -0.08 | -8 |
| | 7B | 1.37 | 188 | 1.39 | 180 | +0.02 | +2 |
| Flood | 4A | 2.25 | 319 | 2.32 | 308 | +0.07 | +3 |
| | 4B | 2.56 | 315 | 2.48 | 315 | -0.08 | -3 |
| | 5A | 1.89 | 319 | 2.08 | 323 | +0.19 | +10 |
| | 5B | 2.17 | 319 | 1.97 | 323 | -0.20 | -9 |
| | 6A | 2.13 | 300 | 2.53 | 293 | +0.40 | +19 |
| | 6B | 1.76 | 15 | 1.58 | 10 | -0.18 | -10 |
| | 7A | 1.28 | †† | 1.37 | †† | +0.09 | +7 |
| | 7B | 1.17 | 190 | 1.08 | 200 | -0.09 | -8 |
| Ebb | 4A | 2.33 | 94 | 2.43 | 101 | +0.10 | +4 |
| | 4B | 4.36 | 146 | 4.25 | 143 | -0.11 | -3 |
| | 5A | 1.69 | 180 | 1.67 | 165 | -0.02 | -1 |
| | 5B | 1.14 | 146 | 1.30 | 135 | +0.16 | +14 |
| | 6A | 3.14 | 229 | 2.56 | 233 | -0.58 | -18 |
| | 6B | 1.98 | 184 | 1.66 | 199 | -0.32 | -16 |
| | 7A | 2.28 | 225 | 2.09 | 229 | -0.19 | -8 |
| | 7B | 2.27 | 206 | 2.10 | 206 | -0.17 | -7 |
| | | East | Wave Dire | ction, 14 | -Sec Wave | Period | |
| Slack | 4A | 1.63 | 56 | 1.94 | 71 | +0.31 | +19 |
| | 4B | 1.33 | ++ | 1.37 | ++ | +0.04 | +3 |
| | 5A | 1.10 | 310 | 0.75 | 225 | -0.35 | -32 |
| | 5B | 0.85 | 340 | 0.45 | ++ | -0.40 | -47 |
| | 6A | 3.04 | 274 | 2.46 | 255 | -0.58 | -19 |
| | 6B | 0.95 | 180 | 2.11 | 184 | +1.16 | +122 |
| | 7A | 1.57 | 191 | 1.91 | 191 | +0.34 | +22 |
| | 7B | 1.78 | 184 | 1.99 | 195 | +0.21 | +12 |

Table 6 (Concluded)

| | | Break | water Out | Breakw | ater In | | |
|-------------------------|--|--|---|--|--|--|---|
| Tidal Condi- tion | Sta- tion | Veloc- ity fps | Azimuth deg | Veloc- ity fps | Azimuth deg | Δ Veloc- Δ ity fps (Continued) | Veloc- ity % |
| Flood | 4A 4B 5A 5B 6A 6B 7A 7B | 1.71 1.91 2.17 1.89 2.47 0.93 1.04 1.65 | 330 315 323 326 300 190 190 | 1.71 2.02 1.78 1.78 2.34 1.01 1.17 1.68 | 345 319 323 326 289 190 200 210 | 0 +0.11 -0.39 -0.11 -0.13 +0.08 +0.13 +0.03 | 0 +6 -18 -5 -5 +9 +13 +2 |
| Ebb | 4A 4B 5A 5B 6A 6B 7A 7B | 1.92 4.21 1.55 1.09 3.44 1.62 2.14 2.28 | 94 146 173 143 236 195 214 210 | 2.25 4.53 1.65 1.31 3.08 1.42 2.90 2.18 | 109 146 161 150 229 199 229 210 | +0.33 +0.32 +0.10 +0.22 -0.36 -0.20 +0.76 -0.10 | +17 +8 +6 +20 -10 -12 +36 -4 |

Table 7

Breaking Wave Data for South Zone, Northeast Wave Direction--Slack Tide

| Test | Wave | | | Brea | king Chars | cteristic | S | |
|--------|--------|-----------------|---------------------|---------|--|--------------|----------|----------------|
| Period | Height | Breakwater | Coordina | | Height | Depth | Angle | Transport |
| sec | _ft_ | Status | E, ft | N, ft | _ft_ | _ft_ | deg | Direction |
| 6 | 4 | Without | 2,102,150 | 235,000 | 3.75 | 8.00 | 32 | South |
| | | With | 2,102,150 | 235,000 | 3.73 | 8.00 | 33 | South |
| | | Without | 2,105,865 | 234,000 | 2.17 | 8.00 | 32 | South |
| | | With | 2,105,865 | 234,000 | 2.15 | 8.00 | 34 | South |
| | | Without | 2,103,060 | 233,000 | 3.97 | 7.50 | 33 | South |
| | | With | 2,103,060 | 233,000 | 4.38 | 7.50 | 31 | South |
| 6 | 7 | Without | 2,108,000 | 235,000 | 5.56 | 12.50 | 41 | South |
| - | | With | 2,108,000 | 235,000 | 6.23 | 12.50 | 39 | South |
| | | Without | 2,108,000 | 234,000 | 6.63 | 13.00 | 41 | South |
| | | With | 2,108,000 | 234,000 | 6.37 | 13.00 | 39 | South |
| | | Without | 2,107,375 | 233,000 | 6.19 | 13.00 | 35 | South |
| | | With | | 233,000 | 6.23 | 13.00 | 36 | South |
| | | | 2,107,375 | | 3.24 | 7.00 | 33 | South |
| | | Without With | 2,103,000 | 232,000 | 3.68 | 7.00 | 32 | South |
| 6 | 10 | Without | 2,109,000 | 235,000 | 8.00 | 19.00 | 43 | South |
| 0 | 10 | With | 2,109,000 | 235,000 | 8.44 | 19.00 | 43 | South |
| | | | 2,108,300 | 234,000 | 10.26 | 16.00 | 43 | South |
| | | Without With | 2,108,300 | 234,000 | 10.41 | 16.00 | 42 | South |
| | | | | | 10.95 | 16.50 | 36 | South |
| | | Without | 2,108,000 | 233,000 | 11.10 | | 34 | South |
| | | With | 2,108,000 | 233,000 | THE RESERVE OF THE PARTY OF THE | 16.50 | | |
| | | Without With | 2,108,000 | 232,000 | 10.18 9.86 | 17.00 | 36 34 | South South |
| 40 | -15 | | | | | 8.50 | 33 | South |
| 10 | 4 | Without | 2,102,120 | 235,000 | 5.17 4.75 | 8.50 | 33 | South |
| | | With | 2,102,120 | 235,000 | 100000000000000000000000000000000000000 | 7.00 | 33 | South |
| | | Without | 2,101,835 | 234,000 | 4.59 | 7.00 | 38 | South |
| | | With | 2,101,835 | 234,000 | 4.15 | 200 | 28 | South |
| | | Without | 2,103,105 | 233,000 | 5.15 | 7.50 | 28 | South |
| | | With | 2,103,105 | 233,000 | 5.45 | 7.50 | 28 | South |
| | | Without With | 2,102,850 2,102,850 | 232,000 | 4.14 3.82 | 5.50 5.50 | 28 | South |
| 00 | | | | | 11.71 | 21.00 | 40 | South |
| 10 | 10 | Without | 2,109,595 | 235,000 | 12.00 | 21.00 | 42 | South |
| | | With | 2,109,595 | 235,000 | | 21.00 | 40 | South |
| | | Without | 2,109,595 | 234,000 | 11.01 | | 42 | South |
| | | With | 2,109,595 | 234,000 | 10.56 | 21.00 | 34 | South |
| | | Without | 2,109,000 | 233,000 | 11.82 | 20.50 | 34 | South |
| | | With | 2,108,700 | 233,000 | 12.00 | Section 1 | 34 | South |
| | | Without With | 2,108,775 | 232,000 | 10.72 | 20.50 | 34 | South |
| -1 | v. | | | 235,000 | 8.77 | 11.00 | 28 | South |
| 14 | 4 | Without | 2,107,700 | | 7.83 | 11.00 | 28 | South |
| | | With | 2,107,700 | 235,000 | 8.46 | 10.50 | 28 | South |
| | | Without | 2,107,700 | | 8.93 | 10.50 | 28 | South |
| | | With | 2,107,700 | 234,000 | Annual Control | 12.50 | 28 | South |
| | | Without | 2,107,700 | 233,000 | 7.07 | | 27 | South |
| | | With | 2,107,700 | 233,000 | 6.55 | 12.50 | 23 | South |
| | | Without | 2,103,300 | 232,000 | 6.19 | 10.00 | 21 | South |
| - | 2.0 | With | | 343 444 | 14.12 | 22.50 | 36 | South |
| 14 | 10 | Without | 2,110,000 | 235,000 | 14.12 | 22.50 | 36 | South |
| | | With | 2,110,000 | | 14.51 | 16.00 | 36 | South |
| | | Without | 2,108,255 | 234,000 | | 16.00 | 36 | South |
| | | With | 2,108,255 | 234,000 | 14.22 | 18.00 | 35 | South |
| | | Without | 2,108,150 | 233,000 | 14.29 | 17.00 | 36 | South |
| | | With | 2,108,000 | 233,000 | 14.57 | | 35 | South |
| | | Without | 2,108,225 | 232,000 | 13.25 | 17.50 | 36 | South |
| | | With | 2,108,225 | 232,000 | 13.86 | 17.50 | 30 | Double |

Note: Zones and baselines for angles are defined in Plate 3; without means breakwater is not installed, with means breakwater is installed.

^{*} Coordinates are referred to New Jersey grid system.

Table 8 Breaking Wave Data for South Zone, E22.5°N Wave Direction -- Slack Tide

| Test | | The second second | | | aking Chara | | | |
|---------------|----------|--|--|--|---|--|--|---|
| Period sec | Heightft | Breakwater Status | E, ft | N, ft | Height ft | Depthft | Angle deg_ | Direction |
| 6 | 4 | Without With Without With | 2,105,150 2,105,360 2,102,501 2,102,060 | 234,000 234,000 233,000 233,000 | 3.51 2.47 2.46 2.94 | 8.00 7.50 5.00 4.50 | 17 17 18 17 | South South South |
| 6 | 7 | Without With Without With Without With Without With Without With | 2,107,501 2,107,501 2,107,501 2,107,501 2,103,240 2,103,000 2,103,000 2,103,000 | 235,000 235,000 234,000 234,000 233,000 233,000 232,000 232,000 | 5.61 5.45 6.42 5.21 6.31 4.06 5.22 3.96 | 9.50 9.50 9.50 9.50 7.50 7.00 6.50 | 18 18 18 18 11 12 12 | South South South South South South South |
| 6 | 10 | Without With Without With Without With Without With Without With | 2,108,000 2,107,850 2,107,850 2,107,850 2,107,300 2,107,300 2,107,000 2,103,000 | 235,000 235,000 234,000 234,000 233,000 233,000 232,000 232,000 | 7.36 8.28 6.23 8.69 8.20 8.81 8.65 5.19 | 12.50 11.50 11.50 12.00 12.00 15.00 6.50 | 18 18 18 18 18 18 18 | South South South South South South South |
| 10 | 4 | Without With Without With Without With | 2,102,240 2,102,240 2,102,300 2,102,300 2,102,150 2,102,700 | 234,000 234,000 233,000 232,000 232,000 | 4.40 5.74 6.71 4.17 5.82 6.64 | 7.00 7.00 4.50 4.50 5.50 5.50 | 13 13 13 13 13 | South South South South South |
| 10 | 10 | Without With Without With Without With Without With Without With | 2,107,700 2,107,700 2,107,850 2,107,850 2,107,850 2,107,501 2,108,700 2,106,300 | 235,000 235,000 234,000 234,000 233,000 233,000 232,000 232,000 | 8.46 8.91 10.47 12.53 8.89 11.70 14.97 9.12 | 10.50 10.50 11.50 11.50 15.50 13.00 19.50 14.50 | 17 16 17 16 17 16 13 | South South South South South South South South |
| 14 | 4 | Without With Without With Without With Without With Without With | 2,102,210 2,107,501 2,105,195 2,107,300 2,106,501 2,103,150 2,106,501 2,102,850 | 235,000 235,000 234,000 234,000 233,000 233,000 232,000 | 5.23 6.88 5.99 8.46 9.69 7.36 11.27 6.32 | 8.00 9.50 8.00 10.00 12.50 7.50 15.50 5.50 | 8 7 7 7 7 7 | South South South South South South South |
| 14 | 10 | Without With Without With Without With With Without With Without | 2,108,000 2,108,501 2,108,501 2,108,150 2,108,300 2,107,000 2,109,000 2,109,000 | 235,000 235,000 234,000 234,000 233,000 233,000 232,000 232,000 | 9.60 13.53 12.82 16.20 16.33 11.35 15.63 13.55 | 12.50 17.00 16.50 14.50 19.00 12.50 21.00 16.50 | 12 12 12 12 12 12 12 12 | South South South South South South South |

Note: Zones and baselines for angles are defined in Plate 3; without means breakwater is not installed, with means breakwater is installed.

* Coordinates are referred to New Jersey grid system.

Table 9

Breaking Wave Data for South Zone, East Wave Direction--Slack Tide

| Test | Wave | | | | king Chara | cteristic | S | |
|--------|--------|-----------------|------------------------|---------|----------------|----------------|---------|----------------|
| Period | Height | Breakwater | Coordina | | Height | Depth | Angle | Transport |
| sec | _ft_ | Status | E, ft | N, ft | ft | _ft_ | deg | Direction |
| 6 | 14 | Without | 2,103,000 | 233,000 | 3.23 | 7.50 | 5 | North |
| | | With | 2,102,501 | 233,000 | 4.28 | 5.20 | 5 1 | North |
| | | Without | 2,103,000 | 232,000 | 3.86 | 7.00 | 7 | South |
| | | With | 2,102,842 | 232,000 | 3.68 | 5.50 | 7 | South |
| 6 | 7 | Without | 2,108,000 | 235,000 | 8.74 | 12.50 | 6 | South |
| | | With | 2,107,501 | 235,000 | 6.79 | 10.00 | 11 | South |
| | | Without | 2,107,700 | 234,000 | 7.62 | 10.00 | 1 | South |
| | | With | 2,106,000 | 234,000 | 7.14 5.62 | 10.50 | 10 | South |
| | | Without With | 2,103,501 2,103,150 | 233,000 | 5.96 | 9.50 7.50 | 1 3 | North North |
| | | Without | 2,104,000 | 232,000 | 8.61 | 12.50 | 7 | South |
| | | With | 2,103,150 | 232,000 | 5.33 | 8.50 | 3 | North |
| 6 | 10 | Without | 2,108,501 | 235,000 | 10.05 | 17.50 | 3 | South |
| | | With | 2,108,000 | 235,000 | 9.32 | 12.50 | 19 | South |
| | | Without | 2,108,501 | 234,000 | 8.55 | 16.50 | 3 | South |
| | | With | 2,107,700 | 234,000 | 4.65 | 10.50 | 14 | South |
| | | Without | 2,108,000 | 233,000 | 10.63 | 16.50 | 7 | South |
| | | With | 2,107,300 | 233,000 | 8.46 | 12.50 | 1 | North |
| | | Without | 2,108,000 | 232,000 | 11.53 | 17.00 16.00 | 8 | North North |
| | 4 | With | 2,107,501 | 232,000 | 8.89 | | | NOT 611 |
| 10 | 4 | Without | 2,107,700 | 235,000 | 7.04 4.76 | 10.50 | 0 | South |
| | | With | 2,107,000 2,107,700 | 235,000 | 7.88 | 10.00 | 0 | 500011 |
| | | Without With | 2,105,700 | 234,000 | 5.61 | 8.00 | 2 | North |
| | | Without | 2,103,300 | 233,000 | 6.25 | 8.00 | 15 | South |
| | | With | 2,103,000 | 233,000 | 4.71 | 7.50 | 12 | South |
| | | Without | 2,103,000 | 232,000 | 4.46 | 7.00 | 7 | South |
| | | With | 2,103,000 | 232,000 | 4.72 | 7.00 | 7 | South |
| 10 | 10 | Without | 2,111,000 | 235,000 | 16.30 | 25.50 | 2 | South |
| | | With | 2,109,000 | 235,000 | 10.79 | 19.50 | 10 | South |
| | | Without | 2,110,000 | 234,000 | 16.65 | 24.50 | 4 | South South |
| | | With | 2,108,501 | 234,000 | 13.76 16.59 | 16.50 20.50 | 7 | South |
| | | Without | 2,109,000 | 233,000 | 10.74 | 14.50 | 2 | North |
| | | With Without | 2,107,700 2,108,000 | 232,000 | 13.46 | 17.00 | | North |
| | | With | 2,108,000 | 232,000 | 13.21 | 17.00 | 3 2 | North |
| 14 | 4 | Without | 2,108,000 | 235,000 | 9.26 | 9.50 | 1 | South |
| | | With | 2,107,501 | 235,000 | 8.67 | 10.00 | 7 | South |
| | | Without | 2,108,000 | 234,000 | 9.79 | 11.00 | 1 | South |
| | | With | 2,107,700 | 234,000 | 8.07 | 10.50 | 5 | North North |
| | | Without | 2,107,501 | 233,000 | 10.14 | 12.50 | 27 | South |
| | | With | 2,103,000 | 233,000 | 6.19 7.95 | 7.50 | 21 7 | North |
| | | Without With | 2,103,499 2,103,150 | 232,000 | 7.09 | 8.50 | 6 | North |
| 14 | 10 | Without | 2,112,000 | 235,000 | 21.52 | 29.50 | 1 | North |
| | 10 | With | 2,108,700 | 235,000 | 12.86 | 18.00 | 12 | South |
| | | Without | 2,111,000 | 234,000 | 17.89 | 26.50 | 1 | North |
| | | With | 2,108,700 | 234,000 | 14.69 | 17.50 | 5 | South |
| | | Without | 2,110,300 | 233,000 | 20.69 | 24.50 | 0 | South South |
| | | With | 2,109,000 | 233,000 | 16.56 | 20.50 | 5 | South |
| | | Without | 2,109,150 | 232,000 | 17.03 12.68 | 20.50 | 20 | North |
| | | With | 2,108,850 | 232,000 | 15.00 | 24.54 | | 1000000 |

Note: Zones and baselines for angles are defined in Plate 3; without means breakwater is not installed, with means breakwater is installed.

^{*} Coordinates are referred to New Jersey grid system.

Breaking Wave Data for South Zone, East Wave Direction--Flood Tide

| Test | | | | Break | | teristics | | |
|--------|--------|--|--|--|--|--|--|---|
| Period | Height | Breakwater | Coordin | | Height | Depth | Angle | Transport |
| sec | _ft_ | Status | E, ft | N, ft | ft | _ft_ | deg | Direction |
| 6 | 4 | Without With Without With Without With | 2,105,700 2,102,000 2,102,700 2,102,501 2,102,700 2,102,150 | 234,000 234,000 233,000 233,000 232,000 232,000 | 5.42 3.36 4.00 4.36 4.09 3.54 | 8.00 7.00 7.00 5.50 5.50 6.00 | 5 7 6 7 | North South South South |
| 6 | 7 | Without With | 2,108,000 2,107,700 | 235,000 | 8.75 6.62 | 12.50 10.50 | 4 | South South South |
| | | Without With Without With Without With | 2,107,700 2,106,000 2,103,501 2,103,150 2,103,300 2,103,150 | 234,000 234,000 233,000 233,000 232,000 232,000 | 7.33 5.65 6.92 5.05 7.33 6.38 | 10.00 10.50 9.00 7.50 9.50 8.50 | 4 7 7 7 7 | South North South South South South |
| 6 | 10 | Without With Without With Without With Without With Without With | 2,108,000 2,107,850 2,108,000 2,107,501 2,108,000 2,106,000 2,108,000 2,106,501 | 235,000 235,000 234,000 234,000 233,000 233,000 232,000 232,000 | 9.47 8.81 9.19 7.10 10.68 6.74 10.93 9.31 | 12.50 11.50 12.50 10.00 16.50 13.00 16.50 14.50 | 7 7 7 7 7 17 7 | South South South South North South North |
| 10 | -14 | Without With Without With Without With Without With Without With | 2,107,300 2,107,000 2,107,300 2,105,700 2,102,700 2,103,000 2,103,000 2,103,000 | 235,000 235,000 234,000 234,000 233,000 233,000 232,000 232,000 | 7.76 5.14 7.21 5.50 4.59 4.83 5.00 5.96 | 9.50 9.50 9.50 8.00 5.50 7.50 6.50 7.00 | 3 2 3 7 43 3 7 | South South South South South South South South |
| 10 | 10 | Without With Without With Without With Without With Without With | 2,111,300 2,109,000 2,110,000 2,108,300 2,109,000 2,108,000 2,108,000 2,108,000 | 235,000 235,000 234,000 234,000 233,000 233,000 232,000 232,000 | 15.64 10.30 15.50 12.81 15.59 9.63 12.44 13.19 | 26.50 19.50 24.00 15.50 20.50 16.50 17.00 | 7 14 7 7 3 0 7 8 | South South South North South North |
| 14 | 14 | Without With Without With Without With Without With Without With | 2,108,000 2,107,499 2,108,000 2,107,499 2,107,501 2,103,000 2,103,300 2,102,850 | 235,000 235,000 234,000 234,000 233,000 233,000 232,000 | 9.48 7.64 9.56 8.11 10.37 6.20 8.60 7.18 | 12.50 10.00 13.00 10.00 13.50 7.50 9.50 5.50 | 8 7 1 4 7 7 12 7 | South South North North South South South |
| 14 | 10 | Without With Without With Without With Without With | 2,112,000 2,109,300 2,111,000 2,108,700 2,110,499 2,108,300 2,109,499 2,107,000 | 235,000 235,000 234,000 234,000 233,000 233,000 232,000 232,000 | 18.87 15.04 17.21 13.71 16.95 15.45 16.60 11.60 | 29.00 20.50 26.50 17.50 25.00 19.00 23.00 15.00 | 5 12 2 5 1 5 1 20 | South South South North North North |

Note: Zones and baselines for angles are defined in Plate 3; without means breakwater is not installed, with means breakwater is installed.

* Coordinates are referred to New Jersey grid system.

Table 11

Breaking Wave Data for South Zone, East Wave Direction--Ebb Tide

| Test | | | | | king Chara | cteristic | S | |
|--------|--------|------------|-----------|---------|------------|-----------|-------|-----------|
| Period | Height | Breakwater | Coording | ates* | Height | Depth | Angle | Transport |
| sec | _ft_ | Status | E, ft | N, ft | _ft_ | <u>ft</u> | deg | Direction |
| 6 | 4 | Without | 2,102,000 | 235,000 | 3.84 | 8.00 | 3 | 0 |
| 7 | - | With | 2,102,000 | | | 60000 | 3 | South |
| | | | | 235,000 | 3.59 | 8.00 | 1 | South |
| | | Without | 2,108,000 | 234,000 | 7.34 | 12.50 | 2 | South |
| | | With | 2,102,000 | 234,000 | 3.67 | 6.50 | 7 | South |
| | | Without | 2,103,150 | 233,000 | 5.00 | 7.50 | 14 | South |
| | | With | 2,102,499 | 233,000 | 4.79 | 5.00 | 2 | North |
| | | Without | 2,103,000 | 232,000 | 3.42 | 6.50 | 4 | South |
| | | With | 2,102,799 | 232,000 | 4.61 | 6.50 | 2 | North |
| 6 | 7 | Without | 2,108,000 | 235,000 | 9.08 | 12.00 | 7 | South |
| | | With | 2,108,000 | 235,000 | 8.94 | 12.00 | 3 | South |
| | | Without | 2,108,000 | 234,000 | 6.51 | 12.50 | 7 | South |
| | | With | 2,105,700 | 234,000 | 5.20 | 8.00 | 7 | South |
| | | Without | 2,108,000 | 233,000 | 8.63 | 16.00 | 7 | South |
| | | With | 2,103,000 | 233,000 | 4.08 | 7.00 | 7 | North |
| | | Without | 2,107,000 | 232,000 | 9.71 | 14.50 | 2 | |
| | | With | 2,103,000 | | 7 | | | South |
| - | | | | 232,000 | 4.91 | 6.50 | 15 | North |
| 6 | 10 | Without | 2,109,000 | 235,000 | 11.26 | 18.50 | 7 | South |
| | | With | 2,108,000 | 235,000 | 10.33 | 12.00 | 3 | South |
| | | Without | 2,109,000 | 234,000 | 9.76 | 19.00 | 7 | South |
| | | With | 2,107,850 | 234,000 | 6.74 | 11.50 | 15 | South |
| | | Without | 2,108,501 | 233,000 | 12.30 | 19.50 | 2 | South |
| | | With | 2,107,501 | 233,000 | 8.30 | 12.50 | 14 | South |
| | | Without | 2,108,501 | 232,000 | 9.46 | 18.50 | 2 | South |
| | | With | 2,107,501 | 232,000 | 6.53 | 15.50 | 5 | North |
| 10 | 4 | Without | 2,107,700 | 235,000 | 6.41 | 10.00 | 5 | South |
| | | With | 2,102,150 | 232,000 | 4.84 | 7.50 | 14 | North |
| | | Without | 2,107,501 | 234,000 | 7.97 | 9.50 | 5 | North |
| | | With | 2,105,700 | 234,000 | 4.12 | 8.00 | 1 | North |
| | | Without | 2,103,000 | 233,000 | 5.24 | 7.00 | 8 | North |
| | | With | 2,102,700 | 233,000 | 4.66 | 5.00 | | South |
| | | Without | 2,103,000 | 232,000 | 6.30 | 6.50 | 9 | North |
| | | With | 2,102,700 | 232,000 | 5.32 | 5.50 | 7 | South |
| 20 | 3.0 | | | | 14.26 | | 2 | |
| 10 | 10 | Without | 2,110,501 | 235,000 | | 22.50 | 3 | South |
| | | With | 2,109,000 | 235,000 | 10.65 | 18.50 | 10 | South |
| | | Without | 2,110,501 | 234,000 | 15.48 | 25,50 | 3 | South |
| | | With | 2,108,499 | 234,000 | 11.82 | 16.50 | 3 | South |
| | | Without | 2,110,501 | 233,000 | 15.25 | 24.50 | | South |
| | | With | 2,108,000 | 233,000 | 9.15 | 16.50 | 7 | South |
| | | Without | 2,108,501 | 232,000 | 14.02 | 18.50 | 1 | South |
| | | With | 2,107,700 | 232,000 | 11.23 | 16.50 | 5 | North |
| 14 | 4 | Without | 2,107,850 | 235,000 | 11.37 | 11.00 | 1 | North |
| | | With | 2,107,499 | 235,000 | 8.55 | 9.50 | 13 | South |
| | | Without | 2,107,700 | 234,000 | 11.57 | 9.50 | 1 | North |
| | | With | 2,107,625 | 234,000 | 7.59 | 9.50 | 2 | North |
| | | Without | 2,107,700 | 233,000 | 10.75 | 14.00 | 10 | North |
| | | With | 2,103,150 | 233,000 | 7.07 | 7.50 | 17 | North |
| | | Without | 2,103,150 | 232,000 | 8.80 | 8.00 | 7 | South |
| | | With | 2,103,150 | 232,000 | 8.07 | 8.00 | 7 | North |
| 14 | 30 | Without | 2,112,000 | 235,000 | 20.34 | 29.50 | 7 | South |
| 14 | 10 | | 2,109,700 | 235,000 | 13.99 | 20.50 | 18 | South |
| | | With | | | 16.91 | 26.00 | 5 | South |
| | | Without | 2,111,000 | 234,000 | | 17.00 | | South |
| | | With | 2,108,700 | 234,000 | 11.75 | | 9 | |
| | | Without | 2,110,501 | 233,000 | 18.90 | 24.50 | 5 | South |
| | | With | 2,109,000 | 233,000 | 16.27 | 20.00 | 2 | South |
| | | Without | 2,109,501 | 232,000 | 19.07 | 22.50 | 1 | North |
| | | With | 2,109,000 | 232,000 | 12.67 | 16.50 | 14 | North |

Note: Zones and baselines for angles are defined in Plate 3; without means breakwater is not installed, with means breakwater is installed.

^{*} Coordinates are referred to New Jersey grid system.

Table 12

Breaking Wave Data for South Zone, E22.5°S Wave Direction--Slack Tide

| Test | Wave | | - | | aking Chara | cteristic | S | |
|--------|--------|------------|-----------|---------|-------------|-----------|-------|-----------|
| Period | Height | Breakwater | Coordin | | Height | Depth | Angle | Transport |
| sec | ft | Status | E, ft | N, ft | _ft_ | _ft_ | deg | Direction |
| 6 | 14 | Without | 2,105,679 | 234,000 | 4.08 | 8.00 | 14 | North |
| | | With | 2,105,679 | 234,000 | 4.75 | 8.00 | 14 | North |
| | | Without | 2,102,586 | 233,000 | 3.75 | 5.00 | 15 | North |
| | | With | 2,102,586 | 233,000 | 4.11 | 5.00 | 13 | North |
| | | Without | 2,102,865 | 232,000 | 4.57 | 5.50 | 15 | North |
| | | With | 2,102,865 | 232,000 | 4.57 | 5.50 | 15 | North |
| 6 | 7 | Without | 2,107,568 | 235,000 | 6.78 | 9.50 | 16 | North |
| | | With | 2,107,568 | 235,000 | 6.14 | 9.50 | 16 | North |
| | | Without | 2,107,661 | 234,000 | 8.63 | 10.00 | 16 | North |
| | | With | 2,107,661 | 234,000 | 6.89 | 10.00 | 16 | North |
| | | Without | 2,107,000 | 233,000 | 6.62 | 12.00 | 16 | North |
| | | With | 2,107,000 | 233,000 | 7.84 | 12.00 | 16 | North |
| | | Without | 2,104,655 | 232,000 | 5.50 | 14.50 | 16 | North |
| | | With | 2,104,655 | 232,000 | 6,26 | 14.50 | 16 | North |
| 6 | 10 | Without | 2,108,069 | 235,000 | 9.46 | 12.50 | 15 | North |
| | | With | 2,107,889 | 235,000 | 7.27 | 11.50 | 15 | North |
| | | Without | 2,108,105 | 234,000 | 9.90 | 14.00 | 15 | North |
| | | With | 2,108,000 | 234,000 | 8.73 | 12.50 | 15 | North |
| | | Without | 2,107,486 | 233,000 | 10.07 | 12.00 | 15 | North |
| | | With | 2,107,679 | 233,000 | 10.79 | 14.50 | 15 | North |
| | | Without | 2,107,000 | 232,000 | 9.43 | 14.50 | 15 | North |
| | | With | 2,106,895 | 232,000 | 9.90 | 14.50 | 15 | North |
| 10 | 4. | Without | 2,105,820 | 234,000 | 5.96 | 7.50 | 12 | North |
| | | With | 2,106,000 | 234,000 | 5.74 | 10.00 | 11 | North |
| | | Without | 2,103,000 | 233,000 | 5.07 | 7.00 | 10 | North |
| | | With | 2,102,835 | 233,000 | 4.49 | 6.50 | 9 | North |
| | | Without | 2,103,000 | 232,000 | 5.62 | 6.50 | 8 | North |
| | | With | 2,103,000 | 232,000 | 5.84 | 6.50 | 9 | North |
| 10 | 10 | Without | 2,108,135 | 235,000 | 10.92 | 13.50 | 13 | North |
| | | With | 2,108,000 | 235,000 | 9.78 | 12.00 | 15 | North |
| | | Without | 2,108,850 | 234,000 | 14.15 | 18.00 | 13 | North |
| | | With | 2,108,679 | 234,000 | 14.13 | 17.00 | 15 | North |
| | | Without | 2,109,000 | 233,000 | 13.12 | 20.00 | 16 | North |
| | | With | 2,108,000 | 233,000 | 13.40 | 16.50 | 16 | North |
| | | Without | 2,108,240 | 232,000 | 13.82 | 17.00 | 16 | North |
| | | With | 2,108,240 | 232,000 | 14.45 | 17.00 | 16 | North |
| 14 | 4 | Without | 2,107,610 | 235,000 | 7.09 | 9.50 | 13 | North |
| | | With | 2,107,000 | 235,000 | 6.30 | 9.50 | 13 | North |
| | | Without | 2,107,685 | 234,000 | 9.53 | 10.00 | 13 | North |
| | | With | 2,107,685 | 234,000 | 9.00 | 10.00 | 13 | North |
| | | Without | 2,107,225 | 233,000 | 10.71 | 12.00 | 13 | North |
| | | With | 2,107,225 | 233,000 | 10.78 | 12.00 | 13 | North |
| | | Without | 2,105,225 | 232,000 | 7.26 | 14.50 | 13 | North |
| 200 | | With | 2,105,000 | 232,000 | 8.74 | 14.50 | 13 | North |
| 14 | 10 | Without | 2,110,300 | 235,000 | 15.79 | 18.00 | 18 | North |
| | | With | 2,108,300 | 235,000 | 11.72 | 14.50 | 13 | North |
| | | Without | 2,109,300 | 234,000 | 13.19 | 20.50 | 18 | North |
| | | With | 2,109,000 | 234,000 | 12.89 | 19.00 | 19 | North |
| | | Without | 2,109,000 | 233,000 | 16.04 | 20.00 | 18 | North |
| | | With | 2,109,500 | 233,000 | 18.74 | 22.00 | 19 | North |
| | | Without | 2,108,700 | 232,000 | 16.76 | 19.50 | 18 | North |
| | | With | 2,109,000 | 232,000 | 16.06 | 21.00 | 19 | North |

Note: Zones and baselines for angles are defined in Plate 3; without means breakwater is not installed, with means breakwater is installed.

* Coordinates are referred to New Jersey grid system.

Breaking Wave Data for South Zone, Southeast Wave Direction--Slack Tide

| Test | | | | | king Chara | cteristic | S | |
|--------|--------|--|--|--|---|--|--|---|
| Period | Height | Breakwater | Coordina | | Height | Depth | Angle | Transport |
| sec | _ft_ | _Status_ | E, ft | N, ft | _ft_ | ft | deg | Direction |
| 6 | 4 | Without With Without With Without | 2,105,835 2,105,835 2,103,375 2,103,375 2,103,180 | 234,000 234,000 233,000 232,000 | 3.86 3.79 6.66 5.07 4.67 | 8.00 8.00 8.00 8.50 | 32 31 28 28 28 | North North North North |
| 6 | 7 | With Without With Without With Without With Without With Without | 2,103,180 2,108,000 2,108,000 2,107,730 2,107,730 2,107,000 2,107,000 2,106,105 | 232,000 235,000 235,000 234,000 234,000 233,000 233,000 | 6.21 6.88 6.46 6.74 7.56 6.68 7.73 8.01 | 8.50 12.50 12.50 10.00 10.00 12.00 12.00 14.50 | 28 31 31 31 31 31 31 | North North North North North North |
| 6 | 10 | Without With Without With Without With Without With Without With | 2,106,105 2,108,105 2,108,105 2,108,000 2,108,000 2,107,769 2,107,769 2,107,901 2,106,904 2,107,481 | 232,000 235,000 235,000 234,000 234,000 233,000 232,000 232,000 | 8.38 8.71 9.34 9.62 10.07 10.60 10.98 8.52 9.84 | 14.50 13.00 13.00 12.50 12.50 15.50 14.50 15.50 | 31 33 31 33 34 34 34 34 | North North North North North North North |
| 10 | 14 | Without With Without With Without With | 2,105,835 2,105,835 2,103,375 2,103,375 2,103,180 2,103,679 | 234,000 234,000 233,000 233,000 232,000 | 5.06 4.92 7.32 7.46 6.47 7.33 | 8.00 8.00 8.00 8.00 8.50 | 29 29 29 29 29 | North North North North North |
| 10 | 10 | Without With Without With Without With Without With Without | 2,108,625 2,108,625 2,108,556 2,108,556 2,108,135 2,108,135 2,108,135 2,108,300 | 235,000 235,000 234,000 234,000 233,000 232,000 232,000 | 12.45 12.45 12.77 14.12 12.36 10.44 11.98 14.00 | 17.50 17.50 16.50 16.50 17.50 17.50 18.50 17.50 | 30 30 30 30 31 30 31 33 | North North North North North North North |
| 14 | 14 | Without With Without With Without With Without With Without With | 2,107,700 2,107,775 2,107,820 2,107,820 2,106,000 2,106,000 2,106,321 2,106,321 | 235,000 235,000 234,000 234,000 233,000 232,000 232,000 | 8.51 8.66 8.26 8.25 8.95 9.54 10.97 10.44 | 10.50 11.00 11.00 11.00 12.50 12.50 14.00 | 31 31 31 31 31 31 31 31 | North North North North North North North |
| 14 | 10 | Without With Without With Without With Without With | 2,110,000 2,110,000 2,109,369 2,110,000 2,109,135 2,109,435 2,109,225 2,109,225 | 235,000 235,000 234,000 234,000 233,000 232,000 232,000 | 16.08 14.45 15.47 16.31 16.43 16.53 15.90 15.44 | 21.50 21.50 21.00 24.00 20.50 22.00 21.50 21.50 | 33 32 33 32 33 32 34 34 | North North North North North North North |

Note: Zones and baselines for angles are defined in Plate 3; without means breakwater is not installed, with means breakwater is installed.

^{*} Coordinates are referred to New Jersey grid system.

Table 14 Breaking Wave Data for North Zone, Southeast Wave Direction--Slack Tide

| 1000 | Wave | | | | aking Chara | cteristic | S | |
|---------------|--------------|----------------------|------------------|---------|--------------|-------------|--------------|------------------------|
| Period sec | Height ft | Breakwater Status | Coordin E, ft | ates* | Height ft | Depth ft | Angle deg | Transport Direction |
| 6 | 10 | Without | 2,111,881 | 246,119 | 8.66 | 13.50 | 12 | North |
| | | With | 2,111,678 | 246,322 | 9.25 | 12.00 | 12 | North |
| | | Without | 2,112,000 | 247,000 | 10.13 | 11.50 | 12 | North |
| | | With | 2,112,000 | 247,000 | 10.15 | 11.50 | 12 | North |
| 10 | 10 | Without | 2,111,756 | 246,244 | 11.05 | 12.50 | 11 | North |
| | | With | 2,112,038 | 245,962 | 11.06 | 15.50 | 12 | North |
| | | Without | 2,112,182 | 246,818 | 12.45 | 14.50 | 11 | North |
| | | With | 2,112,182 | 246,818 | 11.72 | 14.50 | 12 | North |
| | | Without | 2,112,085 | 247,915 | 12.16 | 14.00 | 1.1 | North |
| | | With | 2,112,085 | 247,915 | 10.83 | 14.00 | 12 | North |
| 10 | 14 | Without | 2,114,000 | 244,000 | 15.80 | 25.00 | 9 | North |
| | | With | 2,114,000 | 244,000 | 17.13 | 25.00 | 9 | North |
| | | Without | 2,113,000 | 246,000 | 16.73 | 21.00 | 14 | North |
| | | With | 2,113,000 | 246,000 | 16.67 | 21.00 | 13 | North |
| | | Without | 2,113,000 | 247,000 | 14.84 | 19.00 | 14 | North |
| | | With | 2,113,000 | 247,000 | 13.42 | 19.00 | 13 | North |
| | | Without | 2,114,000 | 247,000 | 17.93 | 21.50 | 14 | North |
| | | With | 2,114,000 | 247,000 | 16.70 | 21.50 | 13 | North |
| 14 | 10 | Without | 2,112,160 | 245,840 | 14.59 | 16.50 | 9 | North |
| | | With | 2,112,160 | 245,840 | 15.63 | 16.50 | 9 | North |
| | | Without | 2,112,160 | 246,840 | 10.43 | 14.00 | 9 | North |
| | | With | 2,112,160 | 246,840 | 9.53 | 14.00 | 9 | North |
| | | Without | 2,112,265 | 247,735 | 13.64 | 14.50 | 10 | North |
| | | With | 2,112,265 | 247,735 | 13.16 | 14.50 | 10 | North |
| 14 | 14 | Without | 2,114,000 | 244,000 | 18.69 | 25.50 | 13 | North |
| | | With | 2,114,000 | 244,000 | 18.40 | 32.00 | 14 | North |
| | | Without | 2,112,788 | 246,212 | 13.25 | 19.00 | 13 | North |
| | | With | 2,112,788 | 246,212 | 13.71 | 19.00 | 13 | North |
| | | Without | 2,112,875 | 247,125 | 15.91 | 18.50 | 13 | North |
| | | With | 2,113,000 | 247,000 | 15.51 | 19.00 | 13 | North |
| | | Without | 2,114,000 | 247,000 | 17.47 | 21.50 | 13 | North |
| | | With | 2,114,000 | 247,000 | 17.58 | 21.50 | 13 | North |

Note: Zones and baselines for angles are defined in Plate 3; without means breakwater is not installed, with means breakwater is installed.

* Coordinates are referred to New Jersey grid system.

Table 15

Breaking Wave Data for North Zone, S22.5°E Wave Direction--Slack Tide

| | Wave | | | | king Chara | cteristic | S | |
|---------------|--------------|----------------------|-------------------|---------|---------------|-----------|---------------|------------------------|
| Period sec | Height ft | Breakwater Status | Coordina E, ft | N, ft | Height _ft | Depth ft | Angle deg_ | Transport Direction |
| 6 | 10 | Without | 2,112,000 | 247,000 | 8.98 | 11.50 | 30 | North |
| | | With | 2,112,000 | 247,000 | 8.98 | 11.50 | 30 | North |
| 10 | 10 | Without | 2,112,000 | 246,000 | 12.59 | 15.50 | 26 | North |
| | | With | 2,112,000 | 246,000 | 12.89 | 15.50 | 26 | North |
| | | Without | 2,113,000 | 246,664 | 13.63 | 19.50 | 26 | North |
| | | With | 2,113,000 | 246,664 | 13.48 | 19.50 | 26 | North |
| 10 | 14 | Without | 2,112,000 | 238,000 | 16.99 | 24.50 | 23 | North |
| | | With | 2,112,000 | 240,000 | 19.87 | 22.50 | 25 | North |
| | | Without | 2,113,000 | 239,000 | 17.11 | 27.00 | 23 | North |
| | | With | 2,113,000 | 242,408 | 18.59 | 24.00 | 25 | North |
| | | Without | 2,114,000 | 240,171 | 14.50 | 29.00 | 22 | North |
| | | With | 2,114,000 | 241,500 | 17.20 | 26.50 | 25 | North |
| | | Without | 2,115,000 | 240,721 | 16.34 | 31.50 | 26 | North |
| | | With | 2,115,000 | 241,000 | 17.09 | 30.50 | 25 | North |
| 14 | 10 | Without | 2,112,000 | 246,000 | 13.01 | 15.50 | 22 | North |
| | | With | 2,112,000 | 246,112 | 12.86 | 14.50 | 22 | North |
| | | Without | 2,113,000 | 247,000 | 11.74 | 19.00 | 22 | North |
| | | With | 2,113,000 | 247,000 | 13.41 | 19.00 | 22 | North |
| 14 | 14 | Without | 2,112,000 | 237,510 | 17.10 | 25.50 | 24 | North |
| | | With | 2,112,000 | 239,550 | 16.03 | 23.50 | 27 | North |
| | | Without | 2,113,000 | 238,000 | 20.61 | 28.50 | 24 | North |
| | | With | 2,113,000 | 244,000 | 14.94 | 23.50 | 25 | North |
| | | Without | 2,114,000 | 238,000 | 22.42 | 32.50 | 24 | North |
| | | With | 2,114,000 | 244,000 | 19.29 | 25.50 | 25 | North |
| | | Without | 2,115,000 | 243,000 | 16.18 | 31.00 | 24 | North |
| | | With | 2,115,000 | 243,000 | 16.46 | 31.00 | 25 | North |

* Coordinates are referred to New Jersey grid system.

Note: Zones and baselines for angles are defined in Plate 3; without means breakwater is not installed, with means breakwater is installed.

Table 16

Breaking Wave Data for North Zone, South Wave Direction--Slack Tide

| Test | | A STATE OF THE STA | | | aking Chars | | | |
|---------------|-----------|--|------------------|--------------|-------------|----------|--------------|------------------------|
| Period sec | Height ft | Breakwater Status | Coordin E, ft | ates* _N, ft | Heightft | Depth ft | Angle deg | Transport Direction |
| 6 | 10 | Without | 2,113,000 | 251,000 | 8.02 | 11.50 | 30 | North |
| | | With | 2,113,000 | 251,000 | 5.56 | 11.50 | 34 | North |
| | | Without | 2,114,000 | 252,000 | 8.18 | 15.00 | 30 | North |
| | | With | 2,114,000 | 252,000 | 7.80 | 15.00 | 34 | North |
| 10 | 10 | Without | 2,111,000 | 244,000 | 8.46 | 13.50 | 23 | North |
| | | With | 2,113,000 | 250,500 | 6.90 | 9.00 | 20 | North |
| | | Without | 2,113,000 | 250,000 | 11.28 | 14.50 | 23 | North |
| | | With | 2,111,000 | 245,000 | 9.62 | 12.50 | 31 | North |
| 10 | 14 | Without | 2,115,000 | 248,000 | 16.82 | 19.50 | 23 | North |
| | | With | 2,113,000 | 246,000 | 10.34 | 20.50 | 24 | North |
| | | Without | 2,116,000 | 248,500 | 17.14 | 21.00 | 23 | North |
| | | With | 2,116,000 | 249,000 | 13.78 | 23.00 | 24 | North |
| | | Without | 2,113,000 | 246,000 | 10.53 | 20.50 | 23 | North |
| | | With | 2,115,000 | 248,000 | 14.14 | 19.50 | 24 | North |
| 14 | 10 | Without | 2,113,000 | 247,000 | 14.48 | 19.50 | 33 | North |
| | | With | 2,114,000 | 251,000 | 12.03 | 16.50 | 37 | North |
| | | Without | 2,114,000 | 250,700 | 11.40 | 17.00 | 40 | North |
| | | With | 2,113,000 | 248,000 | 11.69 | 18.75 | 37 | North |
| 14 | 14 | Without | 2,113,000 | 243,000 | 17.85 | 25.00 | 22 | North |
| | | With | 2,113,000 | 246,000 | 12.69 | 22.00 | 21 | North |
| | | Without | 2,116,000 | 250,000 | 11.89 | 26.50 | 26 | North |
| | | With | 2,116,000 | 249,000 | 14.49 | 23.50 | 21 | North |
| | | Without | 2,115,000 | 247,000 | 16.17 | 26.50 | 24 | North |
| | | With | 2,115,000 | 248,000 | 13.46 | 20.00 | 21 | North |
| | | Without | 2,114,000 | 246,000 | 13.91 | 26.50 | 24 | North |
| | | With | 2,114,000 | 247,000 | 15.52 | 22.50 | 21 | North |

* Coordinates are referred to New Jersey grid system.

Note: Zones and baselines for angles are defined in Plate 3; without means breakwater is not installed, with means breakwater is installed.

Table 17
Breaking Wave Data for North Zone, South Wave Direction--Flood Tide

| | Wave | A | | | king Chara | | | |
|---------------|----------|----------------------|-----------|---------|--------------|----------|---------------|------------------------|
| Period sec | Heightft | Breakwater Status | Coordina | N, ft | Height ft | Depthft_ | Angle deg_ | Transport Direction |
| 6 | 10 | Without | 2,112,000 | 247,000 | 6.61 | 12.50 | 28 | North |
| | | With | 2,112,000 | 247,000 | 4.45 | 12.50 | 31 | North |
| | | Without | 2,114,000 | 252,000 | 7.53 | 15.00 | 22 | North |
| | | With | 2,114,000 | 252,000 | 7.80 | 15.00 | 26 | North |
| | | Without | 2,113,000 | 251,000 | 7.54 | 12.50 | 22 | North |
| | | With | 2,113,000 | 251,000 | 3.87 | 12.50 | 26 | North |
| 10 | 10 | Without | 2,112,000 | 246,000 | 9.05 | 15.50 | 20 | North |
| | | With | 2,112,000 | 247,000 | 7.20 | 12.00 | 21 | North |
| | | Without | 2,114,000 | 248,000 | 10.25 | 19.00 | 27 | North |
| | | With | 2,113,000 | 250,000 | 8.54 | 14.50 | 28 | North |
| | | Without | 2,115,000 | 248,500 | 10.54 | 19.00 | 27 | North |
| | | With | 2,115,000 | 248,000 | 11.99 | 19.50 | 26 | North |
| | | Without | 2,113,000 | 250,000 | 9.80 | 14.50 | 26 | North |
| | | With | 2,114,000 | 248,000 | 10.07 | 19.00 | 26 | North |
| 10 | 14 | Without | 2,114,000 | 247,000 | 20.03 | 22.50 | 26 | North |
| | | With | 2,116,000 | 246,000 | 16.45 | 29.50 | 32 | North |
| | | Without | 2,116,000 | 246,000 | 15.05 | 30.00 | 33 | North |
| | | With | 2,115,000 | 248,000 | 15.84 | 19.50 | 25 | North |
| | | Without | 2,115,000 | 248,000 | 14.96 | 20.00 | 26 | North |
| | | With | 2,114,000 | 247,500 | 12.53 | 20.50 | 25 | North |
| 14 | 10 | Without | 2,113,000 | 247,500 | 13.77 | 18.50 | 24 | North |
| | | With | 2,112,500 | 248,500 | 11.21 | 17.50 | 18 | North |
| | | Without | 2,114,000 | 251,000 | 9.69 | 17.00 | 28 | North |
| | | With | 2,114,000 | 250,000 | 11.42 | 18.50 | 26 | North |
| 14 | 14 | Without | 2,114,000 | 246,000 | 15.56 | 26.00 | 25 | North |
| | | With | 2,115,000 | 247,000 | 10.90 | 26.50 | 27 | North |
| | | Without | 2,116,000 | 249,000 | 10.33 | 23.50 | 28 | North |
| | | With | 2,115,000 | 249,000 | 12.75 | 23.50 | 26 | North |
| | | Without | 2,115,000 | 247,000 | 12.99 | 26.50 | 25 | North |
| | | With | 2,114,000 | 245,000 | 12.28 | 26.50 | 27 | North |
| | | | | | | | | |

Note: Zones and baselines for angles are defined in Plate 3; without means breakwater is not installed, with means breakwater is installed.

^{*} Coordinates are referred to New Jersey grid system.

Table 18

Breaking Wave Data for North Zone, South Wave Direction--Ebb Tide

| Test | Wave | | | | king Chara | | | 77 |
|---------------|--------------|----------------------|-----------|---------|--------------|-------------|--------------|-----------|
| Period sec | Height ft | Breakwater Status | Coording | N, ft | Height ft | Depth ft | Angle deg | Direction |
| 6 | 10 | Without | 2,114,000 | 252,000 | 5.19 | 15.00 | 24 | North |
| | | With | 2,113,000 | 251,000 | 7.89 | 12.50 | 24 | North |
| | | Without | 2,113,000 | 251,000 | 6.67 | 12.50 | 24 | North |
| | | With | 2,114,000 | 252,000 | 4.85 | 15.00 | 24 | North |
| 10 | 10 | Without | 2,113,000 | 250,330 | 10.03 | 13.00 | 26 | North |
| | | With | 2,115,000 | 248,000 | 14.32 | 20.00 | 26 | North |
| | | Without | 2,115,000 | 248,000 | 11.46 | 19.50 | 30 | North |
| | | With | 2,114,000 | 248,000 | 11.01 | 19.00 | 26 | North |
| | | Without | 2,114,000 | 247,500 | 11.64 | 20.00 | 30 | North |
| | | With | 2,113,000 | 250,000 | 7.24 | 14.50 | 25 | North |
| 10 | 14 | Without | 2,112,000 | 246,000 | 13.29 | 16.00 | 28 | North |
| | | With | 2,114,000 | 247,000 | 13.87 | 22.50 | 28 | North |
| | | Without | 2,114,000 | 247,000 | 10.11 | 22.50 | 28 | North |
| | | With | 2,116,000 | 246,000 | 18.00 | 30.00 | 34 | North |
| | | Without | 2,116,000 | 246,000 | 17.41 | 29.50 | 32 | North |
| | | With | 2,112,000 | 246,000 | 10.42 | 16.00 | 28 | North |
| | | Without | 2,115,000 | 248,000 | 15.23 | 19.50 | 28 | North |
| | | With | 2,115,000 | 248,000 | 13.73 | 20.00 | 28 | North |
| 14 | 10 | Without | 2,115,000 | 248,000 | 10.47 | 19.50 | 24 | North |
| | | With | 2,115,000 | 248,500 | 11.33 | 19.50 | 24 | North |
| | | Without | 2,113,000 | 246,500 | 12.64 | 20.50 | 22 | North |
| | | With | 2,113,000 | 250,000 | 13.49 | 14.50 | 19 | North |
| | | Without | 2,112,000 | 246,000 | 11.20 | 15.50 | 20 | North |
| | | With | 2,112,000 | 247,000 | 10.31 | 12.00 | 21 | North |
| 14 | 14 | Without | 2,115,000 | 248,000 | 13.43 | 19.50 | 28 | North |
| | | With | 2,113,000 | 247,000 | 14.53 | 19.50 | 24 | North |
| | | Without | 2,114,000 | 245,000 | 14.94 | 26.50 | 30 | North |
| | | With | 2,114,000 | 247,500 | 13.46 | 20.00 | 24 | North |
| | | Without | 2,116,000 | 249,000 | 14.65 | 23.50 | 28 | North |
| | | With | 2,115,000 | 248,500 | 15.56 | 19.50 | 24 | North |
| | | Without | 2,113,000 | 246,000 | 16.29 | 21.50 | 30 | North |
| | | With | 2,116,000 | 249,000 | 14.49 | 23.50 | 24 | North |

Note: Zones and baselines for angles are defined in Plate 3; without means breakwater is not installed, with means breakwater is installed.

^{*} Coordinates are referred to New Jersey grid system.

Table 19
Consolidation of Waves Approaching South Zone* from the Northeast

| Wave Period | Per | centage | e of Tot | al Wav | e Climat | te per Wa | ave Heig | ht Group | , ft |
|-------------|-------------|----------|----------|---------|----------|-----------|------------|----------|-------|
| sec | 1-3 | 3-5 | 5-7 | 7-9 | 9-11 | 11-13 | 13-15 | 15-17 | Total |
| | Se | elected | Portion | of No | rtheast | Wave Cl | imate | | |
| 5-7 | 0.70 | 0.70 | 0.35 | 0.17 | 0.06 | 0.01 | 0.01 | 0 | 2,00 |
| 7-9 | 0.51 | 0.56 | 0.64 | 0.44 | 0.12 | 0.03 | 0.01 | 0.02 | 2.33 |
| 9-11 | 0.34 | 0.39 | 0.36 | 0.45 | 0.14 | 0.06 | 0.03 | 0.02 | 1.79 |
| 11-13 | 0.03 | 0.12 | 0.18 | 0.22 | 0.13 | 0.05 | 0.04 | 0.03 | 0.80 |
| 13-15 | 0 | 0.03 | 0.04 | 0.05 | 0.05 | 0.04 | 0.03 | 0.02 | 0.26 |
| >15 | 0 | 0 | 0.02 | 0.02 | 0.02 | 0.02 | 0.01 | 0.01 | 0.10 |
| Total | 1.58 | 1.80 | 1.59 | 1.35 | 0.52 | 0.21 | 0.13 | 0.10 | 7.28 |
| | | Elimin | nating 7 | 7-9 Sec | Wave P | eriod Gr | oup | | |
| 5-7 | 0.96 | 0.98 | 0.67 | 0.39 | 0.12 | 0.02 | 0.01 | 0.01 | 3.16 |
| 9-11 | 0.59 | 0.67 | 0.68 | 0.67 | 0.20 | 0.08 | 0.04 | 0.03 | 2.96 |
| 11-13 | 0.03 | 0.12 | 0.18 | 0.22 | 0.13 | 0.05 | 0.04 | 0.03 | 0.80 |
| 13-15 | 0 | 0.03 | 0.04 | 0.05 | 0.05 | 0.04 | 0.03 | 0.02 | 0.26 |
| >15 | 0 | 0 | 0.02 | 0.02 | 0.02 | 0.02 | 0.01 | 0.01 | 0.10 |
| Total | 1.58 | 1.80 | 1.59 | 1.35 | 0.52 | 0.21 | 0.13 | 0.10 | 7.28 |
| | <u>E1</u> : | iminati | ng 11-1 | 3 and > | 15 Sec | Wave Per | iod Grou | ps | |
| 5-7 | 0.96 | 0.98 | 0.67 | 0.39 | 0.12 | 0.02 | 0.01 | 0.01 | 3.16 |
| 9-11 | 0.61 | 0.73 | 0.77 | 0.78 | 0.27 | 0.11 | 0.06 | 0.05 | 3.38 |
| 13-15 | 0.01 | 0.09 | 0.15 | | 0.13 | 0.08 | 0.06 | 0.04 | 0.74 |
| Total | 1.58 | 1.80 | 1.59 | 1.35 | 0.52 | 0.21 | 0.13 | 0.10 | 7.28 |
| | Wave | Period | | | Wave He | ight, ft | | | |
| | | sec | = | 4 | _7_ | 10_ | Total | - | |
| | | | Reduc | ing to | Test Wa | ves | | | |
| | | 6 | 1. | 94 | 1.06 | 0.16 | 3.16 | | |
| | | 10 14 | 2.: | | | 0.49 | 3.38 | | |
| | | 14 | 0.: | _ | | | - | - | |
| | | To | tal 4. | 30 | 1.06 | 1.92 | 7.28 | | |
| Wave Pe | eriod | Wave | Height | 00 | currenc | | / | - /D | 212 |
| sec | | - | ft | - | 1/0 | Sec | /Day | Waves/D | ay |
| | | 0 | btain N | umber c | of Waves | per Day | | | |
| 6 | 6 | | 4 | | 1.94 | | 676 | 279 | |
| 6 | | | 7 | | 1.06 | | 916 | 153 | |
| 6 | | | 10 | | 0.16 | | 138 | 23 | |
| 10 | | | 4 | | 2.11 | | 823 | 182 | |
| 10 | | | 10 | | 1.27 | | 097 | 110 | |
| 14 | | | 4 | | 0.25 | | 216 423 | 15 30 | |
| 14 | | | 10 | | 0.49 | | 423 | 20 | |

^{*} Zones are defined in Plate 3.

Table 20
Consolidation of Waves Approaching South Zone* from the East

| Wave Period | Pe | rcentage | e of To | tal Wav | | te per Wa | ave Heigh | | |
|-------------|--|----------|----------|---------|----------|-----------|-----------|----------|-------|
| sec | 1-3 | 3-5 | 5-7 | 7-9 | 9-11 | 11-13 | 13-15 | 15-17 | Total |
| | | Select | ted Por | tion of | East Wa | ave Clima | ate | | |
| 5-7 | 0.75 | 0.68 | 0.16 | 0.08 | 0.06 | 0.02 | 0 | 0 | 1.75 |
| 7-9 | 0.55 | 0.39 | 0.37 | 0.39 | 0.13 | 0.04 | 0.02 | 0.01 | 1.90 |
| 9-11 | 0.22 | 0.29 | 0.28 | 0.27 | 0.23 | 0.10 | 0.05 | 0.02 | 1.46 |
| 11-13 | 0.07 | 0.09 | 0.11 | 0.16 | 0.15 | 0.12 | 0.05 | 0.04 | 0.79 |
| 13-15 | 0.01 | 0.03 | 0.03 | 0.05 | 0.07 | 0.05 | 0.04 | 0.02 | 0.30 |
| -15 | 0 | 0 | 0.01 | 0.01 | 0.02 | 0.02 | 0.03 | 0.02 | 0.11 |
| Total | 1.60 | 1.48 | 0.96 | 0.96 | 0.66 | 0.35 | 0.19 | 0.11 | 6.31 |
| | | Elimin | nating ' | 7-9 Sec | Wave Pe | eriod Gro | oup | | |
| 5.7 | 7 02 | 0.88 | 0.34 | 0.27 | 0.12 | 0.04 | 0.07 | 0 | 2.69 |
| 5-7 | 0.49 | 0.48 | 0.47 | 0.47 | 0.30 | 0.12 | 0.01 | 0.03 | 2.42 |
| 9-11 | 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1 | | | 0.16 | 0.15 | 0.12 | 0.05 | 0.04 | 0.79 |
| 11-13 | 0.07 | 0.09 | 0.11 | | 0.07 | 0.05 | 0.04 | 0.02 | |
| 13-15 | 0.01 | 0.03 | 0.03 | 0.05 | | | | | 0.30 |
| >15 | 0 | 0 | 0.01 | 0.01 | 0.02 | 0.02 | 0.03 | 0.02 | 0.11 |
| Total | 1.60 | 1.48 | 0.96 | 0.96 | 0.66 | 0.35 | 0.19 | 0.11 | 6.31 |
| | Elim | inating | 11-13 | and >15 | Sec War | ve Period | d Groups | | |
| 5-7 | 1.03 | 0.88 | 0.34 | 0.27 | 0.12 | 0.04 | 0.01 | 0 | 2.69 |
| 9-11 | 0.53 | 0.53 | 0.53 | 0.55 | 0.38 | 0.18 | 0.09 | 0.05 | 2.84 |
| 13-15 | 0.04 | 0.07 | 0.09 | 0.14 | 0.16 | 0.13 | 0.09 | 0.06 | 0.78 |
| Total | 1.60 | 1.48 | 0.96 | 0.96 | 0.66 | 0.35 | 0.19 | 0.11 | 6.31 |
| | Wave | Period | | | Wave He | eight, ft | 5 | | |
| | | sec | = | 4 | _7_ | 10 | Total | | |
| | | | Redu | cing to | Test Wa | aves | | | |
| | | 6 | 1 | .91 | 0.61 | 0.17 | 2.69 | | |
| | | 10 | 1 | .59 | | 1.25 | 2.84 | | |
| | | 14 | 0 | .20 | | 0.58 | 0.78 | | |
| | | Te | otal 3 | .70 | 0.61 | 2.00 | 6.31 | | |
| Wave Pe | riod | Wave | Height | 0c | currence | e | | | _ |
| sec | | | ft | - | 76 | _ Sec | /Day | Waves/Da | ay |
| | | 0 | btain N | umber o | f Waves | per Day | | | |
| 6 | | | 4 | | 1.91 | | 650 | 275 | |
| 6 | | | 7 | | 0.61 | | 527 | 88 | |
| | | | 10 | | 0.17 | | 147 | 24 | |
| 10 | | | 4 | | 1.59 | | 374 | 138 | |
| 10 | | | 10 | | 1.25 | | 080 | 108 | |
| 14 | El- | | 4 | | 0.20 | | 173 | 12 | |
| 14 | | | 10 | | 0.58 | | 501 | 36 | |

^{*} Zones are defined in Plate 3.

Table 21
Consolidation of Waves Approaching South Zone* from the Southeast

| Wave | | | | | | | Wave Hei | ght Grou | |
|-------------|------|-----------|----------|---------|-----------|----------|------------|----------|-----------|
| Period, sec | 1-3 | 3-5 | 5-7 | 7-9 | 9-11 | 11-13 | 13-15 | 15-17 | Total |
| | 1 | Selected | Portio | on of S | outheast | t Wave C | limate | | |
| 5-7 | 0.75 | 0.53 | 0.18 | 0.24 | 0 | 0 | 0 | 0 | 1.70 |
| 7-9 | 0.42 | 0.50 | 0.35 | 0.31 | 0.19 | 0.03 | 0.01 | 0.02 | 1.83 |
| 9-11 | 0.23 | 0.27 | 0.29 | 0.27 | 0.26 | 0.10 | 0.02 | 0.01 | 1.45 |
| 11-13 | 0.07 | 0.05 | 0.09 | 0.16 | 0.17 | 0.08 | 0.03 | 0.02 | 0.67 |
| 13-15 | 0.03 | 0.04 | 0.03 | 0.05 | 0.05 | 0.06 | 0.04 | 0.02 | 0.32 |
| >15 | 0 | 0.01 | 0 | 0.01 | 0.02 | 0.02 | 0.02 | 0.01 | 0.09 |
| Total | 1.50 | 1.40 | 0.94 | 1.04 | 0.69 | 0.29 | 0.12 | 0.08 | 6.06 |
| | | Elimir | nating ' | 7-9 Sec | : Wave Pe | eriod Gr | oup | | |
| 5-7 | 0.96 | 0.78 | 0.35 | 0.39 | 0.09 | 0.01 | 0 | 0.01 | 2.59 |
| 9-11 | 0.44 | 0.52 | 0.47 | 0.43 | 0.36 | 0.12 | 0.03 | 0.02 | 2.39 |
| 11-13 | 0.07 | 0.05 | 0.09 | 0.16 | 0.17 | 0.08 | 0.03 | 0.02 | 0.67 |
| 13-15 | 0.03 | 0.04 | 0.03 | 0.05 | 0.05 | 0.06 | 0.04 | 0.02 | 0.32 |
| >15 | 0 | 0.01 | 0 | 0.01 | 0.02 | 0.02 | 0.02 | 0.01 | 0.09 |
| Total | 1.50 | 1.40 | 0.94 | 1.04 | 0.69 | 0.29 | 0.12 | 0.08 | 6.06 |
| | Elim | inating | 11-13 | and >15 | Sec War | ve Perio | d Groups | | |
| 5-7 | 0.96 | 0.78 | 0.35 | 0.39 | 0.09 | 0.01 | 0 | 0.01 | 2.59 |
| 9-11 | 0.48 | 0.55 | 0.52 | 0.51 | 0.45 | 0.16 | 0.04 | 0.03 | 2.74 |
| 13-15 | 0.06 | 0.07 | 0.07 | 0.14 | 0.15 | 0.12 | 0.08 | 0.04 | 0.73 |
| Total | 1.50 | 1.40 | 0.94 | 1.04 | 0.69 | 0.29 | 0.12 | 0.08 | 6,06 |
| | Wa | ve Perio | od | V | Vave Hei | ght, ft | | | |
| | _ | sec | = = | 4 | _7_ | _10_ | Total | | |
| | | | Reduc | ing to | Test War | ves | | | |
| | | 6 | 1 | .74 | 0.74 | 0.11 | 2.59 | | |
| | | 10 | | .55 | 201 | 1.19 | 2.74 | | |
| | | 14 | 0 | .20 | | 0.53 | 0.73 | | |
| | | Tot | tal 3 | .49 | 0.74 | 1.83 | 6.06 | | |
| Wave Period | | Wave He | eight | Oc | currenc | e | | | |
| sec | | ft | | - | % | - | Sec/Day | <u>r</u> | laves/Day |
| | | <u>Ob</u> | tain Nu | mber of | Waves | per Day | | | |
| 6 | | 4 | | | 1.74 | | 1,503 | | 250 |
| 6 | | 7 | | | 0.74 | | 639 | | 107 |
| 6 6 | | 10 | | | 0.11 | | 95 | | 16 |
| 10 | | 4 | | | 1.55 | | 1,339 | | 134 |
| | | 10 | | | 1.19 | | 1,028 | | 103 |
| 10 | | | | | | | | | |
| 14 | | 4 | | | 0.20 | | 173 458 | | 12 33 |

^{*} Zones are defined in Plate 3.

Table 22
Consolidation of Waves Approaching North Zone* from the South

| Vave Period | Pe | ercentag | e of Tot | tal Wav | e Clima | te per W | ave Hei | ght Group, | ft |
|-------------|-------|-------------|----------|----------|----------|-------------|---------|------------|-------|
| sec | 1-3 | 3-5 | 5-7 | 7-9 | 9-11 | 11-13 | 13-15 | 15-17 | Total |
| | Se | elected | Portion | of Nor | theast 1 | Wave Cli | mate | | |
| 5-7 | 1.50 | 0.65 | 0.45 | 0.12 | 0.04 | 0.04 | 0 | 0 | 2.80 |
| 7-9 | 0.70 | 0.80 | 0.60 | 0.45 | 0.11 | 0.04 | 0.05 | 0.04 | 2.79 |
| 9-11 | 0.38 | 0.37 | 0.43 | 0.38 | 0.30 | 0.11 | 0.03 | 0.03 | 2.03 |
| 11-13 | 0.10 | 0.16 | 0.16 | 0.18 | 0.19 | 0.10 | 0.10 | 0.05 | 1.04 |
| 13-15 | 0.02 | 0.01 | 0.06 | 0.06 | 0.06 | 0.08 | 0.05 | 0.04 | 0.38 |
| >15 | 0 | 0 | 0.01 | 0.03 | 0.03 | 0.03 | 0.02 | 0.02 | 0.14 |
| Total | 2.70 | 1.99 | 1.71 | 1.22 | 0.73 | 0.40 | 0.25 | 0.18 | 9.18 |
| | | Elimin | ating 7- | -9 Sec 1 | Wave Pe | riod Gro | up | | |
| 5-7 | 1.85 | 1.05 | 0.75 | 0.34 | 0.09 | 0.06 | 0.02 | 0.02 | 4.18 |
| 9-11 | 0.73 | 0.77 | 0.73 | 0.61 | 0.36 | 0.13 | 0.06 | 0.05 | 3.44 |
| 11-13 | 0.10 | 0.16 | 0.16 | 0.18 | 0.19 | 0.10 | 0.10 | 0.05 | 1.04 |
| 13-15 | 0.02 | 0.01 | 0.06 | 0.06 | 0.06 | 0.08 | 0.05 | 0.04 | 0.38 |
| >15 | 0 | 0 | 0.01 | 0.03 | 0.03 | 0.03 | 0.02 | 0.02 | 0.14 |
| Total | 2.70 | 1.99 | 1.71 | 1.22 | 0.73 | 0.40 | 0.25 | 0.18 | 9.18 |
| | Elimi | nating : | 11-13 ar | nd >15 | Sec Wave | e Period | Groups | | |
| 5-7 | 1.85 | 1.05 | 0.75 | 0.34 | 0.09 | 0.06 | 0.02 | 0.02 | 4.18 |
| 9-11 | 0.78 | 0.85 | 0.81 | 0.70 | 0.46 | 0.18 | 0.11 | 0.08 | 3.97 |
| 13-15 | 0.07 | 0.09 | 0.15 | 0.18 | 0.18 | 0.16 | 0.12 | 0.08 | 1.03 |
| Total | 2.70 | 1.99 | 1.71 | 1.22 | 0.73 | 0.40 | 0.25 | 0.18 | 9.18 |
| | | Wave Per | riod | | ave Hei | | | | |
| | | sec | _ | 10 | _14 | _ <u>To</u> | tal | | |
| | | | Reduci | ing to | Test War | ves | | | |
| | | 6 | | 4.18 | | 4. | 18 | | |
| | | 10 | | 3.69 | 0.2 | | 97 | | |
| | | 14 | | 0.75 | 0.2 | | 03 | | |
| | | | Total | 8.62 | 0.56 | 5 9. | 18 | | |
| Wave Per | iod | Wave | Height | 0eei | urrence | | | | |
| sec | | | ft | + | % | Sec/ | Day | Waves/Day | |
| | | <u>Ob</u> - | tain Num | nber of | Waves | per Day | | | |
| 6 | | | 10 | | 4.18 | | 12 | 602 | |
| 10 | | | 10 | | 3.69 | | 88 | 319 | |
| 10 | | | 14 | | 0.28 | | 42 | 24 | |
| 14 | | | 10 | | 0.75 | | 48 | 46 | |
| 14 | | | 14 | 1 | 0.28 | 9 | 42 | 17 | |

^{*} Zones are defined in Plate 3.

Table 23
Consolidation of Waves Approaching North Zone* from the Southeast

| Wave Period | | centage | | | | _ | ve Heigh | | ft |
|---------------|------|------------|-----------|---------|--------------|-------------------------|------------|------------|-------|
| sec | 1-3 | 3-5 | 5-7 | 7-9 | 9-11 | 11-13 | 13-15 | 15-17 | Total |
| | Se | elected 1 | Portion | of Sou | theast W | ave Cli | mate | | |
| 5-7 | 0.75 | 0.53 | 0.18 | 0.24 | 0 | 0 | 0 | 0 | 1.70 |
| 7-9 | 0.42 | 0.50 | 0.35 | 0.31 | 0.19 | 0.03 | 0.01 | 0.02 | 1.83 |
| 9-11 | 0.23 | 0.27 | 0.29 | 0.27 | 0.26 | 0.10 | 0.02 | 0.01 | 1.45 |
| 11-13 | 0.07 | 0.05 | 0.09 | 0.16 | 0.17 | 0.08 | 0.03 | 0.02 | 0.67 |
| 13-15 | 0.03 | 0.04 | 0.03 | 0.05 | 0.05 | 0.06 | 0.04 | 0.02 | 0.32 |
| -15 | 0 | 0.01 | 0 | 0.01 | 0.02 | 0.02 | 0.02 | 0.01 | 0.09 |
| Total | 1.50 | 1.40 | 0.94 | 1.04 | 0.69 | 0.29 | 0.12 | 0.08 | 6.06 |
| | | | | | Wave Per | | | | |
| | | | 101118 1- | 9 000 | wave rer | 100 010 | <u>ар</u> | | |
| 5-7 | 0.96 | 0.78 | 0.35 | 0.39 | 0.09 | 0.01 | 0 | 0.01 | 2.59 |
| 9-11 | 0.44 | 0.52 | 0.47 | 0.43 | 0.36 | 0.12 | 0.03 | 0.02 | 2.39 |
| 11-13 | 0.07 | 0.05 | 0.09 | 0.16 | 0.17 | 0.08 | 0.03 | 0.02 | 0.6 |
| 13-15 | 0.03 | 0.04 | 0.03 | 0.05 | 0.05 | 0.06 | 0.04 | 0.02 | 0.32 |
| -15 | 0 | 0.01 | 0 | 0.01 | 0.02 | 0.02 | 0.02 | 0.01 | 0.09 |
| Total | 1.50 | 1.40 | 0.94 | 1.04 | 0.69 | 0.29 | 0.12 | 0.08 | 6.06 |
| | Elin | ninating | 11-13 a | ind >15 | Sec Wav | e Perio | d Groups | | |
| 5-7 | 0.96 | 0.78 | 0.35 | 0.39 | 0.09 | 0.01 | 0 | 0.01 | 2.59 |
| | | | | | 0.45 | 0.16 | 0.04 | 0.03 | 2.71 |
| 9-11 13-15 | 0.48 | 0.55 | 0.52 | 0.51 | 0.15 | 0.12 | 0.08 | 0.04 | 0.73 |
| 13-17 | | - | _ | _ | | | - | - | - |
| Total | 1.50 | 1.40 | 0.94 | 1.04 | 0.69 | 0.29 | 0.12 | 0.08 | 6.00 |
| | | Wave Per | riod | | ave Heig | | | | |
| | | sec | | 10 | | To | tal | | |
| | | | Reducir | ig to T | est Wave | s | | | |
| | | 6 | | 2.59 | | 2 | .59 | | |
| | | 10 | | 2.59 | 0.15 | | .74 | | |
| | | 14 | | 0.55 | 0.18 | | .73 | | |
| | | | Total | 5.73 | 0.33 | 6 | .06 | | |
| | | | | | | | | | |
| Wave Per | iod | | Height | 0cc | urrence | Coa! | Dorr | Waves/Day | |
| sec | | | ft | - | 70 | Sec/ | <u>Day</u> | waves/Day | |
| | | <u>0</u> b | tain Num | ber of | Waves p | er Day | | | |
| 6 | | | 10 | 13 | 2.59 | 22 | | 373 | |
| | | | 10 | | 2.59 | 22 | 38 | 224 | |
| | | | | | 60 M T 187 W | | 30 | 13 | |
| | | | | | | | | | |
| | | | | | | | | | |
| | | <u>00</u> | tain Num | | | er Day 22 22 1 | 38 38 | 373 224 | |

^{*} Zones are defined in Plate 3.

Table 24

Determination of Number of Waves Approaching North Zone* from S22.5°E

| Wave Period sec | Wave Height ft | Waves per Day Southeast | y from Indicated | d Direction S22.5°E |
|-----------------------|----------------------|----------------------------|------------------|------------------------|
| 6 | 10 | 373 | 602 | 244 |
| 10 | 10 | 224 | 319 | 136 |
| 10 | 14 | 13 | 24 | 9 |
| 14 | 10 | 34 | 46 | 20 |
| 14 | 14 | 11 | 17 | 7 |

^{*} Zones are defined in Plate 3.

Table 25

Determination of Number of Waves Approaching South Zone* from E22.5°N

| Wave Period | Wave Height | Waves per Day | from Indicate | |
|----------------|----------------|---------------|---------------|---------|
| sec | ft | Northeast | East | E22.5°N |
| 6 | 4 | 279 | 275 | 139 |
| 6 | 7 | 153 | 88 | 60 |
| 6 | 10 | 23 | 24 | 12 |
| 10 | 14 | 182 | 138 | 80 |
| 10 | 10 | 110 | 108 | 55 |
| 14 | 4 | 15 | 12 | 7 |
| 14 | 10 | 30 | 36 | 17 |
| | | | | |

^{*} Zones are defined in Plate 3.

Table 26

Determination of Number of Waves Approaching South Zone* from E22.5°S

| Wave Period sec | Wave Height <u>ft</u> | Waves per East | Day from Indicated Southeast | Directions E22.5°S |
|-----------------------|-----------------------------|-------------------|------------------------------|-----------------------|
| 6 | 4 | 275 | 250 | 131 |
| 6 | 7 | 88 | 107 | 49 |
| 6 | 10 | 24 | 16 | 10 |
| 10 | 4 | 138 | 134 | 68 |
| 10 | 10 | 108 | 103 | 53 |
| 14 | 24 | 12 | 12 | 6 |
| 14 | 10 | 36 | 33 | 17 |

^{*} Zones are defined in Plate 3.

Table 27
Summary of Data Used in Determining Longshore Transport Rates in South Zone*

| | | | | | | Contract Con | ore Energy ot of Beach |
|-----------------------|----------------------|---------------------|---------------|--|------------------------|--|---|
| Test Period sec | Wave Height ft | t Breakwater Status | Waves per Day | Breaking Height Squared, ft ² | Transport Direction | Per Wave × 10 ⁴ ft-lb/ft | Per Wave Per Day × 10 ¹ 4 ft-lb/ft-day |
| | | Nor | theast Wave | DirectionS | lack Tide | | |
| 6 | 4 | Without | 209 | 11.50 | South | 0.365 | 76.29 |
| | | With | | 12.57 | South | 0.394 | 82.35 |
| 6 | 7 | Without | 115 | 30.91 | South | 1.277 | 146.86 |
| | | With | | 32.93 | South | 1.343 | 154.45 |
| 6 | 10 | Without | 17 | 98.19 | South | 4.492 | 76.36 |
| | | With | | 100.00 | South | 4.514 | 76.74 |
| 10 | 4 | Without | 137 | 22.85 | South | 1.134 | 155.36 |
| | | With | | 21.01 | South | 1.042 | 142.75 |
| 10 | 10 | Without | 83 | 128.24 | South | 11.596 | 962.47 |
| | | With | | 131.12 | South | 11.610 | 963.63 |
| 14 | 4 | Without | 11 | 59.19 | South | 4.655 | 51.21 |
| | | With | | 56.84 | South | 4.367 | 48.04 |
| 14 | 10 | Without | 23 | 197.41 | South | 22.933 | 527.46 |
| | | With | | 203.62 | South | 23.543 | 541.49 |
| | | E | 22.5°N Wave | DirectionSl | ack Tide | | |
| 6 | 4 | Without | 138 | 9.19 | South | 0.174 | 24.19 |
| | | With | | 7.37 | South | 0.124 | 17.24 |
| 6 | 7 | Without | 60 | 34.94 | South | 0.600 | 36.00 |
| | | With | | 22.25 | South | 0.421 | 25.26 |
| 6 | 10 | Without | 12 | 58.76 | South | 1.468 | 17.62 |
| | | With | | 62.16 | South | 1.386 | 16.63 |
| 10 | 4 | Without | 80 | 32.75 | South | 0.604 | 48.32 |
| | | With | | 31.48 | South | 0.641 | 51.28 |
| 10 | 10 | Without | 55 | 121.08 | South | 4.744 | 260.92 |
| | | With | | 114.12 | South | 4.044 | 222.42 |
| 14 | 4 | Without | 7 | 71.04 | South | 1.796 | 12.57 |
| | | With | | 53.25 | South | 1.066 | 7.46 |
| | | | (| Continued) | | | |

Note: Without means breakwater is not installed. With means breakwater is installed.

* Zones are defined in Plate 3. (Sheet 1 of 4)

| m- 1 | 7.7 | | | Dunaldina | | per Fo | ore Energy ot of Beach |
|---------------|----------------------|----------------------|---------------|--|------------------------|---|---|
| Period sec | Wave Height ft | Breakwater Status | Waves per Day | Breaking Height Squared, ft ² | Transport Direction | Per Wave × 10 ⁴ ft-lb/ft | Per Wave Per Day × 10 ⁴ ft-lb/ft-day |
| | | E22.5°N | Wave Direct | ionSlack Ti | de (Continu | (ed) | |
| 14 | 10 | Without | 17 | 191.87 | South | 9.486 | 161.26 |
| | | With | | 189.48 | South | 8.291 | 140.95 |
| | | | East Wave D | irectionSla | ck Tide | | |
| 6 | 4 | Without | 138 | 12.66 | South | 0.028 | 3.86 |
| | | With | | 15.93 | South | 0.039 | 5.38 |
| 6 | 7 | Without | 1,1, | 60.94 | South | 0.356 | 15.66 |
| | | With | | 40.25 | South | 0.274 | 12.06 |
| 6 | 10 | Without | 12 | 105.01 | South | 0.480 | 5.76 |
| | | With | | 64.77 | South | 0.292 | 3.50 |
| 10 | 4 | Without | 69 | 42.65 | South | 0.350 | 24.15 |
| | | With | | 24.65 | South | 0.214 | 14.77 |
| 10 | 10 | Without | 54 | 249.83 | South | 2.517 | 135.92 |
| | | With | | 148.90 | South | 1.426 | 77.00 |
| 14 | 4 | Without | 6 | 86.90 | North | 0.305 | 1.83 |
| | | With | | 57.22 | South | 0.425 | 2.55 |
| 14 | 10 | Without | 18 | 375.31 | South | 2.363 | 42.53 |
| | | With | | 204.04 | South | 1.257 | 22.63 |
| | | 1 | East Wave D | irectionFloo | od Tide | | |
| 6 | 4 | Without | 138 | 20.70 | South | 0.009 | 1.24 |
| | | With | | 14.28 | South | 0.105 | 14.49 |
| 6 | 7 | Without | 44 | 57.98 | South | 0.398 | 17.51 |
| | | With | | 35.49 | South | 0.195 | 8.58 |
| 6 | 10 | Without | 12 | 101.92 | South | 1.079 | 12.95 |
| | | With | | 65.04 | South | 0.012 | 0.14 |
| 10 | 4 | Without | 69 | 39.57 | South | 0.515 | 35.54 |
| | | With | | 28.88 | South | 0.224 | 15.46 |
| 10 | 10 | Without | 54 | 220.67 | South | 3.191 | 172.31 |
| | | With | | 134.23 | South | 0.935 | 50.49 |
| | | | | (Continued) | | | |

| | | | | | | | ore Energy ot of Beach |
|-----------------------|----------------------|----------------------|--------------|--|------------------------|----------|---|
| Test Period sec | Wave Height ft | Breakwater Status | Waves per | Breaking Height Squared, ft ² | Transport Direction | Per Wave | Per Wave Per Day × 10 ⁴ ft-lb/ft-day |
| | | East W | Nave Directi | onFlood Tid | le (Continue | ed) | |
| 14 | 4 | Without | 6 | 96.27 | South | 0.029 | 0.17 |
| | | With | | 54.19 | South | 0.399 | 2.39 |
| 14 | 10 | Without | 18 | 303.78 | South | 2.489 | 44.80 |
| | | With | | 196.86 | South | 2.846 | 51.23 |
| | | | East Wave | DirectionEl | ob Tide | | |
| 6 | 14 | Without | 138 | 26.33 | South | 0.095 | 13.11 |
| | | With | | 17.64 | South | 0.032 | 4.42 |
| 6 | 7 | Without | 44 | 73.40 | South | 0.591 | 26.00 |
| | | With | | 36.93 | South | 0.014 | 0.62 |
| 6 | 10 | Without | 12 | 115.71 | South | 0.869 | 10.43 |
| | | With | | 65.93 | South | 0.351 | 4.21 |
| 10 | 4 | Without | 69 | 42.94 | North | 0.293 | 20.22 |
| | | With | | 22.53 | South | 0.098 | 6.76 |
| 10 | 10 | Without | 54 | 218.03 | South | 1.910 | 103.14 |
| | | With | | 115.74 | South | 1.044 | 56.38 |
| 14 | 14 | Without | 6 | 114.04 | North | 0.907 | 5.44 |
| | | With | | 61.45 | North | 0.233 | 1.40 |
| 14 | 10 | Without | 18 | 355.14 | South | 7.501 | 135.02 |
| | | With | | 189.76 | South | 5.007 | 90.13 |
| | | E | 22.5°S Wave | DirectionS | lack Tide | | |
| 6 | 4 | Without | 131 | 17.20 | North | 0.253 | 33.14 |
| | | With | | 20.11 | North | 0.286 | 37.47 |
| 6 | 7 | Without | 49 | 48.63 | North | 1.004 | 49.20 |
| | | With | | 46.46 | North | 0.992 | 48.61 |
| 6 | 10 | Without | 10 | 94.46 | North | 1.957 | 19.57 |
| 0 | | With | 7.5 | 85.87 | North | 1.816 | 18.16 |
| | | | | (Continued) | | | |

| | | | | | | Longshore Energy per Foot of Beach | | |
|-----------------------|----------------------|----------------------|---------------|-----------------------------------|------------------------|---|---|--|
| Test Period sec | Wave Height ft | Breakwater Status | Waves per Day | Breaking Height Squared,ft2 | Transport Direction | Per Wave × 10 ⁴ ft-lb/ft | Per Wave Per Day × 10 ⁴ ft-1b/ft-day | |
| | | E22.5°S | Wave Direct | ionSlack Ti | de (Continu | ed) | | |
| 10 | 4 | Without | 68 | 30.94 | North | 0.581 | 39.51 | |
| | | With | | 29.07 | North | 0.566 | 38.49 | |
| 10 | 10 | Without | 53 | 170.65 | North | 6.958 | 368.77 | |
| | | With | | 170.92 | North | 7.017 | 371.90 | |
| 14 | 4 | Without | 6 | 77.13 | North | 3.255 | 19.53 | |
| | | With | | 78.32 | North | 3.373 | 20.24 | |
| 14 | 10 | Without | 17 | 240.37 | North | 17.638 | 299.85 | |
| | | With | | 228.16 | North | 17.519 | 297.82 | |
| | | Sou | theast Wave | DirectionS | lack Tide | | | |
| 6 | 4 | Without | 188 | 27.02 | North | 0.779 | 146.45 | |
| | | With | | 26.21 | North | 0.765 | 143.82 | |
| 6 | 7 | Without | 80 | 50.39 | North | 1.869 | 149.52 | |
| | | With | | 57.21 | North | 2.092 | 167.36 | |
| 6 | 10 | Without | 12 | 88.34 | North | 3.420 | 41.04 | |
| | | With | | 101.02 | North | 3.988 | 47.86 | |
| 10 | 4 | Without | 101 | 40.35 | North | 1.991 | 201.09 | |
| | | With | | 44.53 | North | 2.443 | 246.74 | |
| 10 | 10 | Without | 77 | 153.59 | North | 11.375 | 875.88 | |
| | | With | | 164.84 | North | 12.051 | 927.93 | |
| 14 | 14 | Without | 9 | 85.27 | North | 7.626 | 68.63 | |
| | | With | | 85.77 | North | 7.699 | 69.29 | |
| 14 | 10 | Without | 25 | 255.16 | North | 30.778 | 769.45 | |
| | | With | | 246.61 | North | 30.465 | 761.63 | |

Table 28
Summary of Data Used in Determining Longshore Transport Rates in North Zone*

| | | | | | | | ore Energy ot of Beach |
|-----------------------|----------------------|----------------------|--------------|--|------------------------|---|---|
| Test Period sec | Wave Height ft | Breakwater Status | Waves per | Breaking Height Squared, ft ² | Transport Direction | Per Wave × 10 ⁴ ft-lb/ft | Per Wave Per Day × 104 ft-1b/ft-day |
| | | Sou | theast Wave | DirectionS | lack Tide | | |
| 6 | 10 | Without | 280 | 88.81 | North | 1.439 | 402.92 |
| | | With | | 94.29 | North | 1.477 | 413.56 |
| 10 | 10 | Without | 168 | 141.66 | North | 3.877 | 651.34 |
| | | With | | 125.66 | North | 3.949 | 663.43 |
| 10 | 14 | Without | 10 | 267.82 | North | 10.543 | 105.43 |
| | | With | | 257.88 | North | 9.543 | 95.43 |
| 14 | 10 | Without | 26 | 169.24 | North | 5.934 | 154.28 |
| | | With | | 169.44 | North | 5.930 | 154.18 |
| 14 | 14 | Without | 8 | 270.80 | North | 15.694 | 125.55 |
| | | With | | 269.04 | North | 16.858 | 134.86 |
| | | St | 22.5°E Wave | DirectionSI | lack Tide | | |
| 6 | 10 | Without | 244 | 80.64 | North | 2.711 | 661.48 |
| - | | With | | 80.64 | North | 2.711 | 661.48 |
| 10 | 10 | Without | 136 | 172.14 | North | 11.428 | 1554.21 |
| - | | With | | 172.93 | North | 11.512 | 1565.63 |
| 10 | 14 | Without | 9 | 264.67 | North | 20.638 | 185.74 |
| 10.7 | | With | | 332.08 | North | 25.280 | 227.52 |
| 14 | 10 | Without | 20 | 153.54 | North | 12.714 | 254.27 |
| - | | With | | 172.60 | North | 14.032 | 280.64 |
| 14 | 14 | Without | 7 | 370.40 | North | 43.196 | 302.37 |
| -, | - | With | | 280.80 | North | 32.127 | 224.89 |
| | | | South Wave I | DirectionSl | ack Tide | | |
| 6 | 10 | Without | 452 | 65.62 | North | 2.435 | 1100.62 |
| 0 | 10 | With | 7,25 | 45.88 | North | 1.886 | 852.47 |
| 10 | 30 | | 239 | 99.41 | North | 5.442 | 1300.64 |
| 10 | 10 | Without With | 237 | 70.08 | North | 3.900 | 932.10 |
| | | HT OT | | (Continued) | - | - | - |

Note: Without means breakwater is not installed. With means breakwater is installed. * Zones are defined in Plate 3.

| | | | | | | | ore Energy ot of Beach |
|-----------------------|----------------------|----------------------|--------------|-----------------------------------|------------------------|---|---|
| Test Period sec | Wave Height ft | Breakwater Status | Waves per | Breaking Height Squared, ft | Transport Direction | Per Wave × 10 ⁴ ft-lb/ft | Per Wave Per Day × 104 ft-lb/ft-day |
| | | South W | ave Directi | onSlack Tid | e (Continue | <u>d)</u> | |
| 10 | 14 | Without | 18 | 229.19 | North | 14.620 | 263.16 |
| | | With | | 165.58 | North | 11.481 | 206.66 |
| 14 | 10 | Without | 35 | 169.82 | North | 19.874 | 695.59 |
| | | With | | 140.69 | North | 16.583 | 580.41 |
| 14 | 14 | Without | 13 | 228.74 | North | 24.993 | 324.91 |
| | | With | | 198.26 | North | 18.208 | 236.70 |
| | | S | outh Wave D | irectionFlo | od Tide | | |
| 6 | 10 | Without | 452 | 52.41 | North | 1.671 | 755.29 |
| | | With | | 31.87 | North | 1.161 | 524.77 |
| 10 | 10 | Without | 239 | 98.52 | North | 6.540 | 1563.06 |
| | | With | | 84.49 | North | 6.263 | 1496.86 |
| 10 | 14 | Without | 18 | 283.83 | North | 22.487 | 404.77 |
| | | With | | 226.17 | North | 18.207 | 327.73 |
| 14 | 10 | Without | 35 | 141.76 | North | 13.522 | 473.27 |
| | | With | | 128.04 | North | 11.082 | 387.87 |
| 14 | 14 | Without | 13 | 172.52 | North | 20.185 | 262.41 |
| | | With | | 144.06 | North | 17.397 | 226.16 |
| | | 5 | South Wave I | DirectionEb | b Tide | | |
| 6 | 10 | Without | 452 | 35.72 | North | 1.176 | 531.55 |
| 8 | | With | | 42.89 | North | 1.378 | 622.86 |
| 10 | 10 | Without | 239 | 122.47 | North | 9.006 | 2152.43 |
| | | With | | 126.23 | North | 8.804 | 2104.16 |
| 10 | 14 | Without | 18 | 203.47 | North | 16.658 | 299.84 |
| | | With | | 203.37 | North | 17.501 | 315.02 |
| 14 | 10 | Without | 35 | 131.61 | North | 11.598 | 405.93 |
| | | With | - | 138.88 | North | 10.434 | 365.19 |
| 14 | 14 | Without | 13 | 220.89 | North | 26.092 | 339.20 |
| | | With | | 211.09 | North | 20.575 | 267.48 |

Table 29 Longshore Transport Rates for South and North Zones*

| | | | Per Fo | | Aver | | Manus | Protection Equation | | | ell Equation | | | n Equation | |
|-------------------|--------------------|------------------------|-----------------------------------|------------------|---------------------|--|-------------------|---------------------|----------|-------------------|----------------------|-------------|-------------------|------------------|------|
| | | | Beach F × 10 ⁶ ft-1 | | Breaking Squared | and the second s | | yd3/day | | | Transport yd3/day | | | ransport yd3/day | |
| Wave Direction | Tidal Condition | Transport Direction | Breakwater Out | Breakwater In | Breakwater Out | Breakwater In | Breakwater Out | Breakwater In | ΔQ** | Breakwater Out | Breakwater In | ΔQ** - % | Breakwater Out | Breakwater In | ΔQ** |
| | | | | | | <u> </u> | South Zone* | | | | | | | | |
| Northeast | Slack | South | 19.960 | 20.095 | 44.69 | 45.69 | 2373 | 2389 | +1 | 2303 | 2316 | +1 | 24,000 | 25,000 | + 2, |
| E22.5°N | Slack | South | 5.609 | 4.812 | 46.26 | 41.88 | 667 | 572 | -14 | 834 | 738 | -12 | 25,000 | 23,000 | -8 |
| East | Slack | South | 2.261 | 1.379 | 86.21 | 54.26 | 269 | 164 | -39 | 403 | 272 | -33 | 47,000 | 30,000 | -36 |
| East | Flood | South | 2.845 | 1.428 | 80.13 | 51.09 | 338 | 170 | -50 | 485 | 279 | -42 | 44,000 | 28,000 | -36 |
| East | Ebb | South | 2,620 | 1.611 | 88.17 | 48.21 | 312 | 192 | -38 | 454 | 308 | -32 | 48,000 | 26,000 | -46 |
| E22.5°S | Slack | North | 8.296 | 8.327 | 63.71 | 63.34 | 986 | 990 | 0 | 1141 | 1144 | 0 | 35,000 | 35,000 | Ö |
| Southeast | Slack | North | 22.521 | 23.646 | 67.52 | 70.82 | 2678 | 2812 | +5 | 2537 | 2638 | +4 | 37,000 | 39,000 | +5 |
| | | | | | | Ī | North Zone* | | | | | | | | |
| Southeast | Slack | North | 14.395 | 14.615 | 117.70 | 115.14 | 1712 | 1738 | +2 | 1773 | 1795 | +1 | 64,000 | 63,000 | -2 |
| S22.5°E | Slack | North | 29.581 | 29.602 | 122.92 | 124.04 | 3517 | 3520 | 0 | 3155 | 3157 | 0 | 67,000 | 68,000 | +1 |
| South | Slack | North | 36.849 | 28.083 | 87.80 | 63.37 | 4381 | 3339 | -24 | 3761 | 3027 | -20 | 48,000 | 35,000 | -27 |
| South | Flood | North | 34.588 | 29.634 | 78.66 | 59.48 | 4113 | 3523 | -14 | 3576 | 3160 | -12 | 43,000 | 33,000 | -23 |
| South | Ebb | North | 37,290 | 36.747 | 74.71 | 80.34 | 4434 | 4369 | -1 | 3797 | 3753 | -1 | 41,000 | 44,000 | +7 |
| | | | | | | | | | | | | | | | |

^{*} Zones are defined in Plate 3.

** AQ = (transport rate out transport rate out)(100).

Table 30
Changes in Longshore Transport Rates for South and North Zones*

| | | Longshor Per Fo | e Energy ot of | | Average | | E | otection Manu quation | ıal | |
|------------------------|-------|----------------------------------|---------------------|---------------|------------------------------|---|---------|--------------------------------------|------|--|
| | | Beach F × 10 ⁶ ft- | er Day lb/ft-day | | Breaking Height Squared, ft2 | | | Longshore Transport Rate, yd3/day | | |
| Transport Direction | Zone* | Breakwater Out | Breakwater In | Breakw Out | | | out Out | Breakwater In | ΔQ*: | |
| South | South | 28.066 | 26.356 | 55. | 71 46 | .25 | 3337 | 3134 | -6 | |
| North | South | 30.817 | 31.973 | 65. | 98 67 | .80 | 3664 | 3801 | +4 | |
| North | North | 80.370 | 74.854 | 102. | 88 95 | .31 | 9556 | 8900 | -7 | |
| | | Longshore Rate, y | | | Longshore | vin Equation Transport yd ³ /day | i | - | | |
| | | Breakwater Out | Breakwater In | ΔQ** | Breakwater Out | | er ΔQ*: | * | | |
| South | South | 3025 | 2877 | -5 | 31,000 | 25,000 | -19 | | | |
| North | South | 3260 | 3358 | +3 | 36,000 | 37,000 | +3 | | | |
| North | North | 7019 | 6613 | -6 | 56,000 | 52,000 | -7 | | | |

^{*} Zones are defined in Plate 3.

^{**} AQ = (transport rate - transport rate out/transport rate out)(100).

Table 31 Comparison of Test Series III Current Measurements

| | Test | Wave | Breakwa | ter Out | Breakw | ater In | | |
|-------------------|--------------------------------|-------------------------------------|--|--|--|--|---|--|
| Wave Direction | Period sec | Heightft | Velocity fps | Direction of Flow | Velocity fps | Direction of Flow | Δ Velocity*fps | Δ Velocity** |
| | | | | South | Zonet | | | |
| Northeast | 6 6 10 10 14 14 | 4 7 10 4 10 4 | 0.83 0.75 0.73 0.73 0.32 0.63 0.63 | South South South South South South South | 0.80 0.69 0.69 0.79 0.38 0.58 0.65 | South South South South South South South | -0.03 -0.06 -0.04 +0.06 +0.06 -0.05 +0.02 | -4 -8 -5 +8 +19 -8 +3 |
| E22.5°N | 6 6 10 10 14 14 | 4 7 10 4 10 4 | 0.61 0.95 1.21 0.61 1.21 1.21 0.78 | South South South South South South South | 0.61 1.21 1.21 0.43 1.73 1.21 1.21 | South South South South South South South | 0 +0.26 0 -0.18 +0.52 0 +0.43 | 0 +27 0 -30 +43 0 +55 |
| E22.5°S | 6 6 10 10 14 14 | 4 7 10 4 10 4 10 | 1.15 1.88 1.49 1.48 1.74 1.83 2.13 | North North North North North North | 1.07 1.88 1.60 1.40 1.76 2.04 2.04 | North North North North North North | -0.08 0 +0.11 -0.08 +0.02 +0.21 -0.09 | -7 0 +7 -5 +1 +11 |
| Southeast | 6 6 10 10 14 14 | 14 7 10 4 10 4 10 | 1.97 1.77 1.22 1.97 1.54 1.52 1.27 | North North North North North North | 2.09 1.65 1.32 2.12 1.70 1.42 1.12 | North North North North North North | +0:12 -0.12 +0.10 +0.15 +0.16 -0.10 -0.15 | +6 -7 +8 +8 +10 -7 -12 |
| | | | | Nort | h Zonet | | | |
| Southeast | 6 10 10 14 14 | 10 10 14 10 14 | 1.92 2.33 3.53 2.24 3.33 | North North North North | 1.83 2.06 3.74 2.38 3.13 | North North North North North | -0.09 -0.27 +0.21 +0.14 -0.20 | -5 -12 +6 +6 -6 |
| S22.5°E | 6 10 10 14 14 | 10 10 14 10 14 | 1.86 2.89 2.69 2.69 2.84 | North North North North | 1.59 3.04 2.73 2.53 2.71 | North North North North | -0.27 +0.15 +0.04 -0.16 -0.13 | -15 +5 +1 -6 -5 |

^{*} Δ velocity (fps) = velocity - velocity out. ** Δ velocity (%) = [(velocity - velocity out)/velocity out)] (100).

⁺ Zones are defined in Plate 3.



Photo 1. Setting templates and finishing concrete during model construction

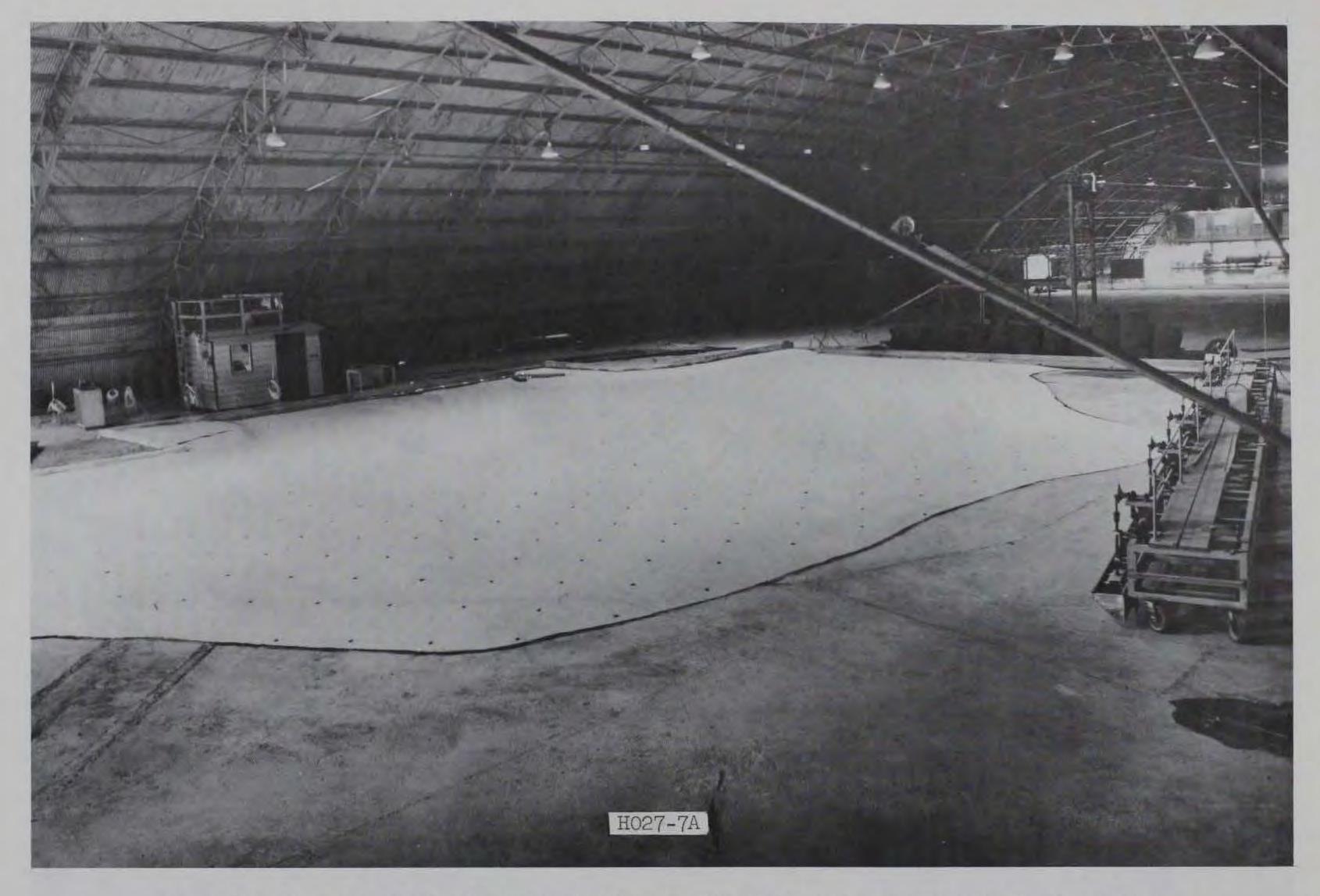


Photo 2. General view of model looking north with wave generator on the right and instrumentation building on the left

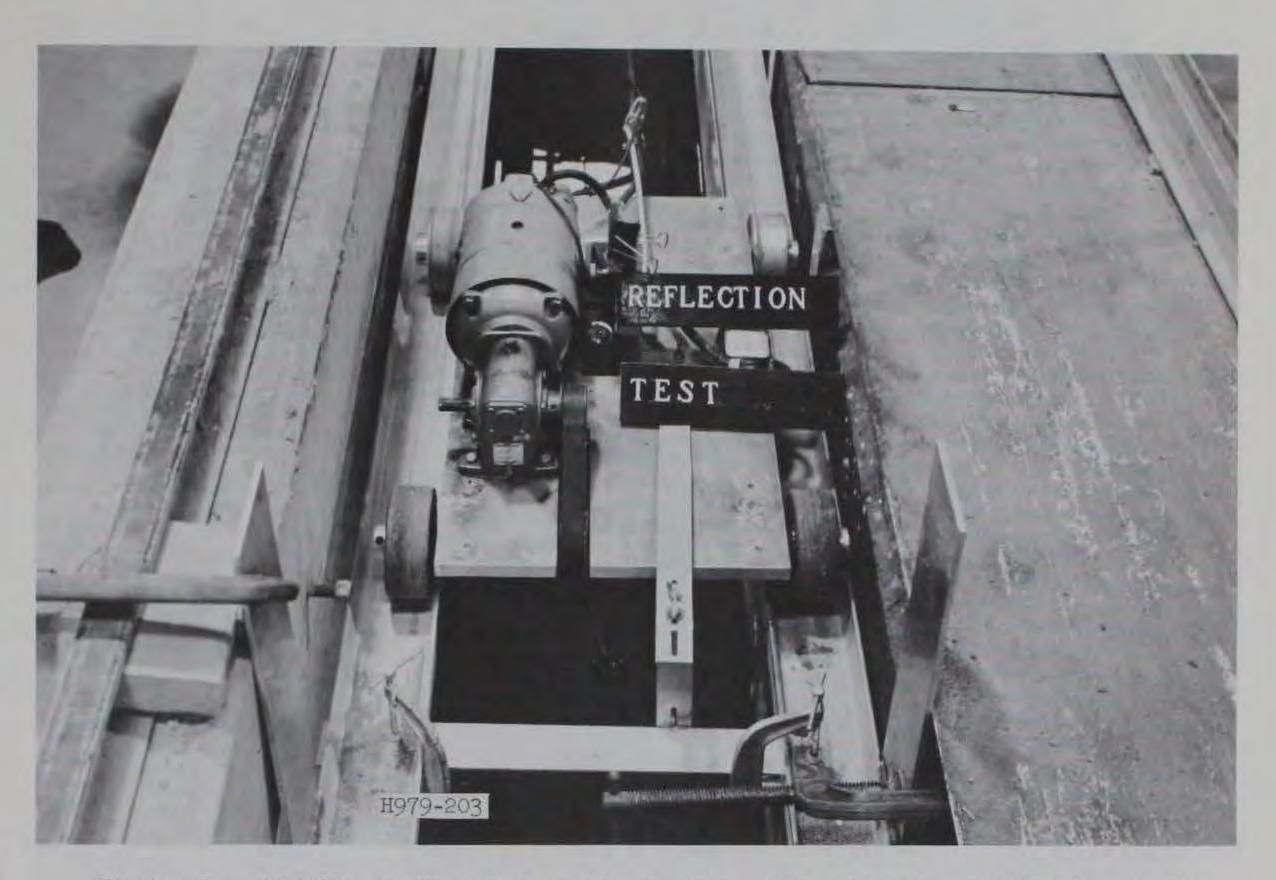


Photo 3. Mobile wave gage used in two-dimensional reflection tests



Photo 4. Recording equipment used in measuring wave heights



Photo 5. Test series I, south wave direction, slack tide, 6-sec wave period, 10-ft wave height

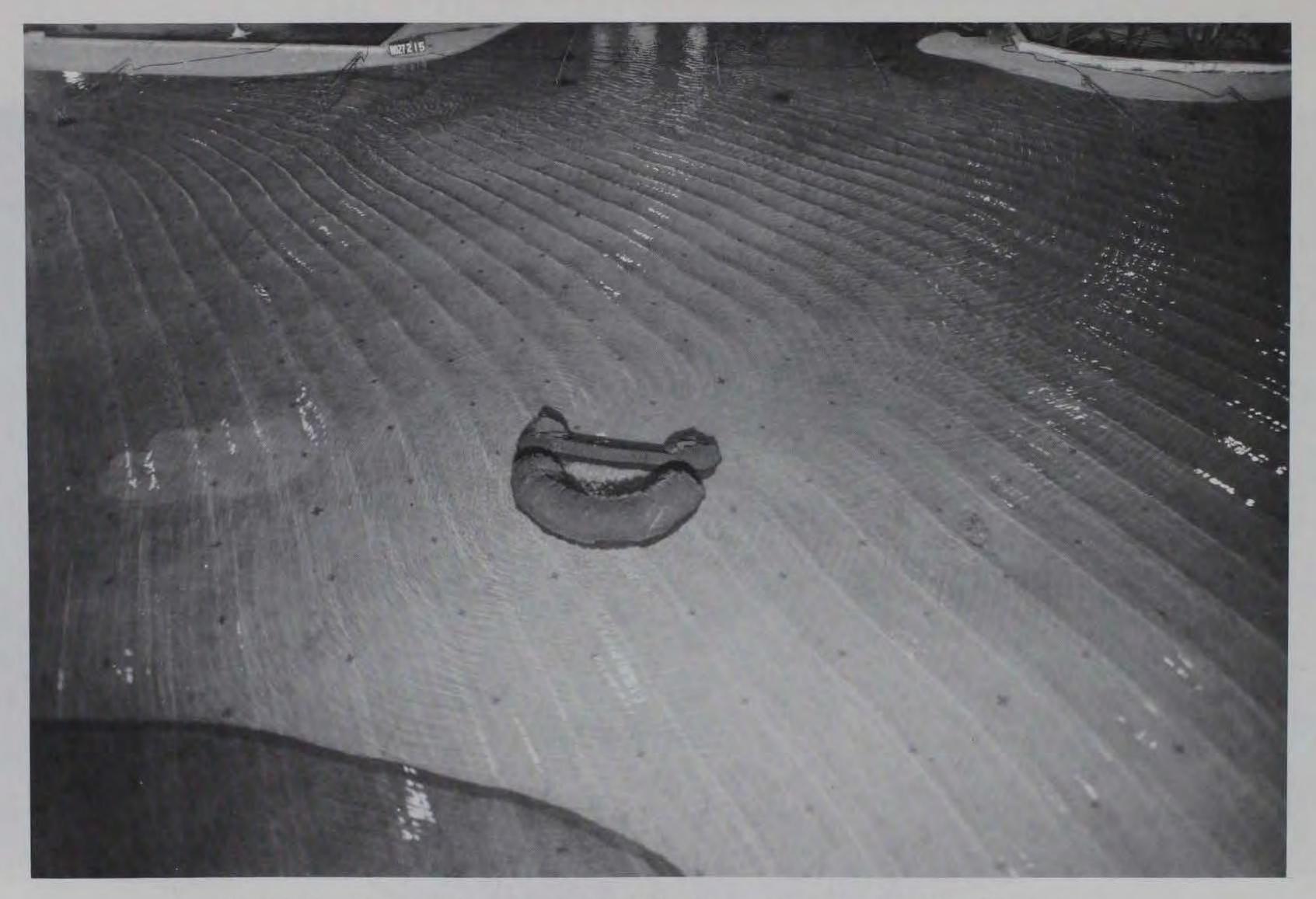


Photo 6. Test series I, south wave direction, slack tide, 6-sec wave period, 10-ft wave height, proposed breakwater installed

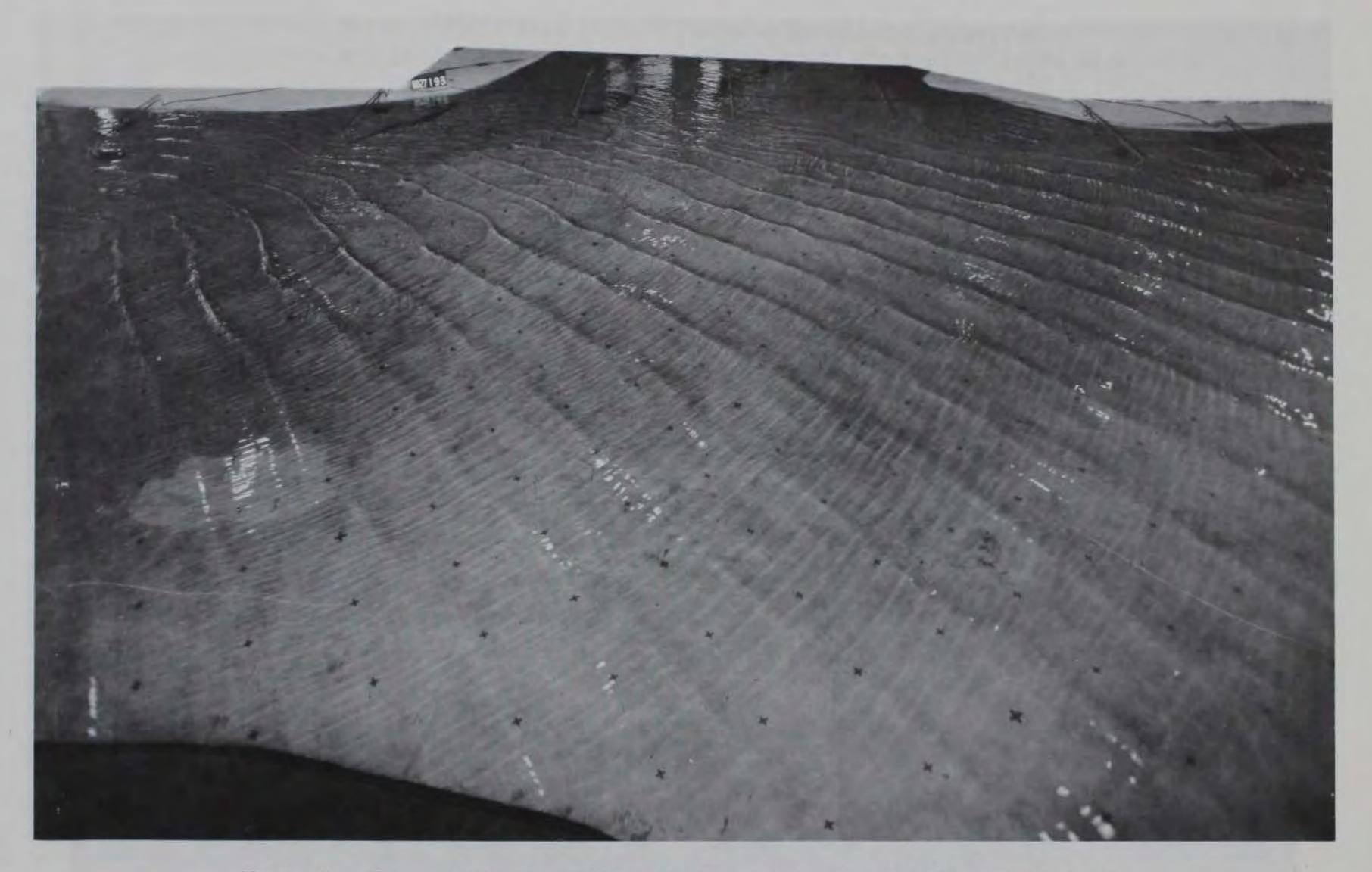


Photo 7. Test series I, south wave direction, flood tide, 10-sec wave period, 10-ft wave height

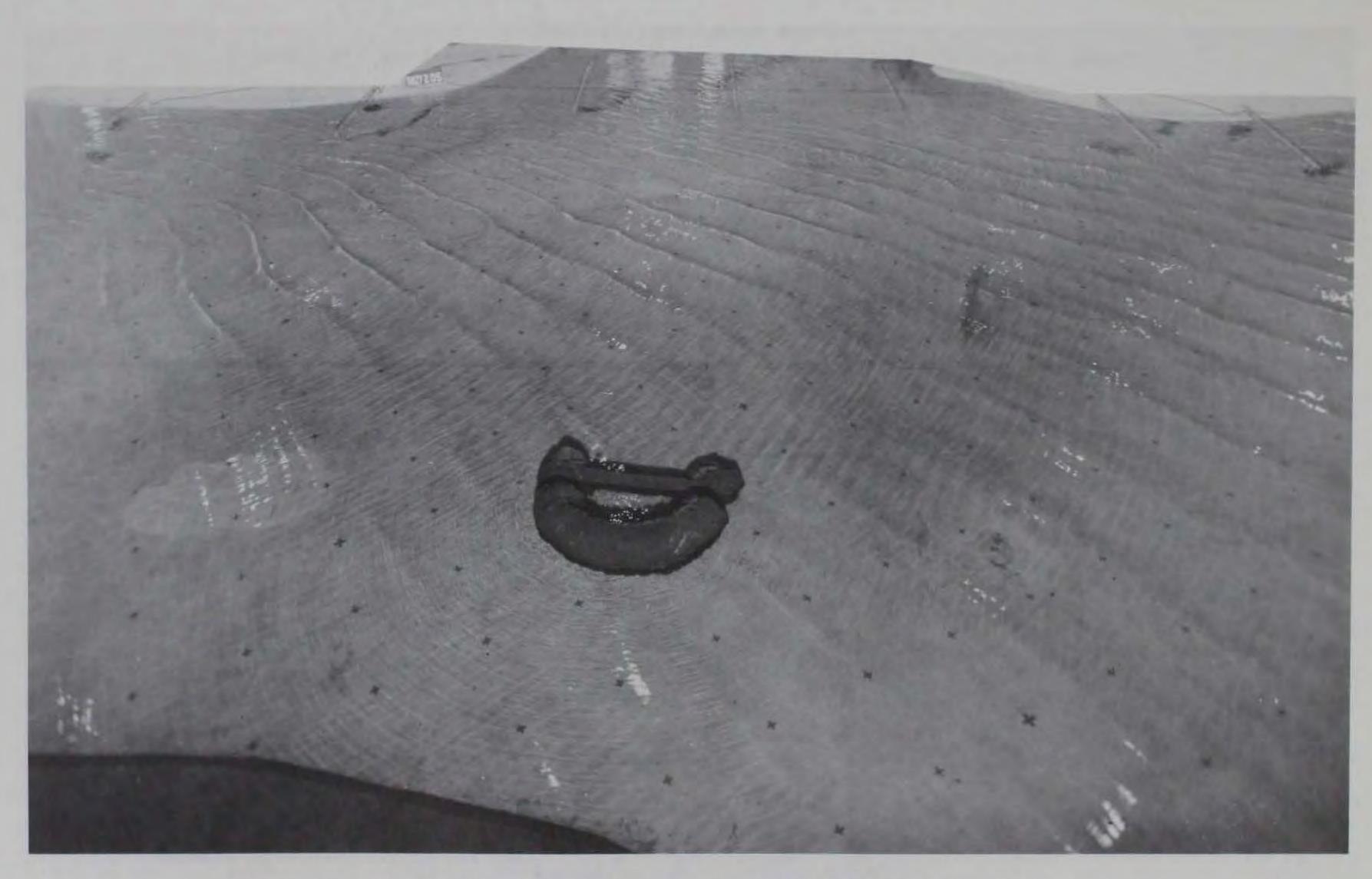


Photo 8. Test series I, south wave direction, flood tide, 10-sec wave period, 10-ft wave height, proposed breakwater installed



Photo 9. Test series I, south wave direction, ebb tide, 14-sec wave period, 18-ft wave height

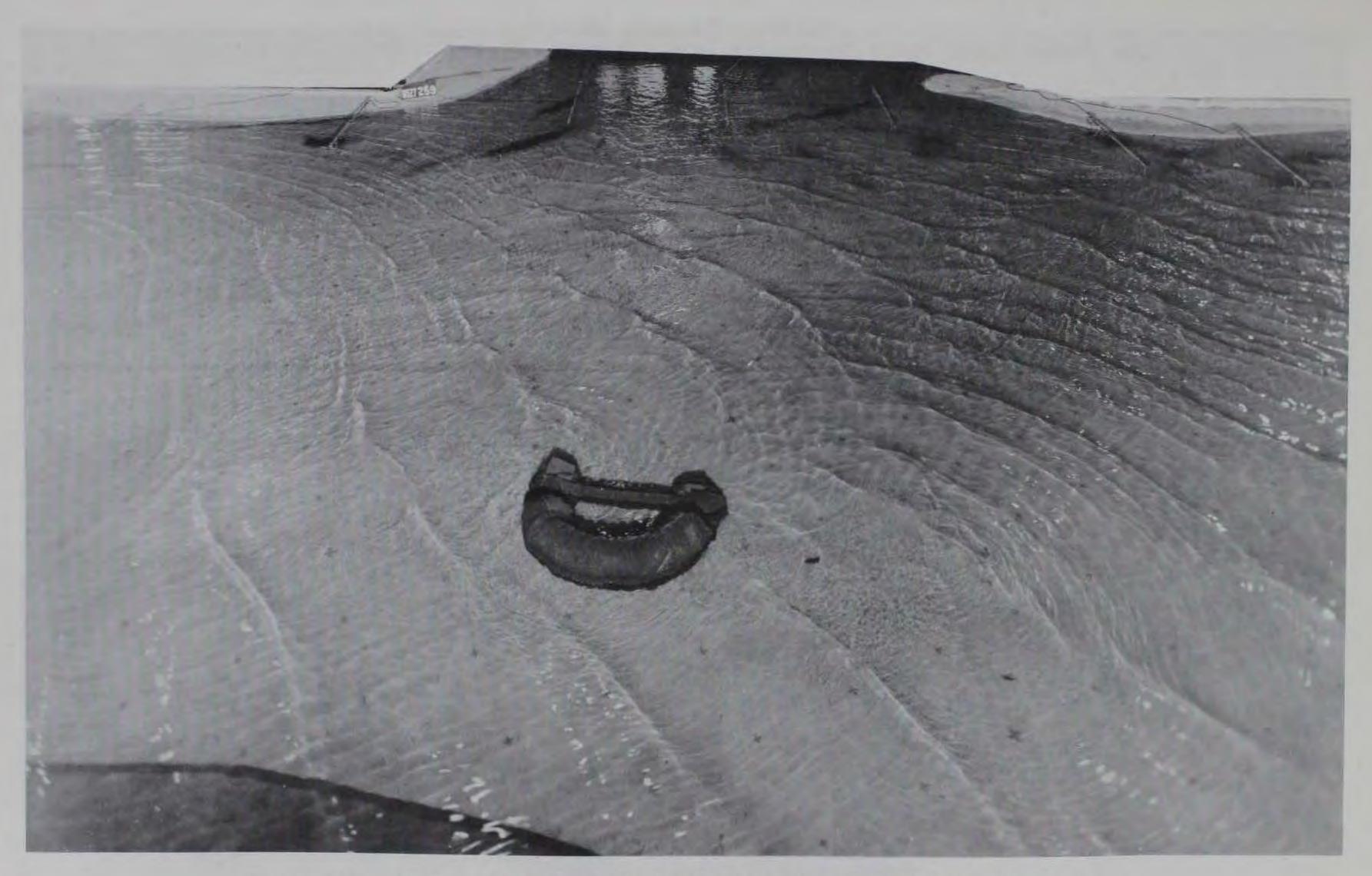


Photo 10. Test series I, south wave direction, ebb tide, 14-sec wave period, 18-ft wave height, proposed breakwater installed



Photo 11. Test series I, southeast wave direction, slack tide, 10-sec wave period, 4-ft wave height

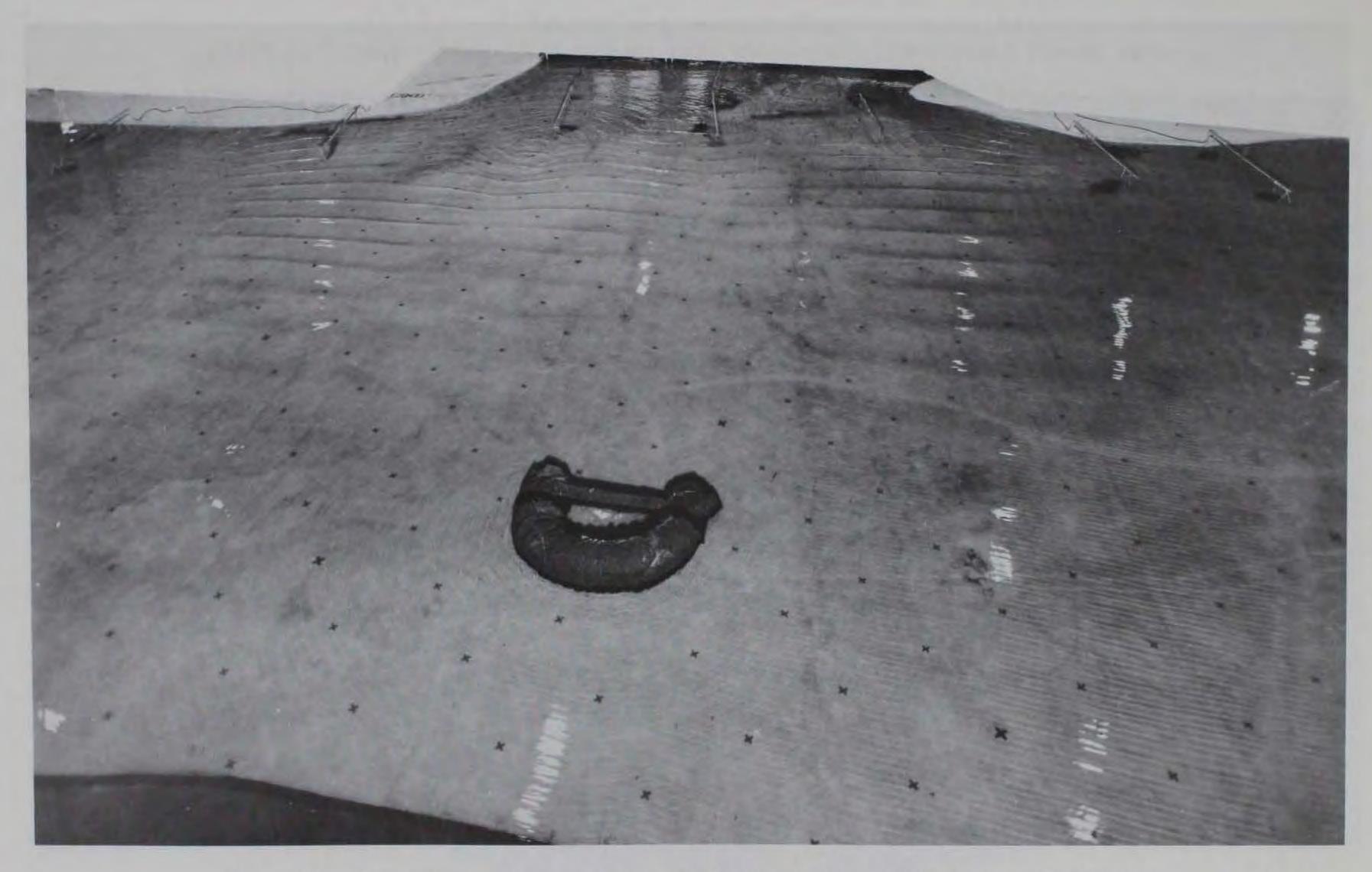


Photo 12. Test series I, southeast wave direction, slack tide, 10-sec wave period, 4-ft wave height, proposed breakwater installed

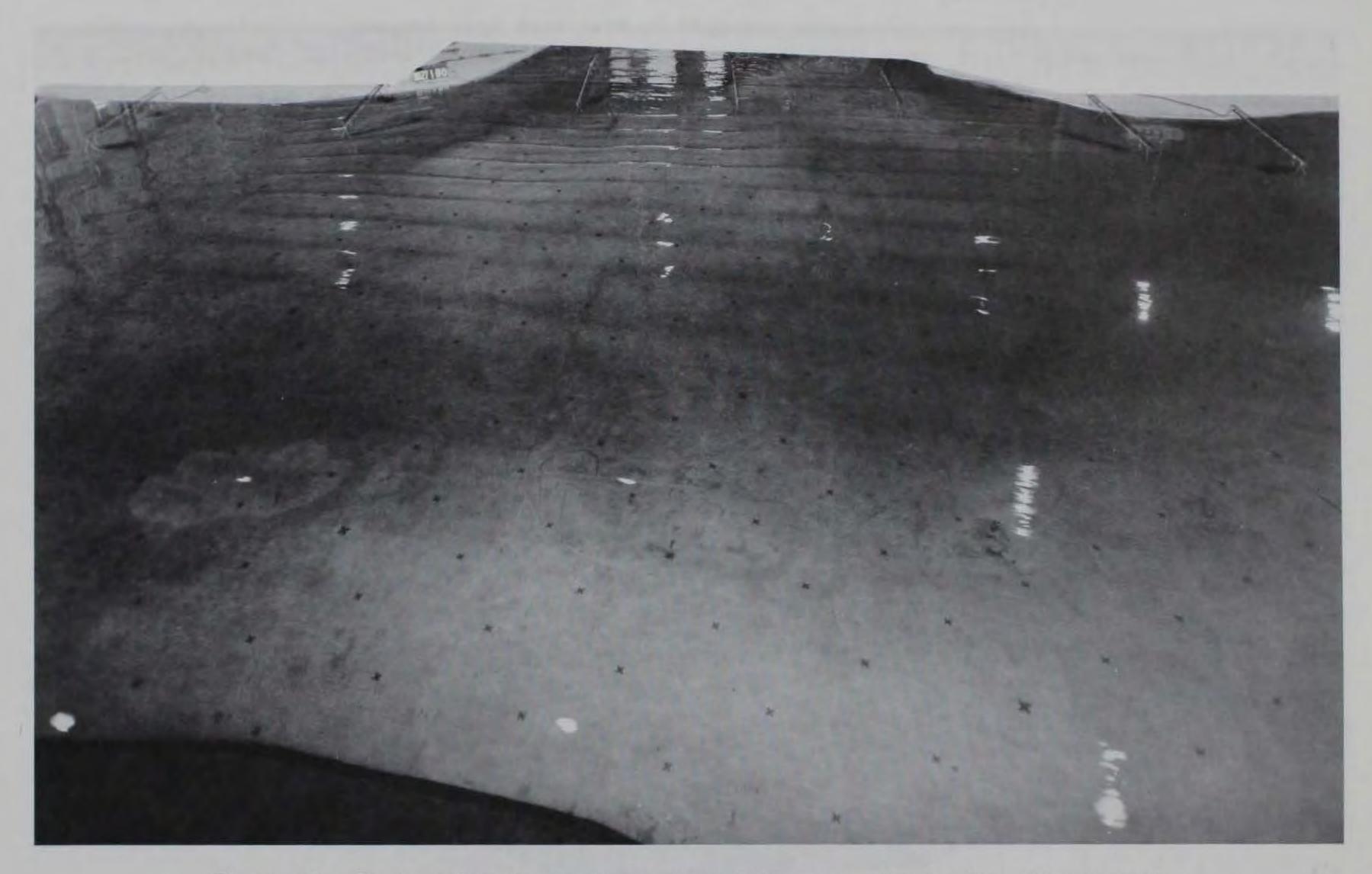


Photo 13. Test series I, southeast wave direction, flood tide, 10-sec wave period, 4-ft wave height

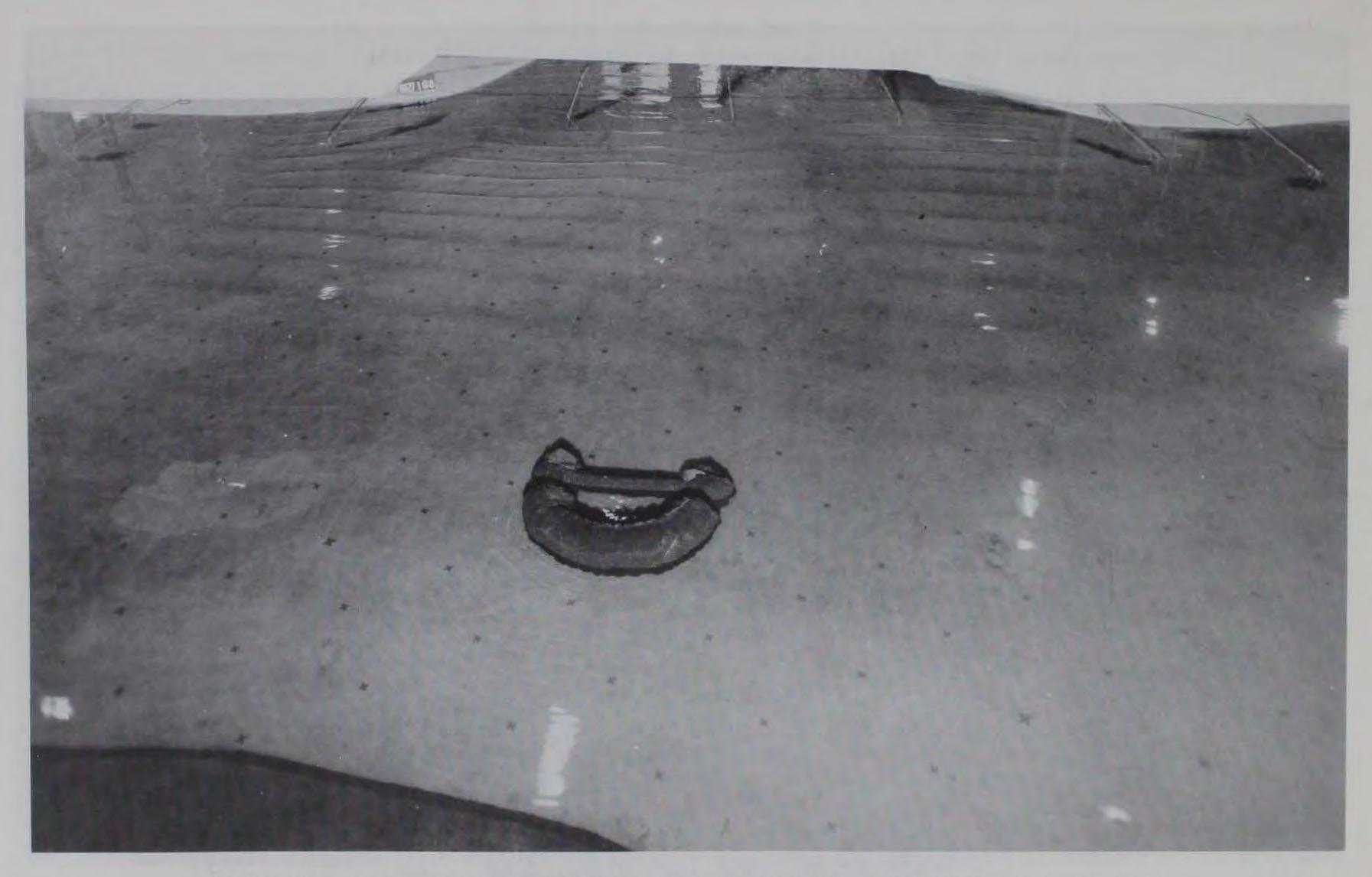


Photo 14. Test series I, southeast wave direction, flood tide, 10-sec wave period, 4-ft wave height, proposed breakwater installed



Photo 15. Test series I, southeast wave direction, ebb tide, 6-sec wave period, 2-ft wave height

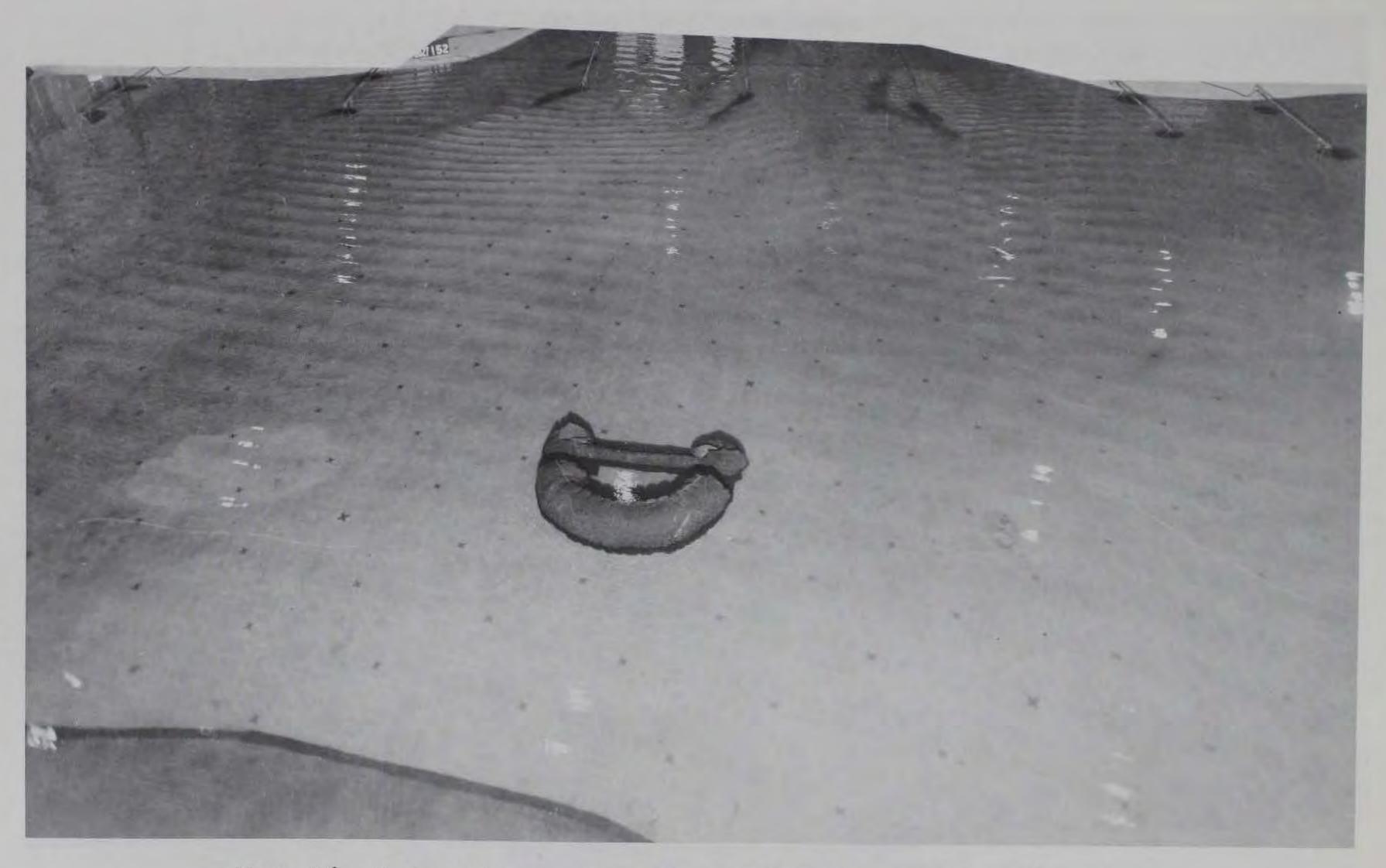


Photo 16. Test series I, southeast wave direction, ebb tide, 6-sec wave period, 2-ft wave height, proposed breakwater installed

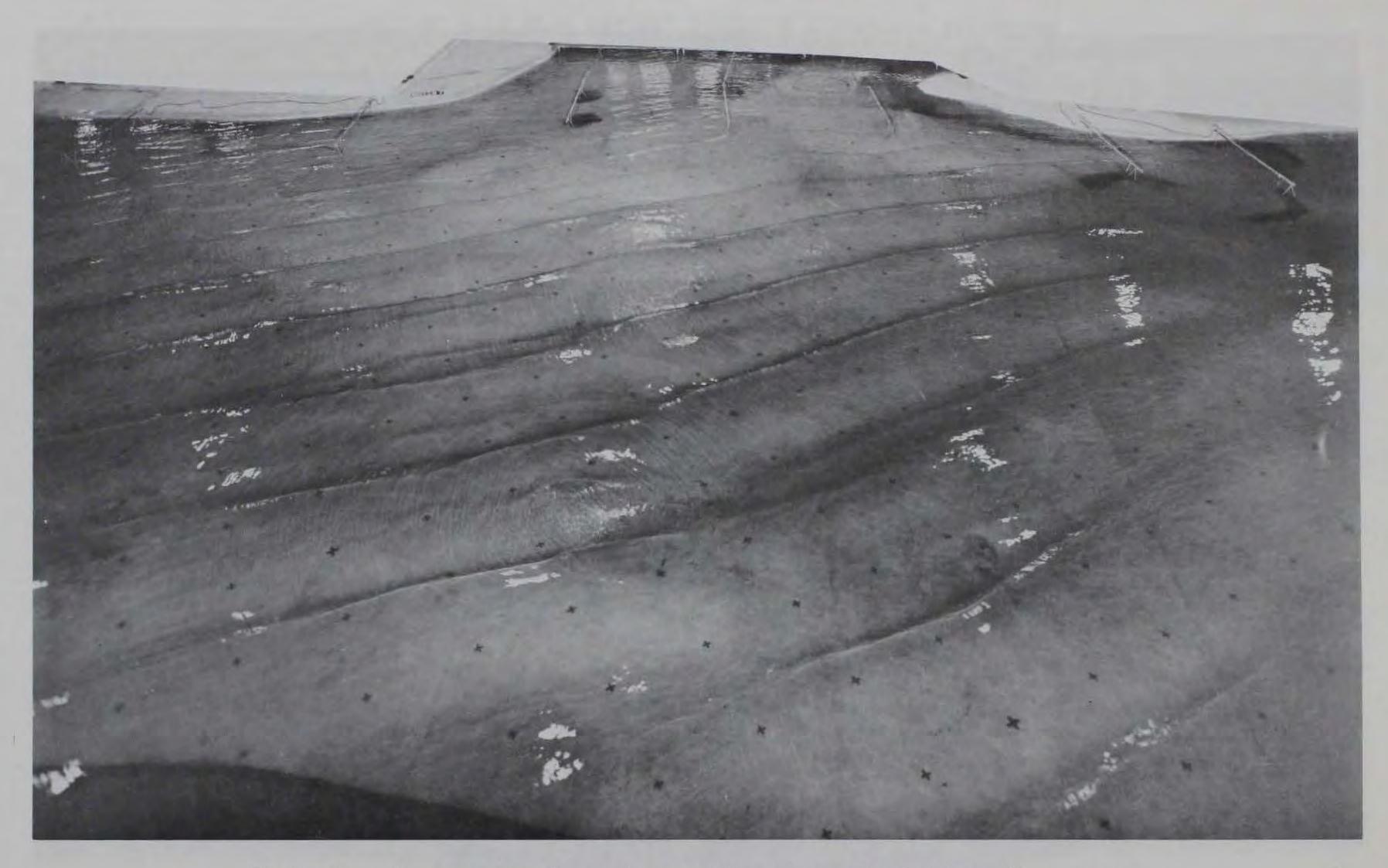


Photo 17. Test series I, east wave direction, slack tide, 14-sec wave period, 14-ft wave height



Photo 18. Test series I, east wave direction, slack tide, 14-sec wave period, 14-ft wave height, proposed breakwater installed



Photo 19. Test series I, east wave direction, flood tide, 6-sec wave period, 7-ft wave height



Photo 20. Test series I, east wave direction, flood tide, 6-sec wave period, 7-ft wave height, proposed breakwater installed



Photo 21. Test series I, east wave direction, ebb tide, 10-sec wave period, 14-ft wave height

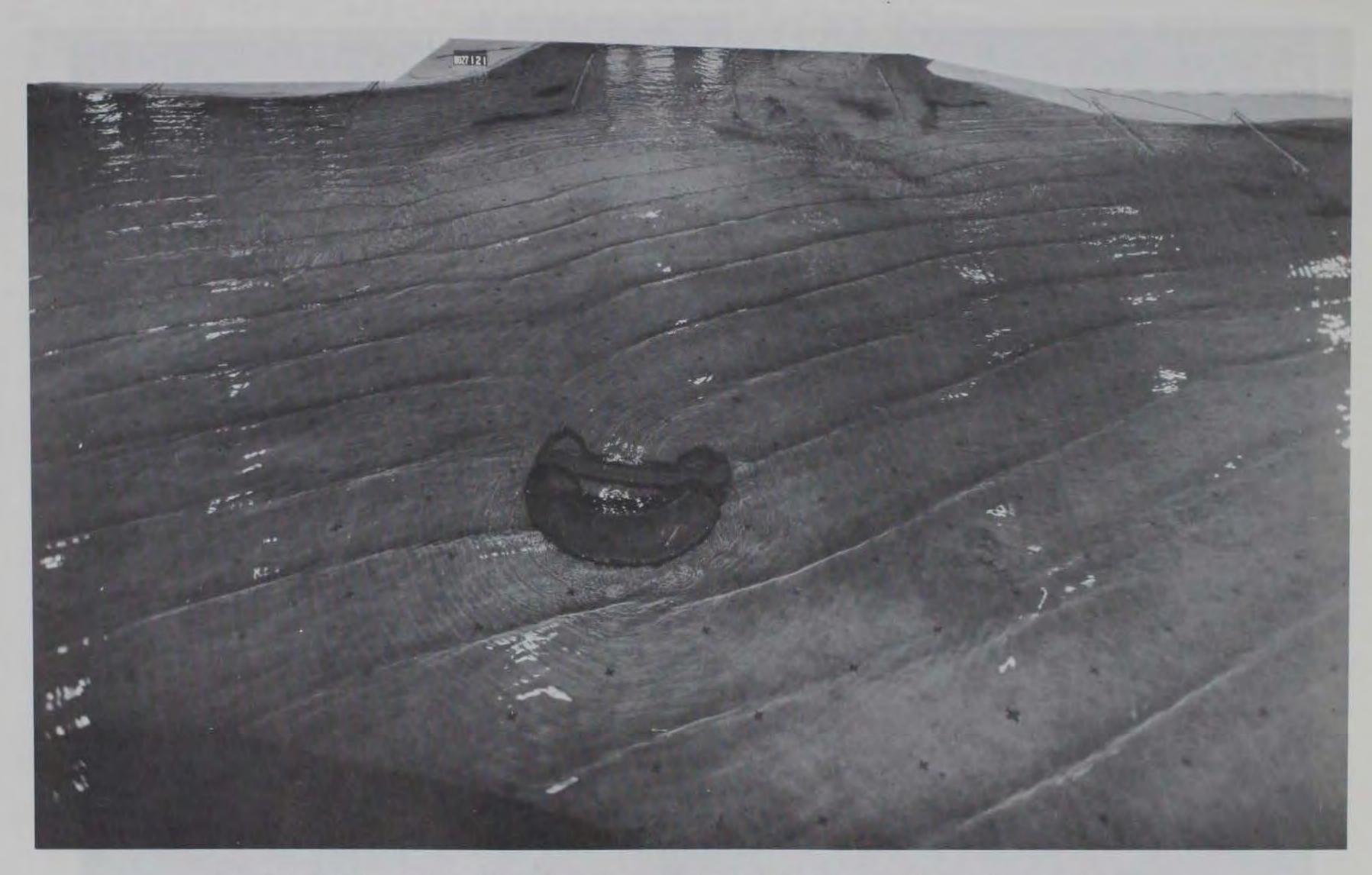


Photo 22. Test series I, east wave direction, ebb tide, 10-sec wave period, 14-ft wave height, proposed breakwater installed



Photo 23. Test series II and III, south zone, southeast wave direction, slack tide, 6-sec wave period, 7-ft wave height

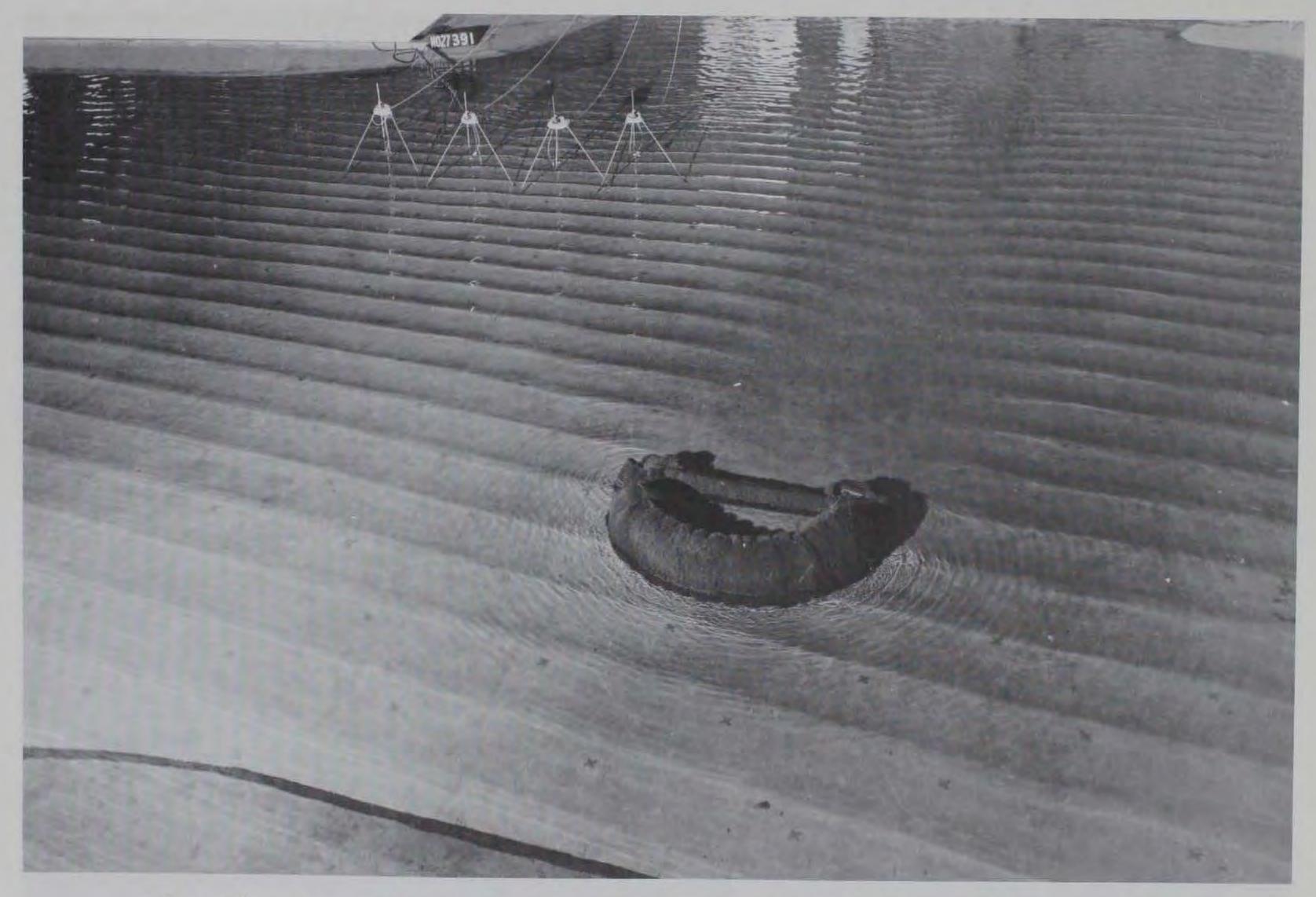


Photo 24. Test series II and III, south zone, southeast wave direction, slack tide, 6-sec wave period, 7-ft wave height, proposed breakwater installed

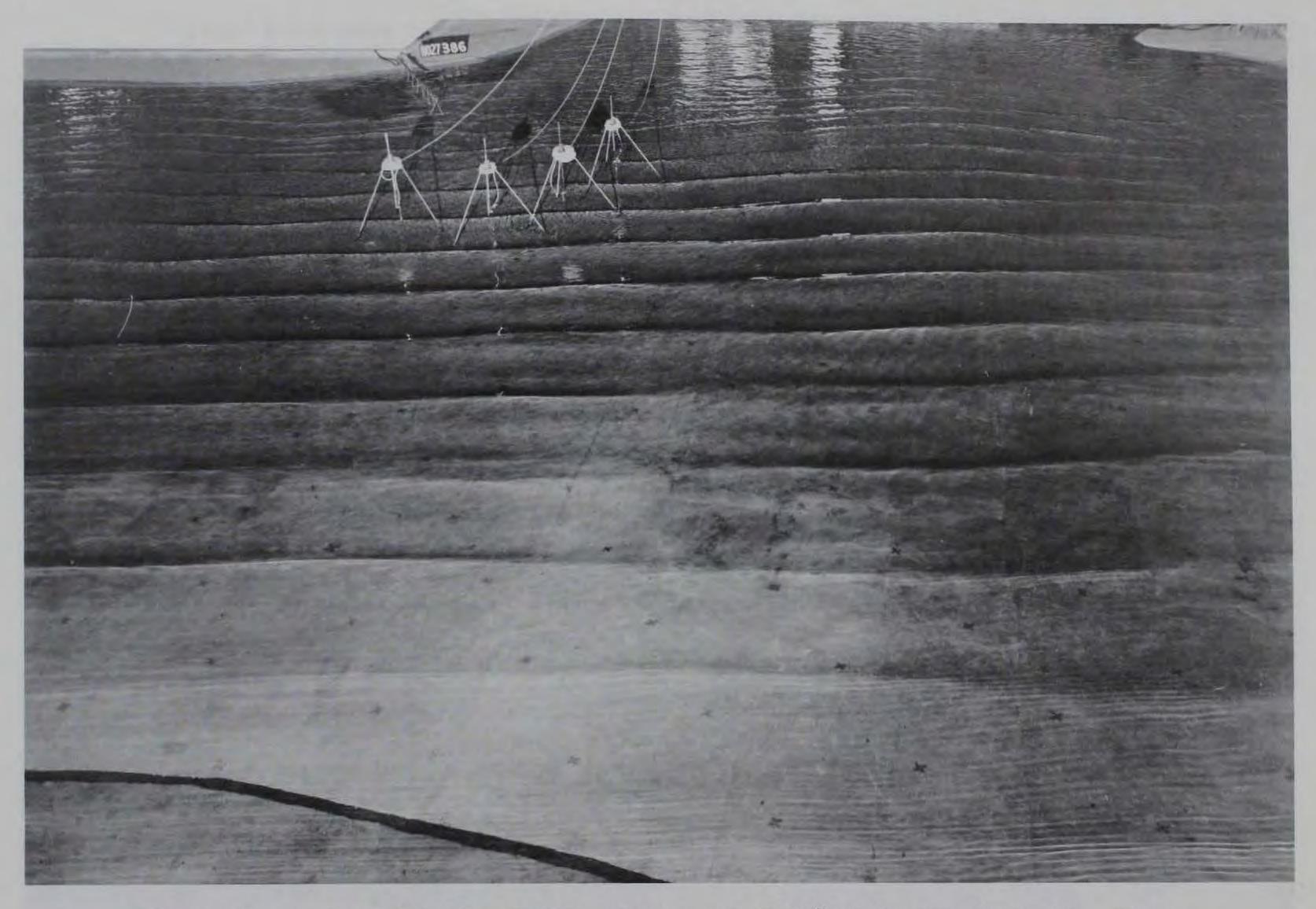


Photo 25. Test series II and III, south zone, E 22°30' S wave direction, slack tide, 10-sec wave period, 10-ft wave height

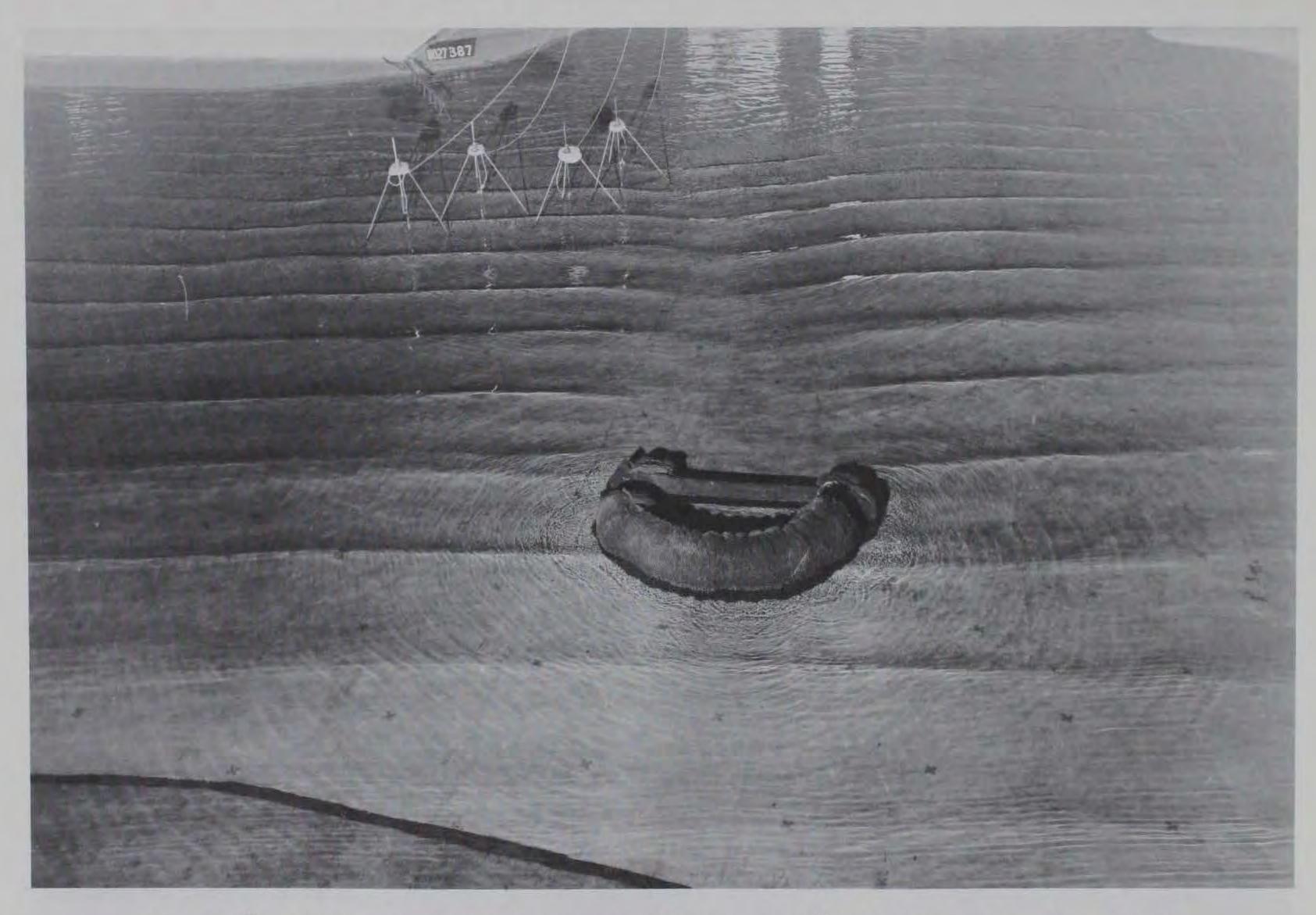


Photo 26. Test series II and III, south zone, E 22°30' S wave direction, slack tide, 10-sec wave period, 10-ft wave height, proposed breakwater installed



Photo 27. Test series II and III, south zone, E 22°30' N wave direction, slack tide, 14-sec wave period, 10-ft wave height

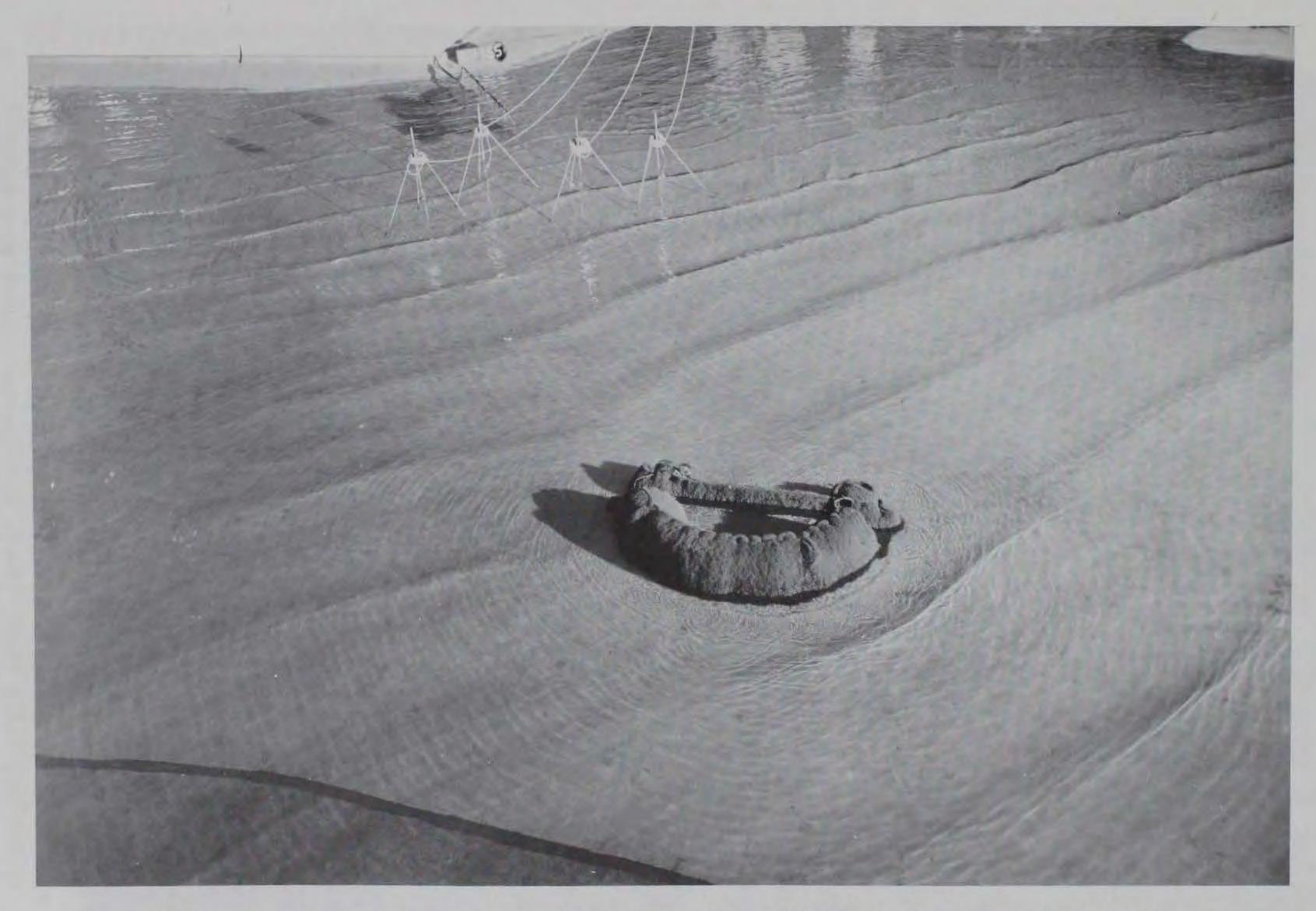


Photo 28. Test series II and III, south zone, E 22°30' N wave direction, slack tide, 14-sec wave period, 10-ft wave height, proposed breakwater installed



Photo 29. Test series II and III, north zone, S 22°30' E wave direction, slack tide, 10-sec wave period, 10-ft wave height

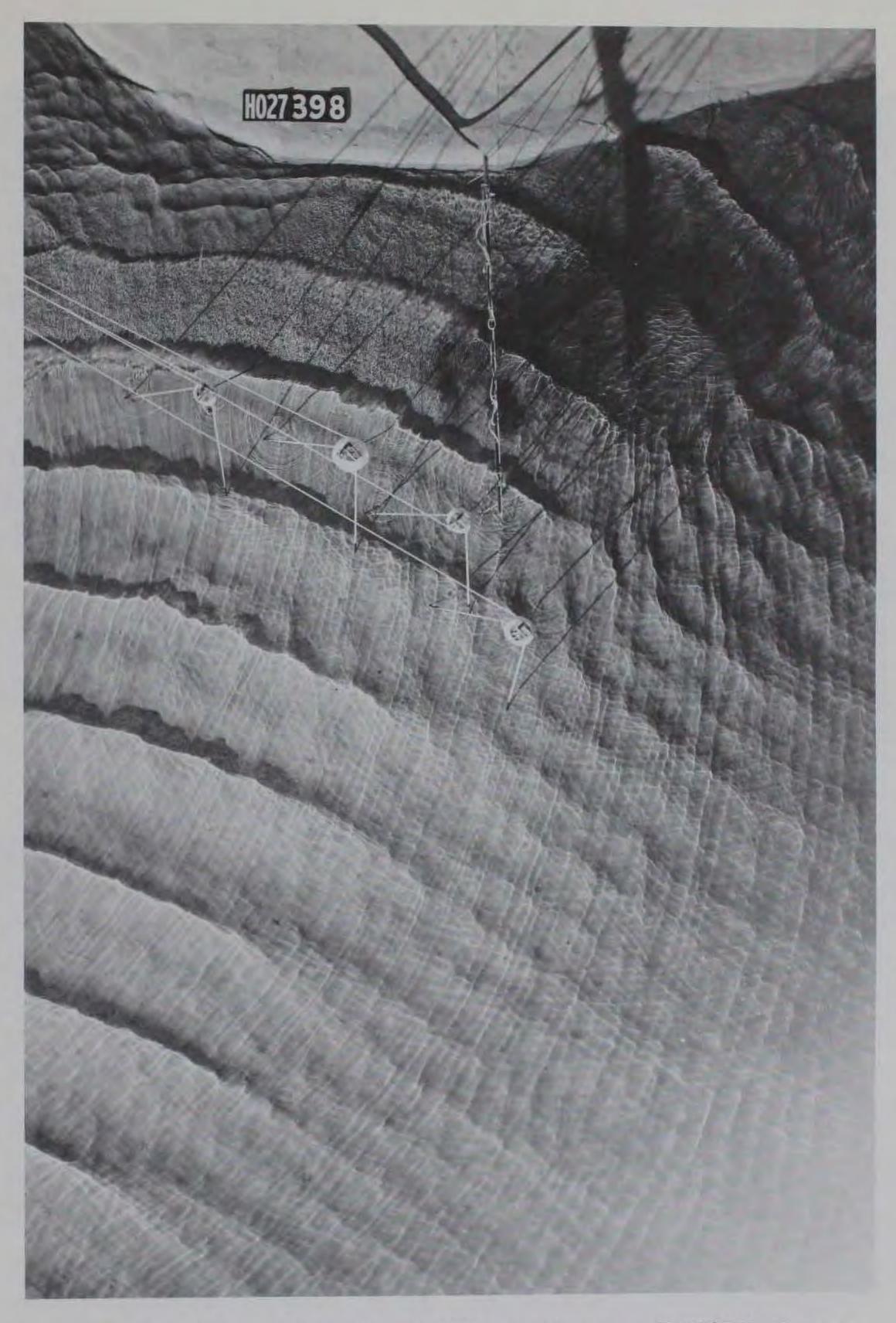


Photo 30. Test series II and III, north zone, S 22°30' E wave direction, slack tide, 10-sec wave period, 10-ft wave height, proposed breakwater installed



Photo 31. Test series II and III, north zone, southeast wave direction, slack tide, 14-sec wave period, 10-ft wave height

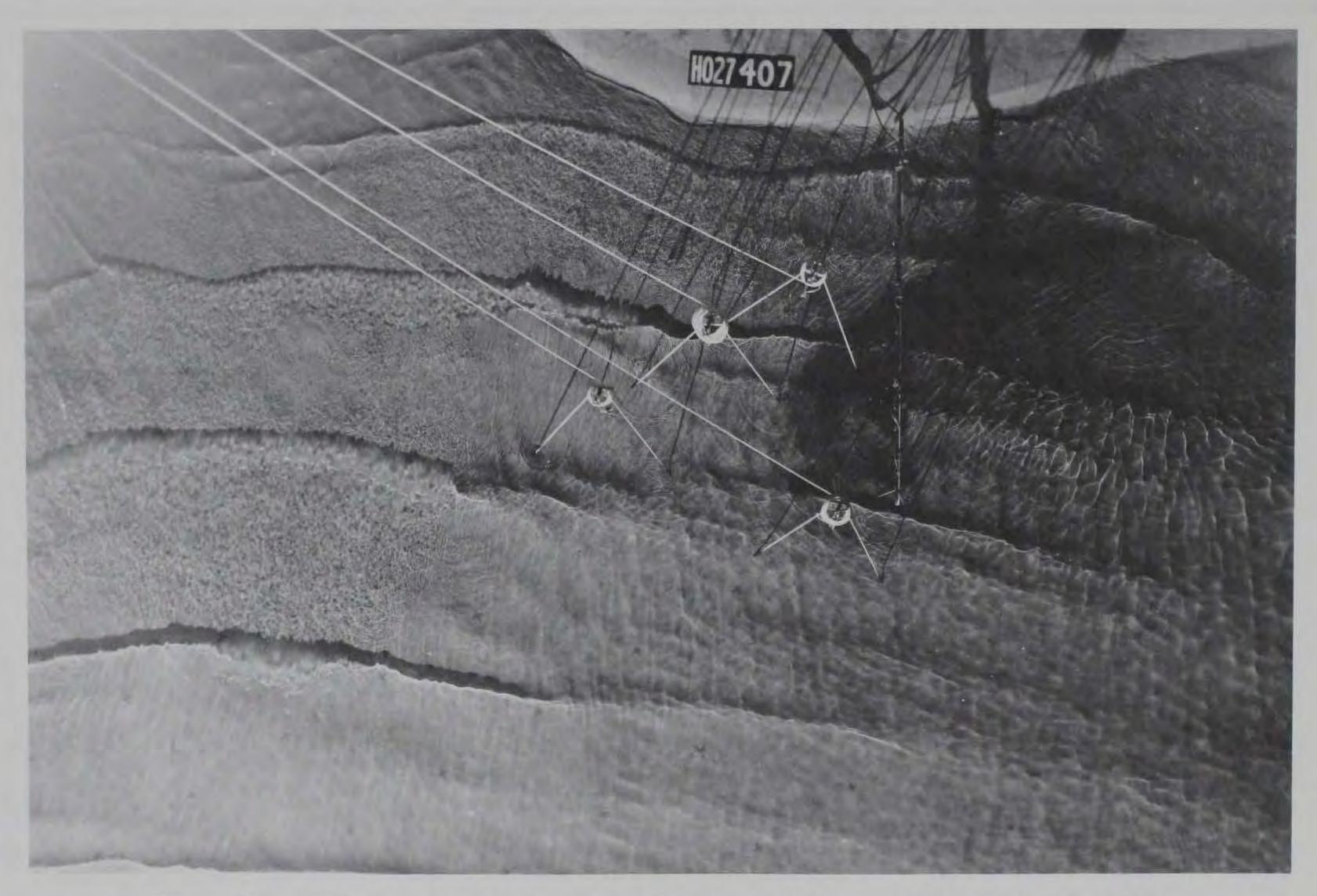
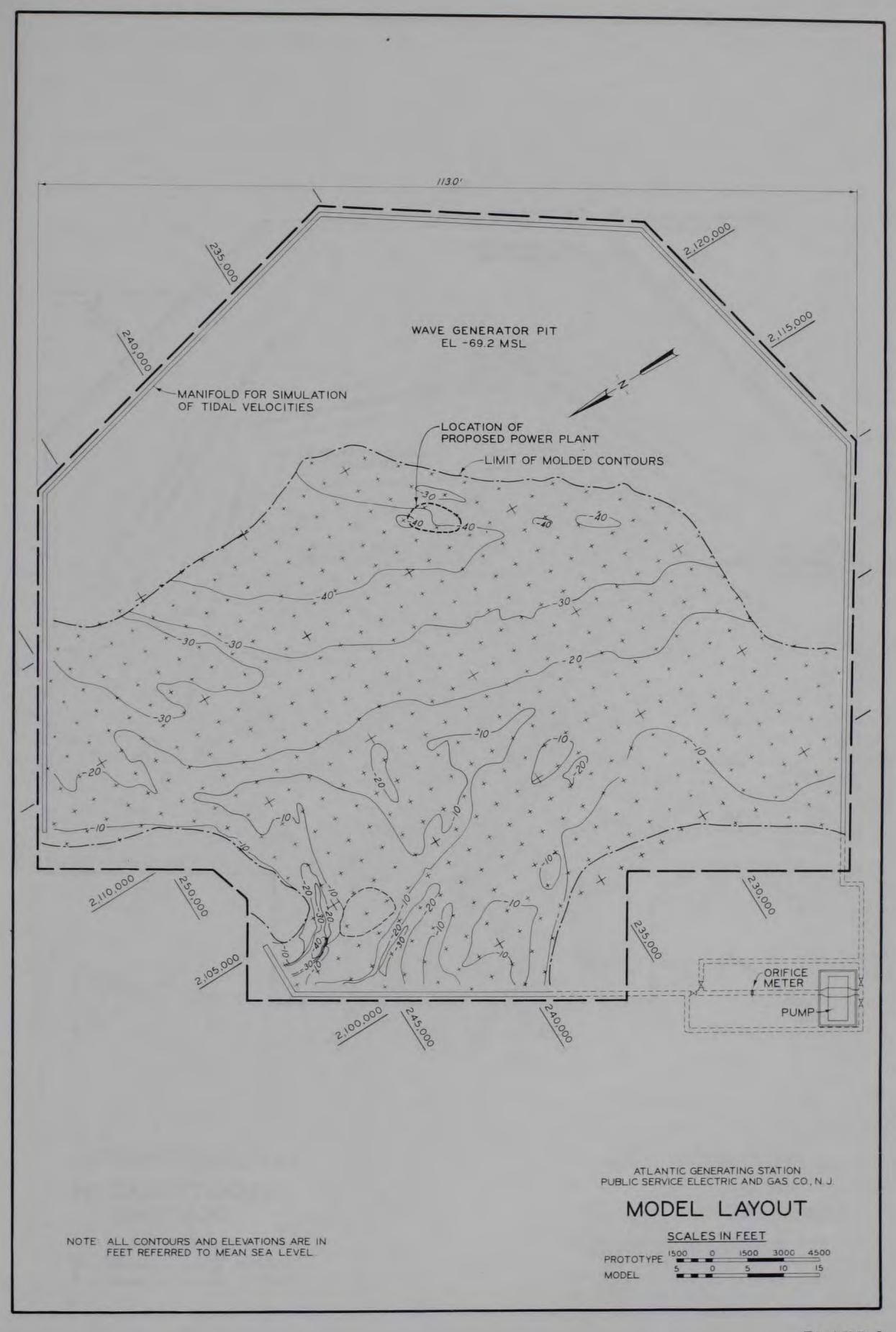
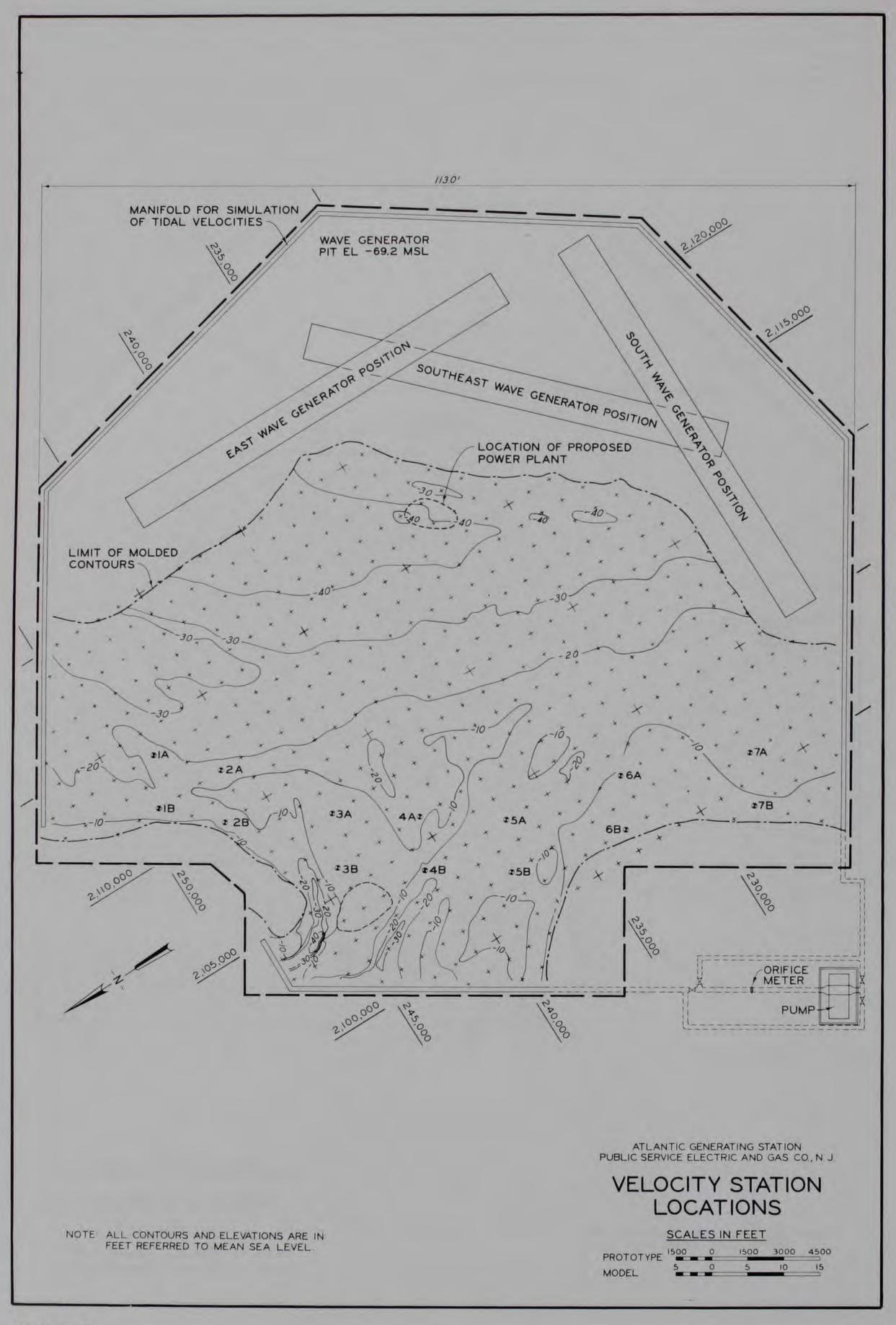
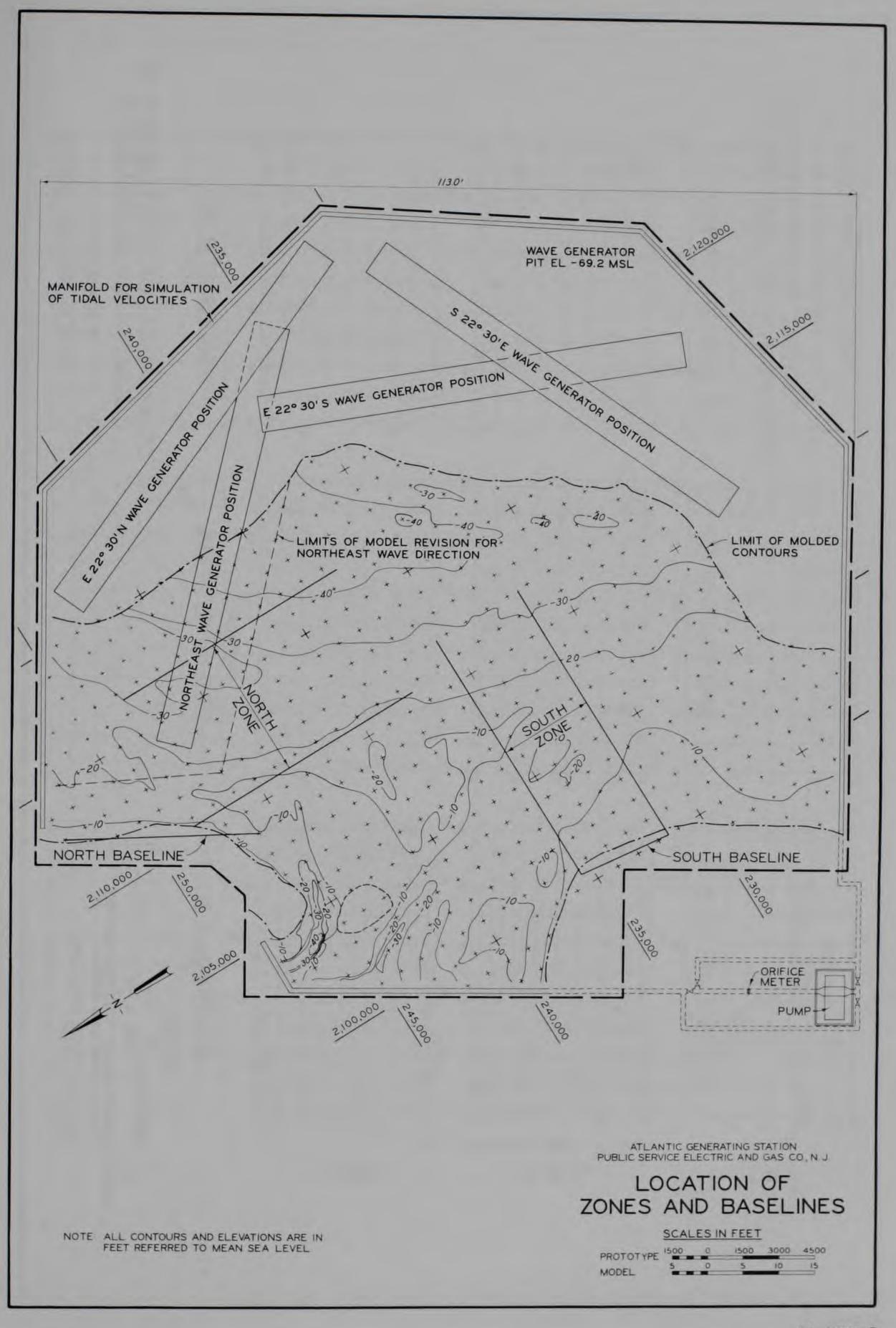
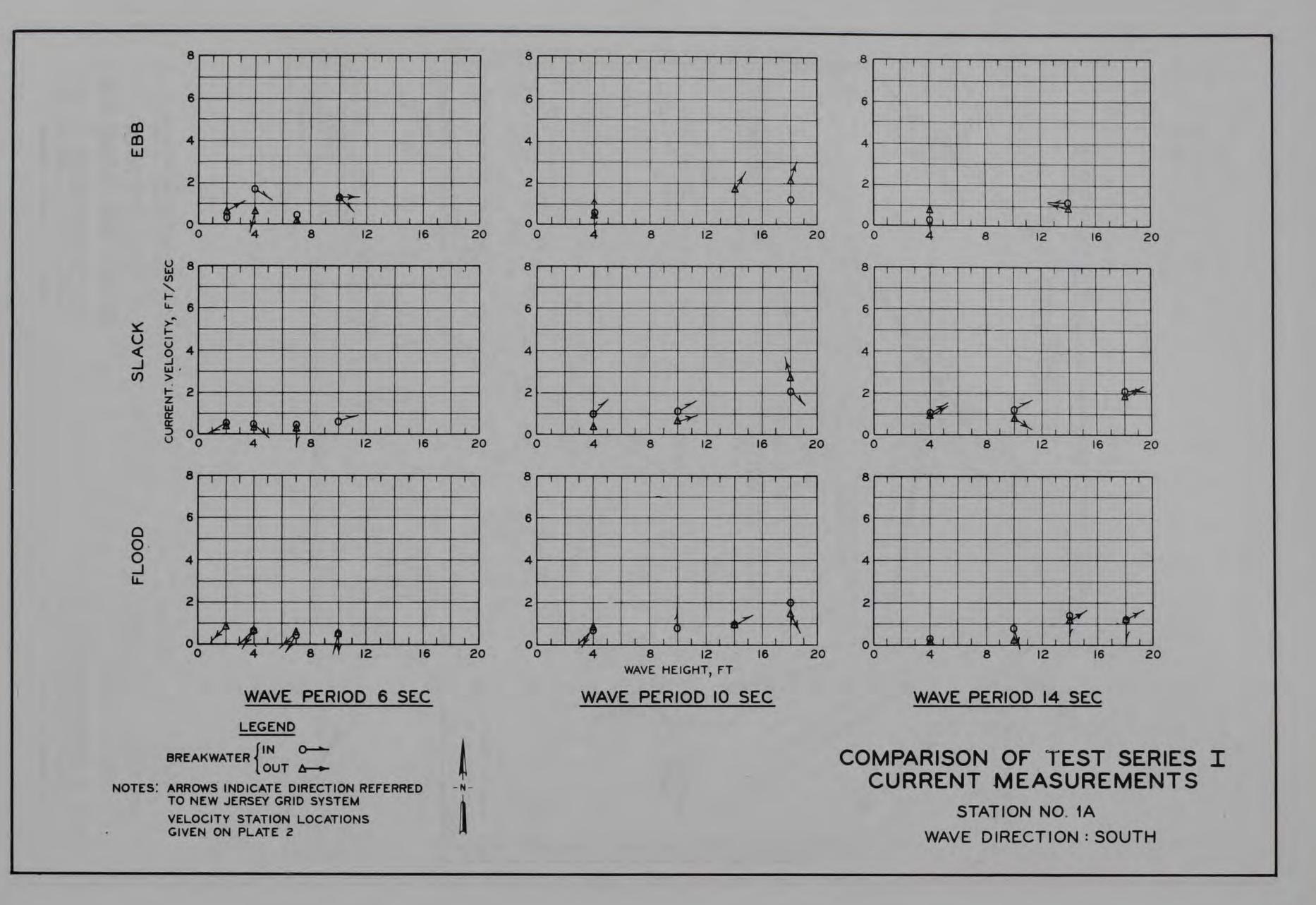


Photo 32. Test series II and III, north zone, southeast wave direction, slack tide, 14-sec wave period, 10-ft wave height, proposed breakwater installed









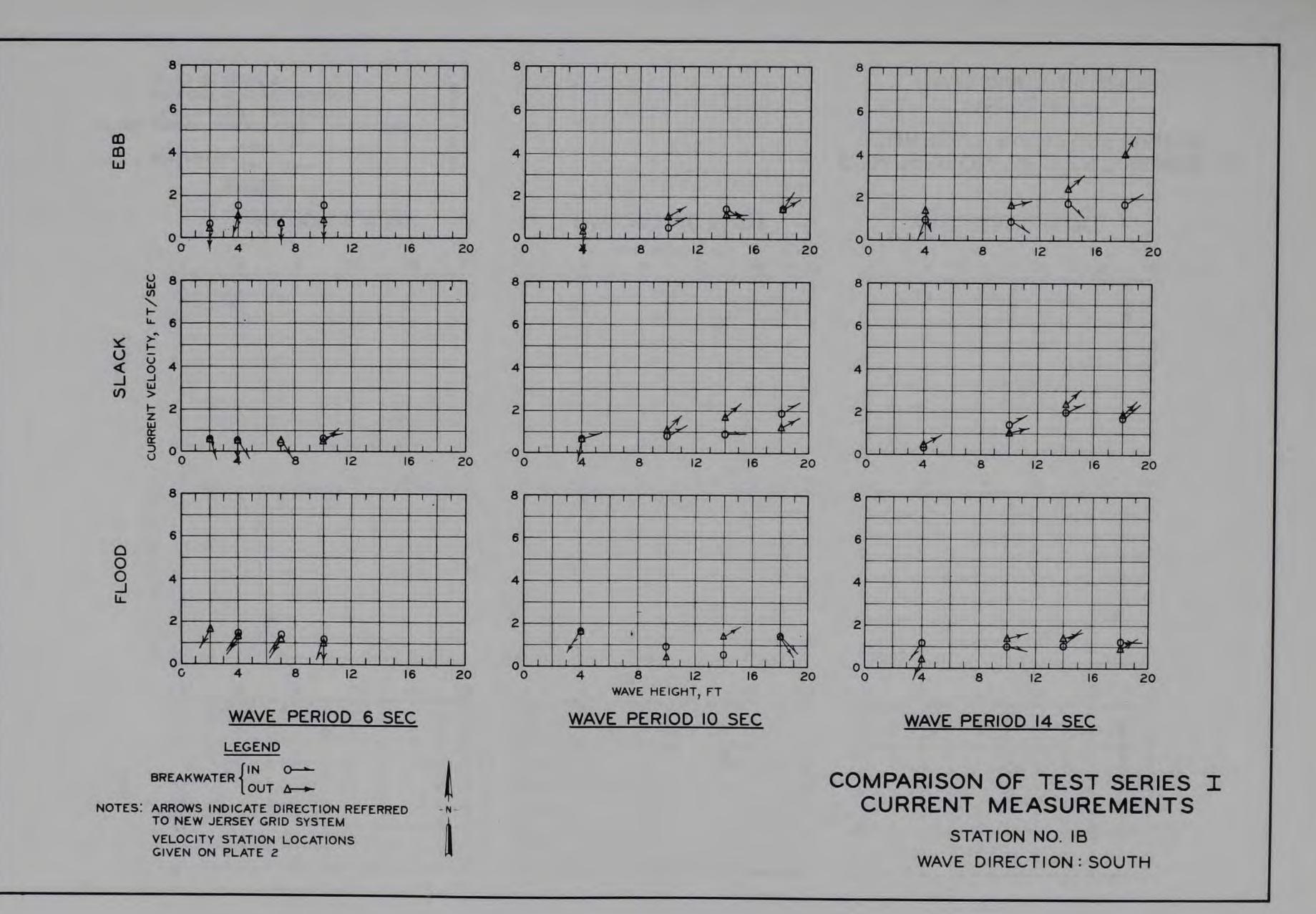
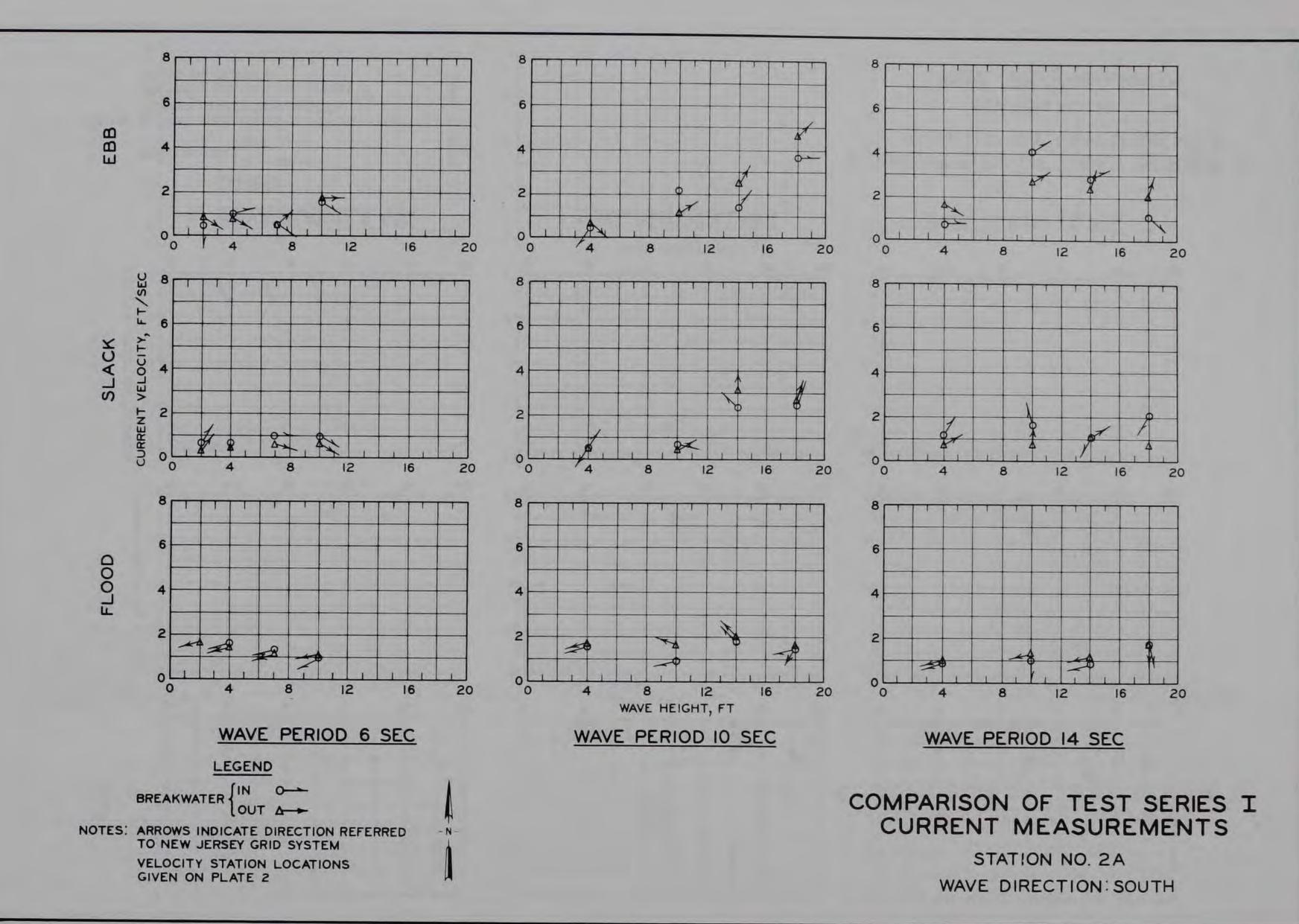


PLATE 5



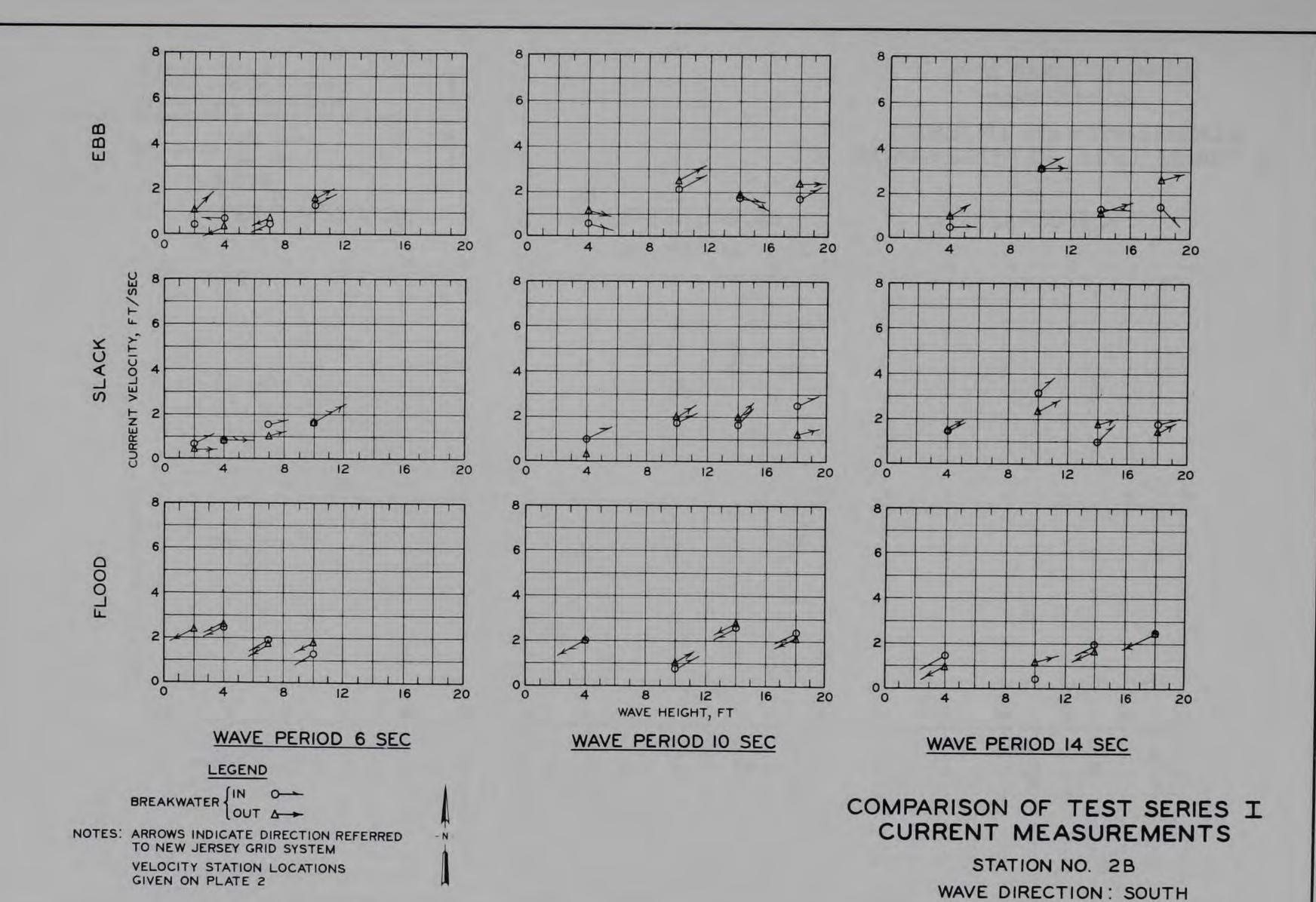
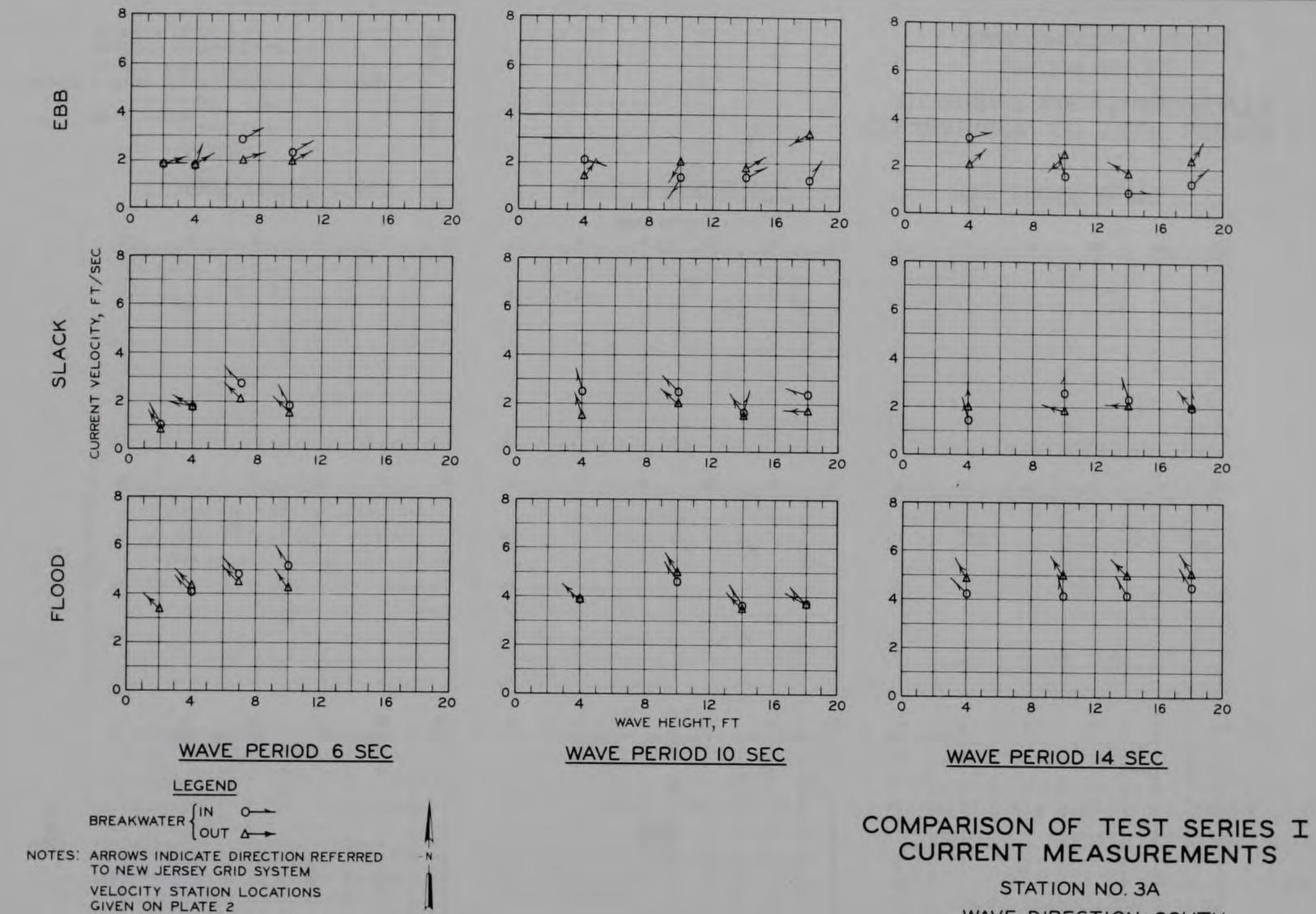
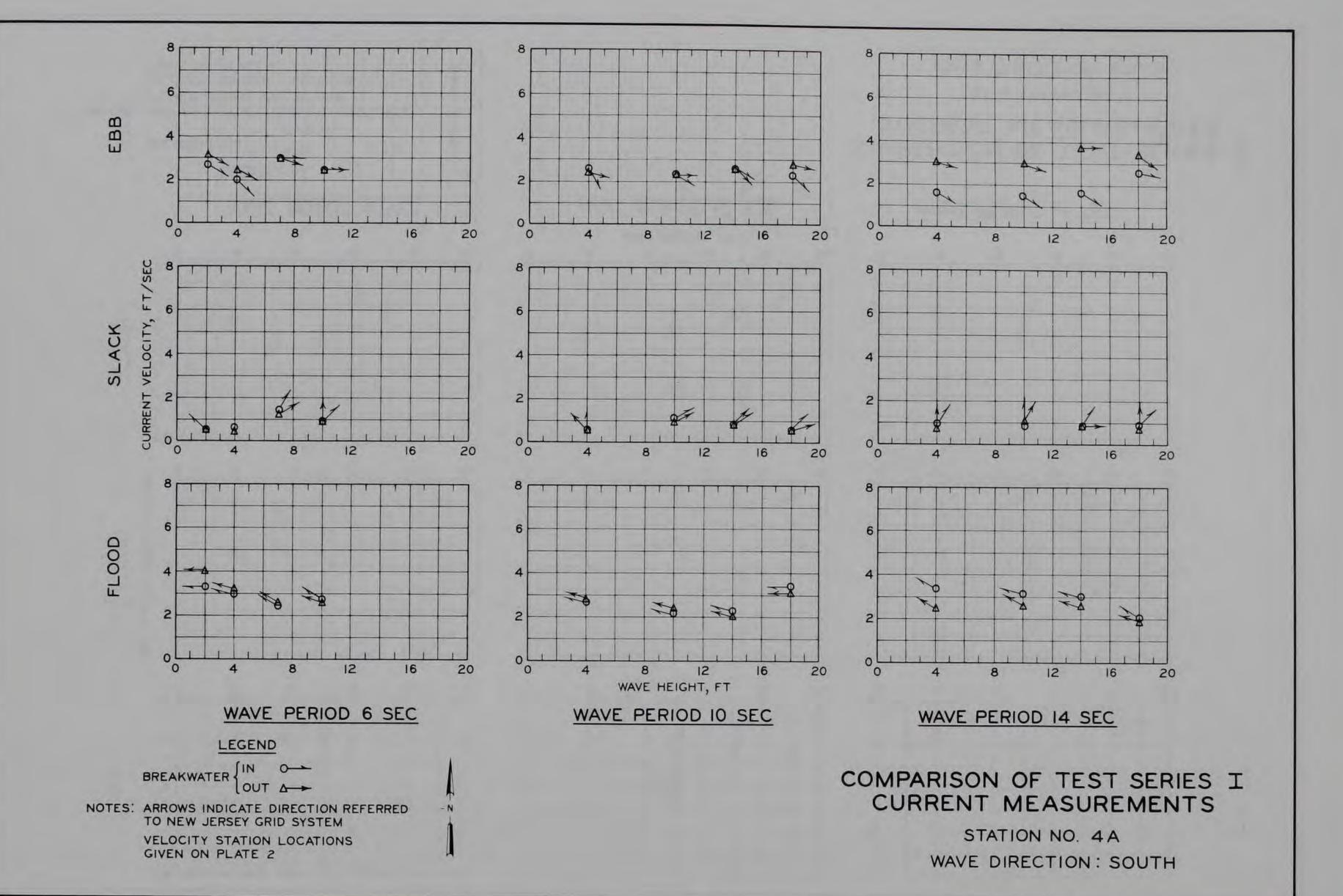
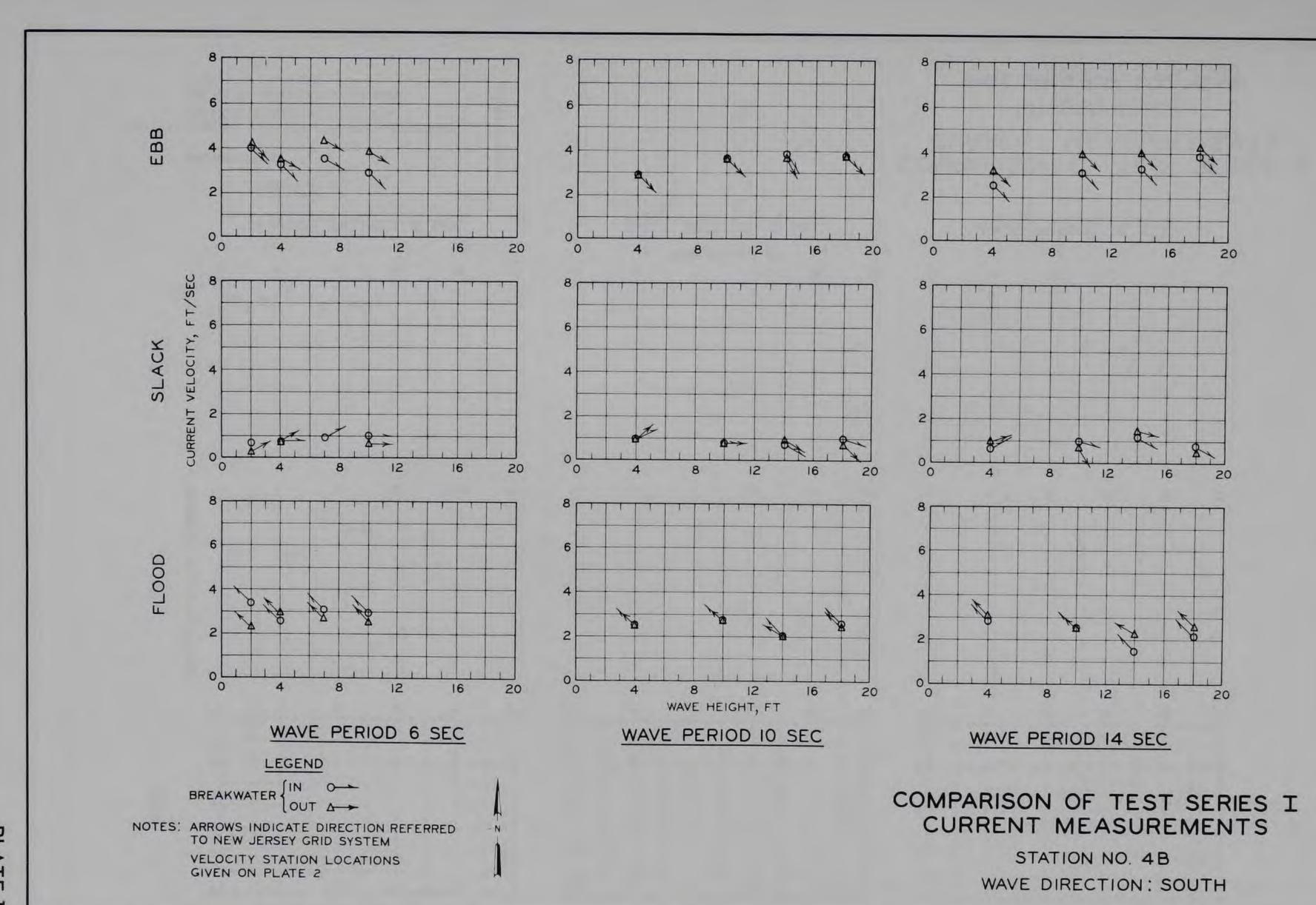


PLATE !



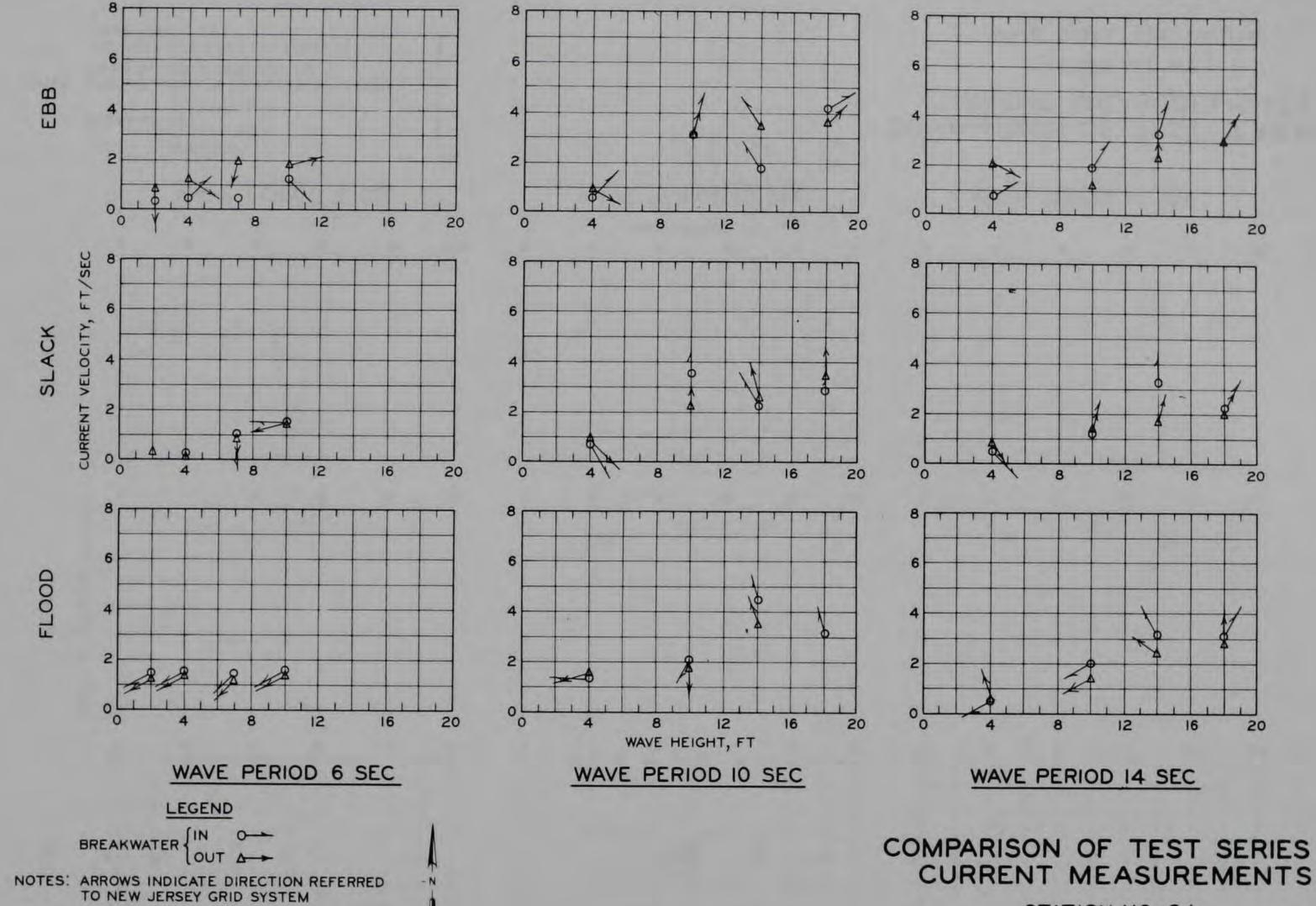
WAVE DIRECTION: SOUTH





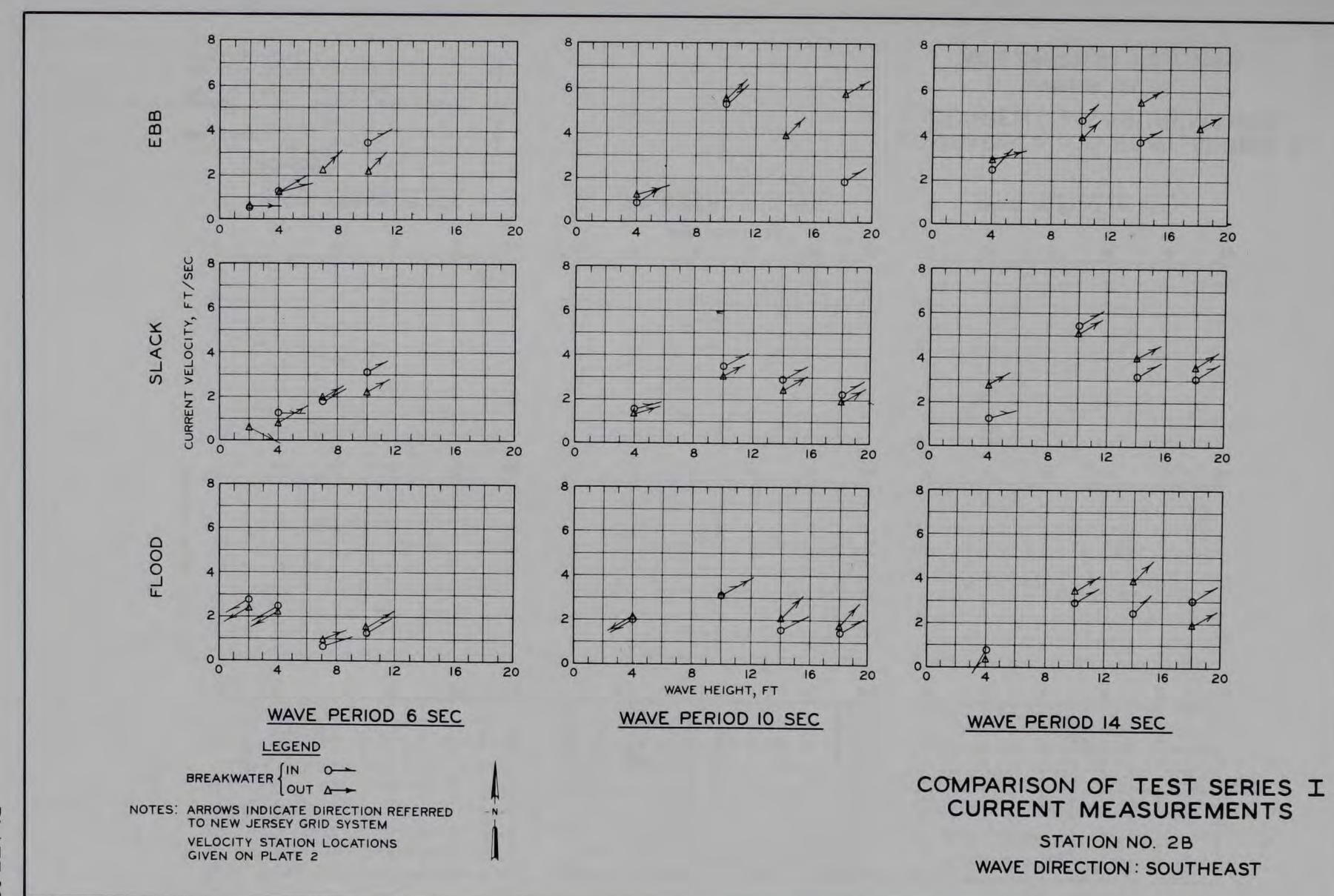
VELOCITY STATION LOCATIONS

GIVEN ON PLATE 2



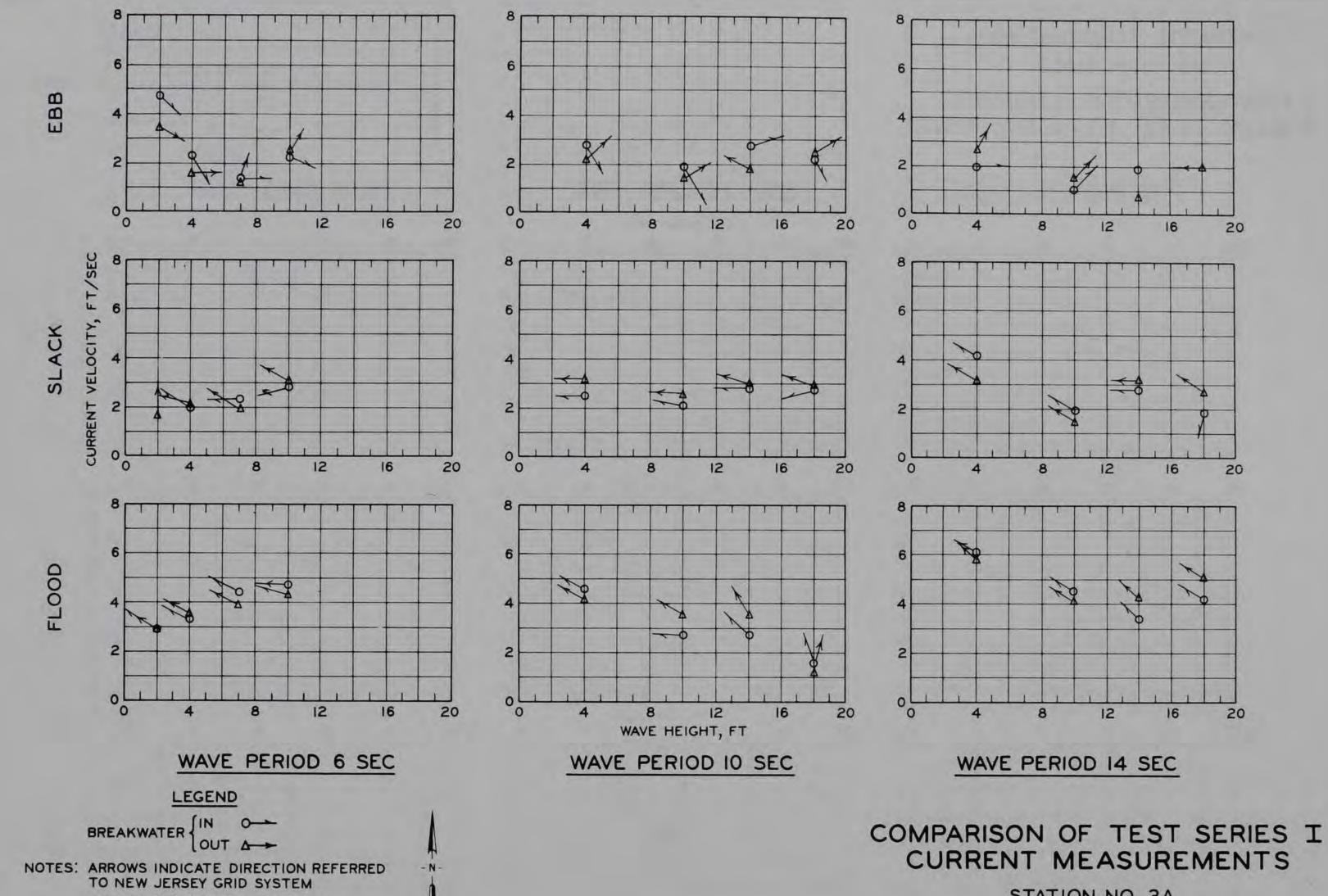
COMPARISON OF TEST SERIES I

STATION NO. 2A WAVE DIRECTION : SOUTHEAST

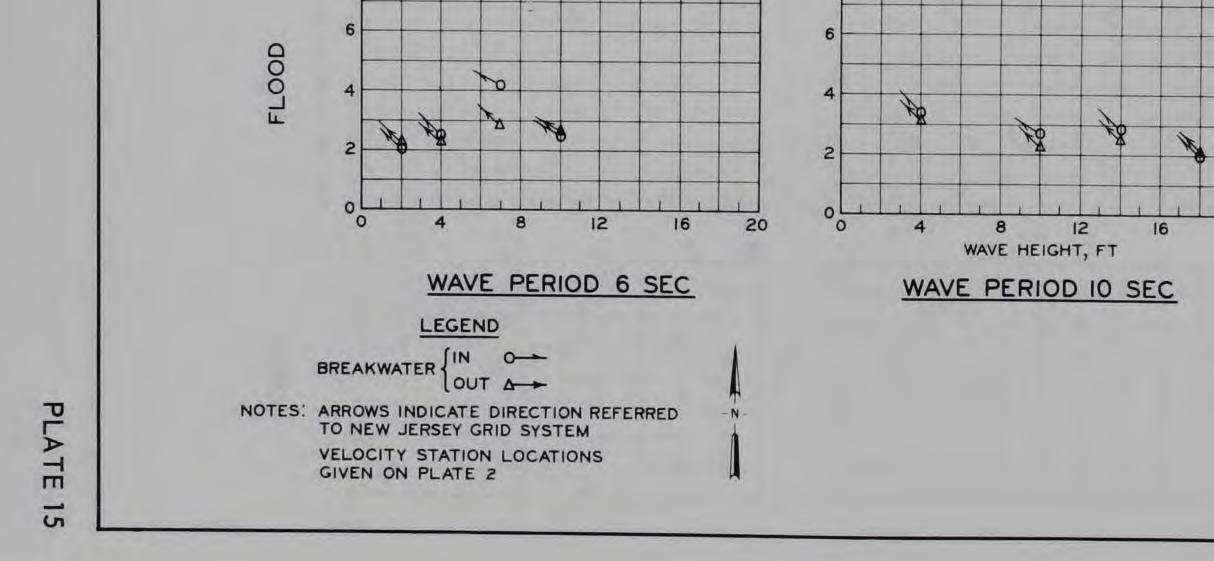


VELOCITY STATION LOCATIONS

GIVEN ON PLATE 2



STATION NO. 3A WAVE DIRECTION: SOUTHEAST



12

12

16

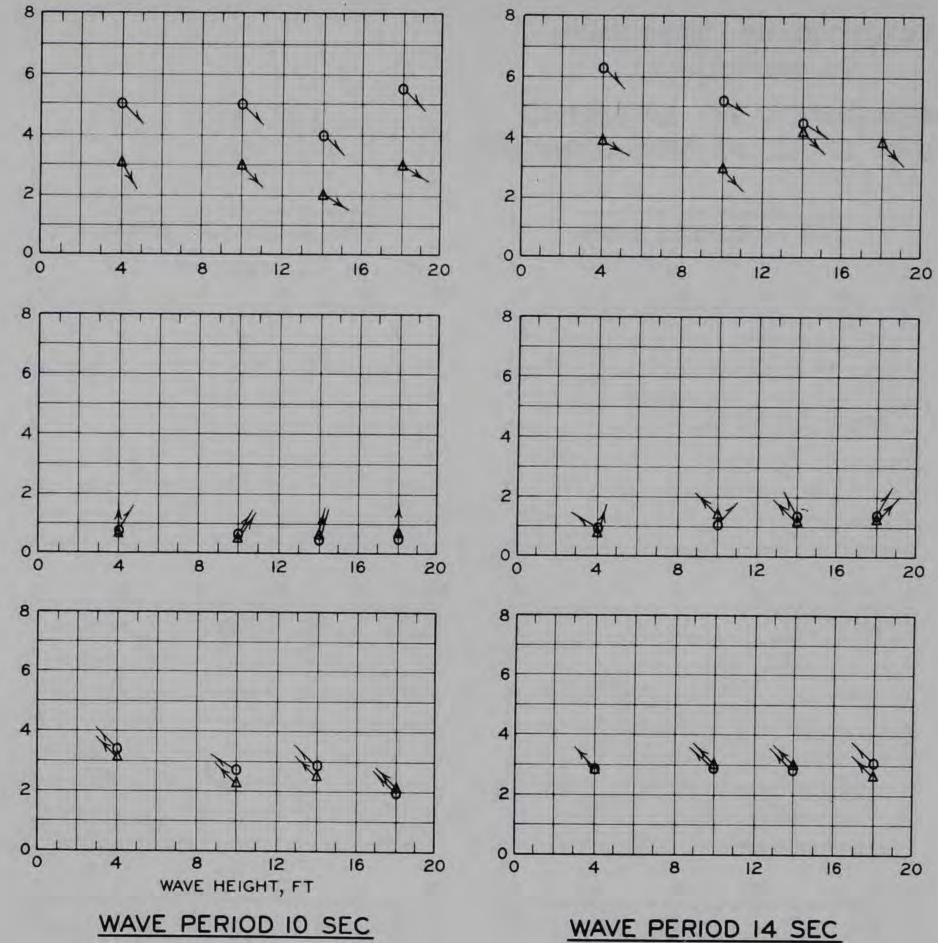
20

EBB

FT/SEC

VELOCITY,

SLACK



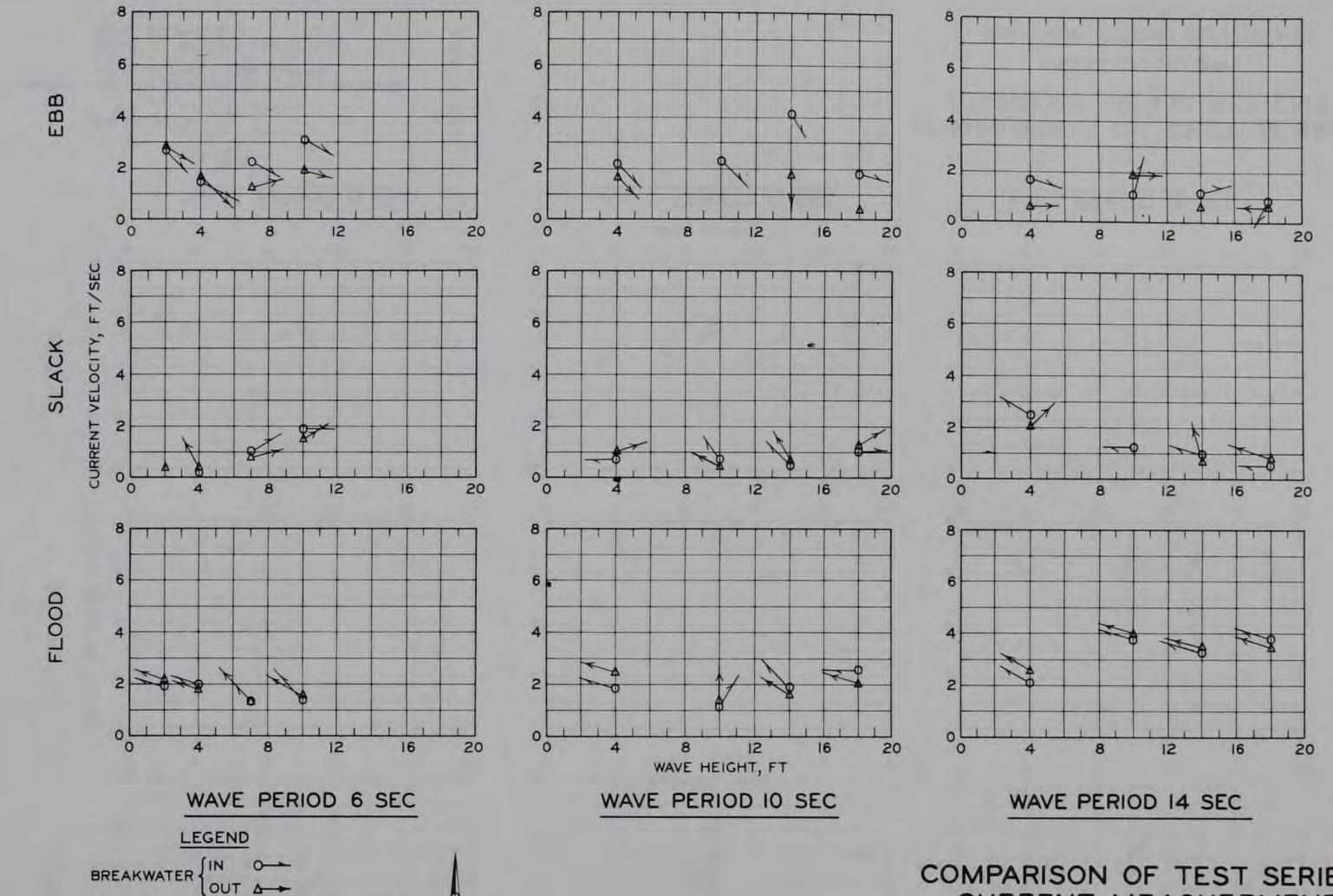
COMPARISON OF TEST SERIES I CURRENT MEASUREMENTS

STATION NO. 3B
WAVE DIRECTION: SOUTHEAST

NOTES: ARROWS INDICATE DIRECTION REFERRED TO NEW JERSEY GRID SYSTEM

VELOCITY STATION LOCATIONS

GIVEN ON PLATE 2



COMPARISON OF TEST SERIES I CURRENT MEASUREMENTS

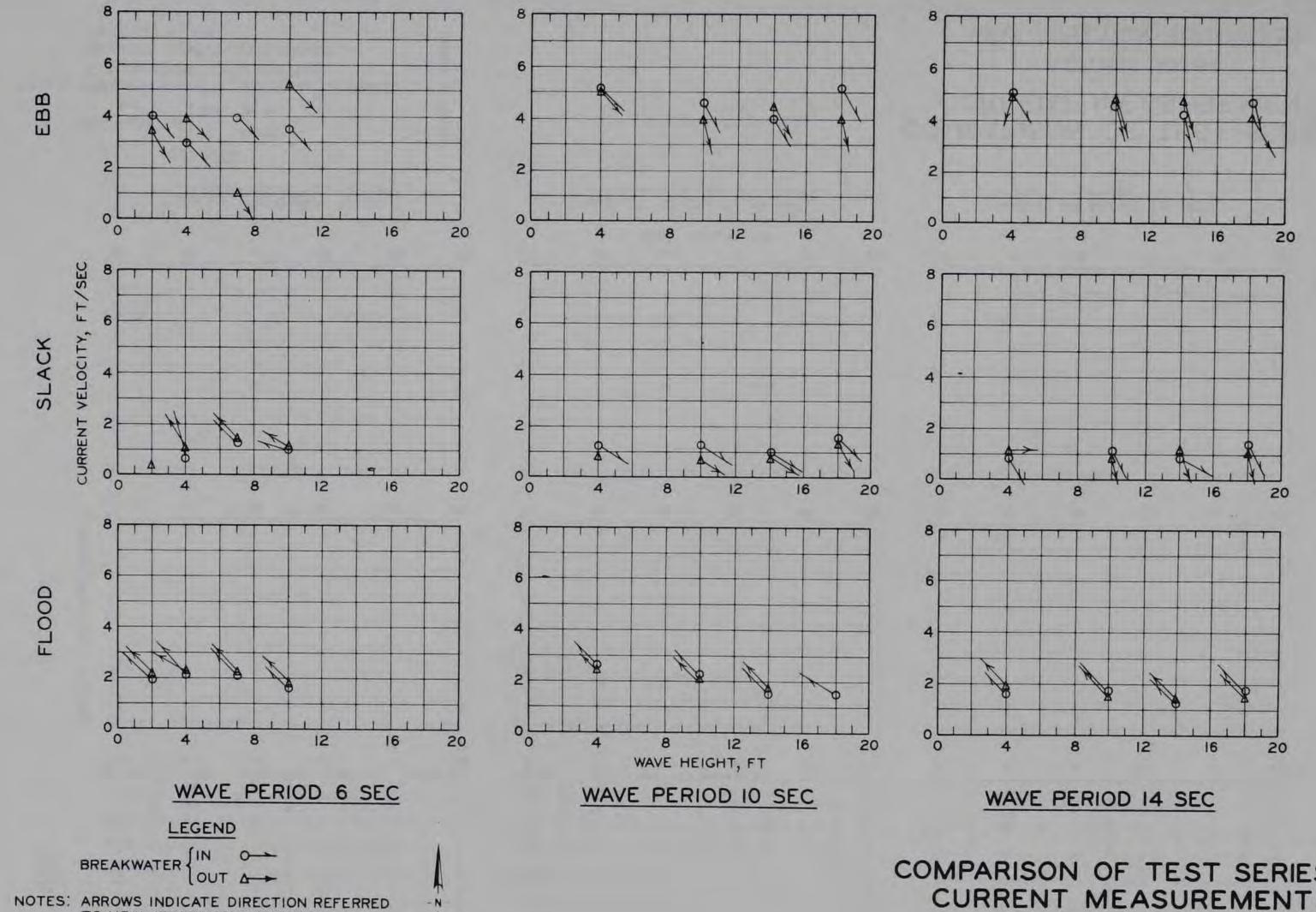
STATION NO. 4A WAVE DIRECTION : SOUTHEAST



TO NEW JERSEY GRID SYSTEM

GIVEN ON PLATE 2

VELOCITY STATION LOCATIONS

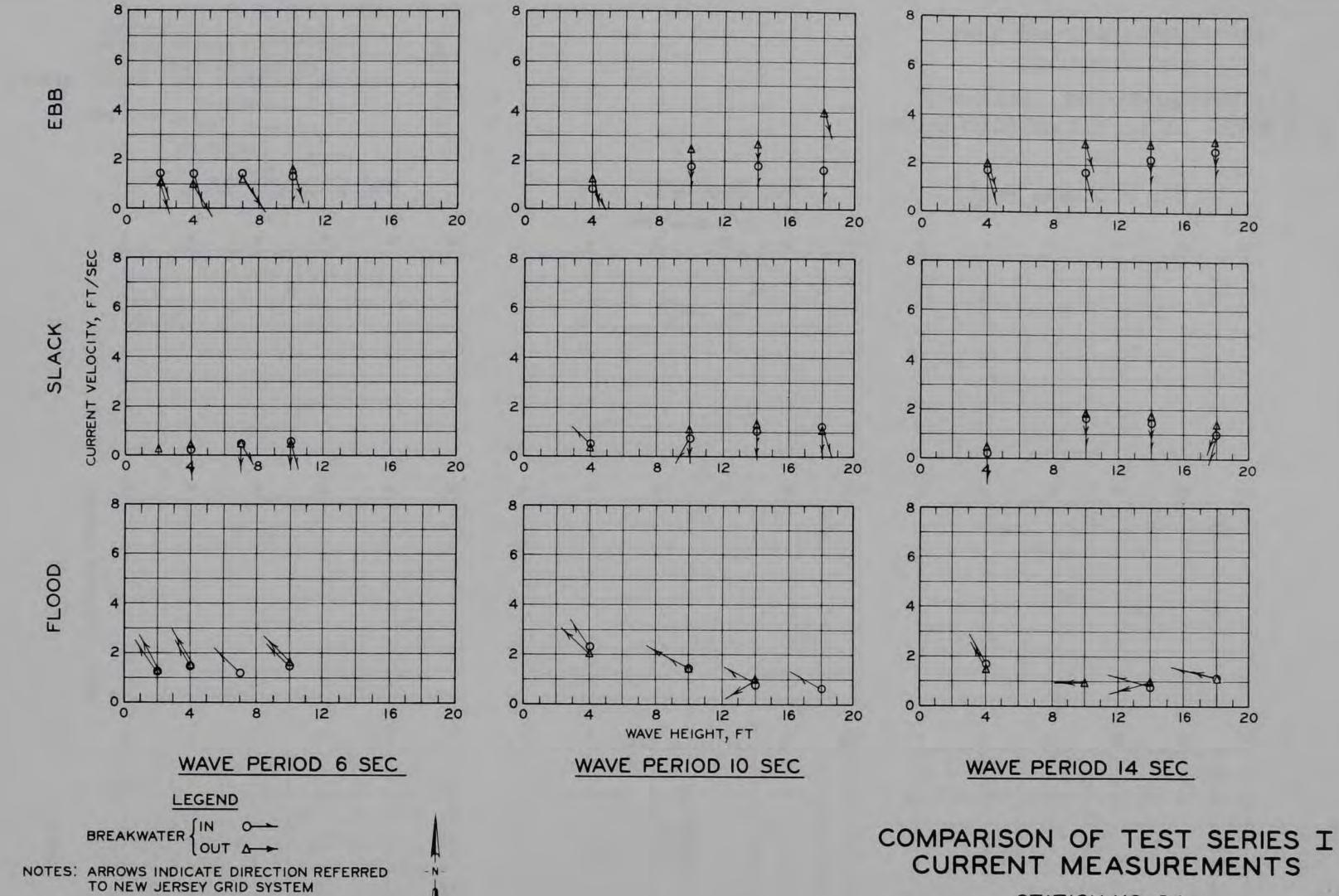


COMPARISON OF TEST SERIES I CURRENT MEASUREMENTS

> STATION NO. 4B WAVE DIRECTION : SOUTHEAST

VELOCITY STATION LOCATIONS

GIVEN ON PLATE 2



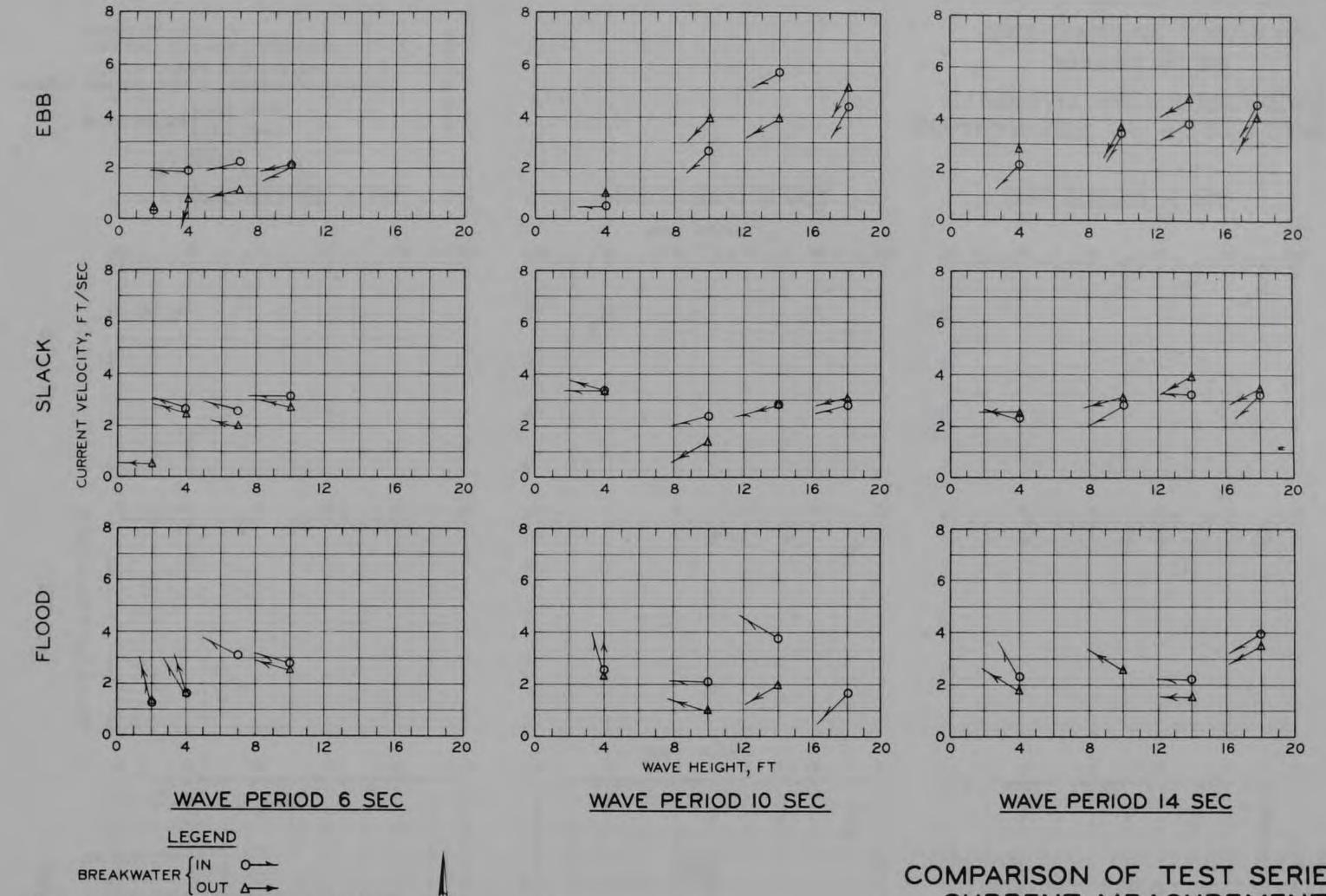
CURRENT MEASUREMENTS

STATION NO. 5A WAVE DIRECTION : SOUTHEAST

NOTES: ARROWS INDICATE DIRECTION REFERRED TO NEW JERSEY GRID SYSTEM

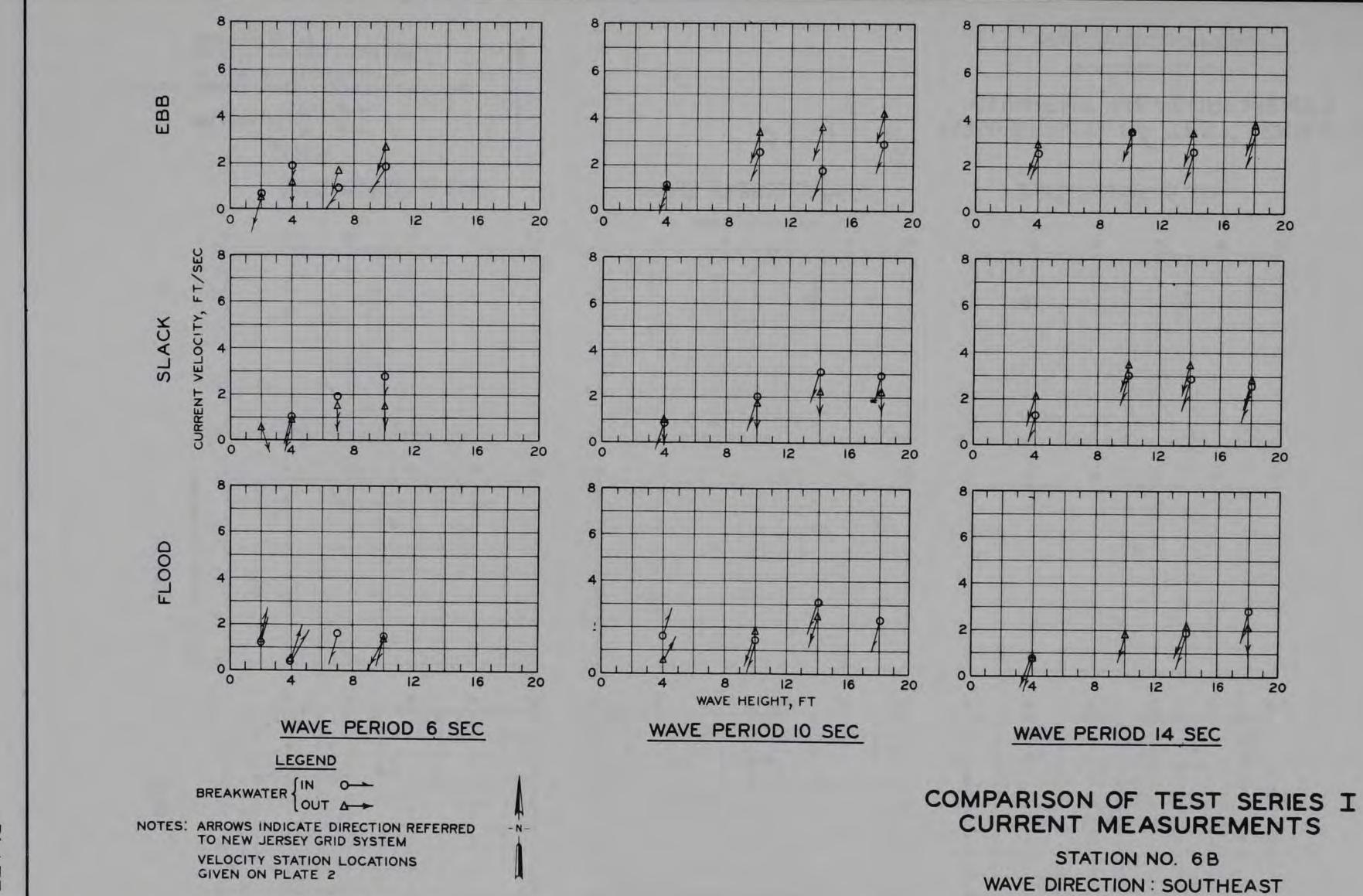
VELOCITY STATION LOCATIONS

GIVEN ON PLATE 2



COMPARISON OF TEST SERIES I CURRENT MEASUREMENTS

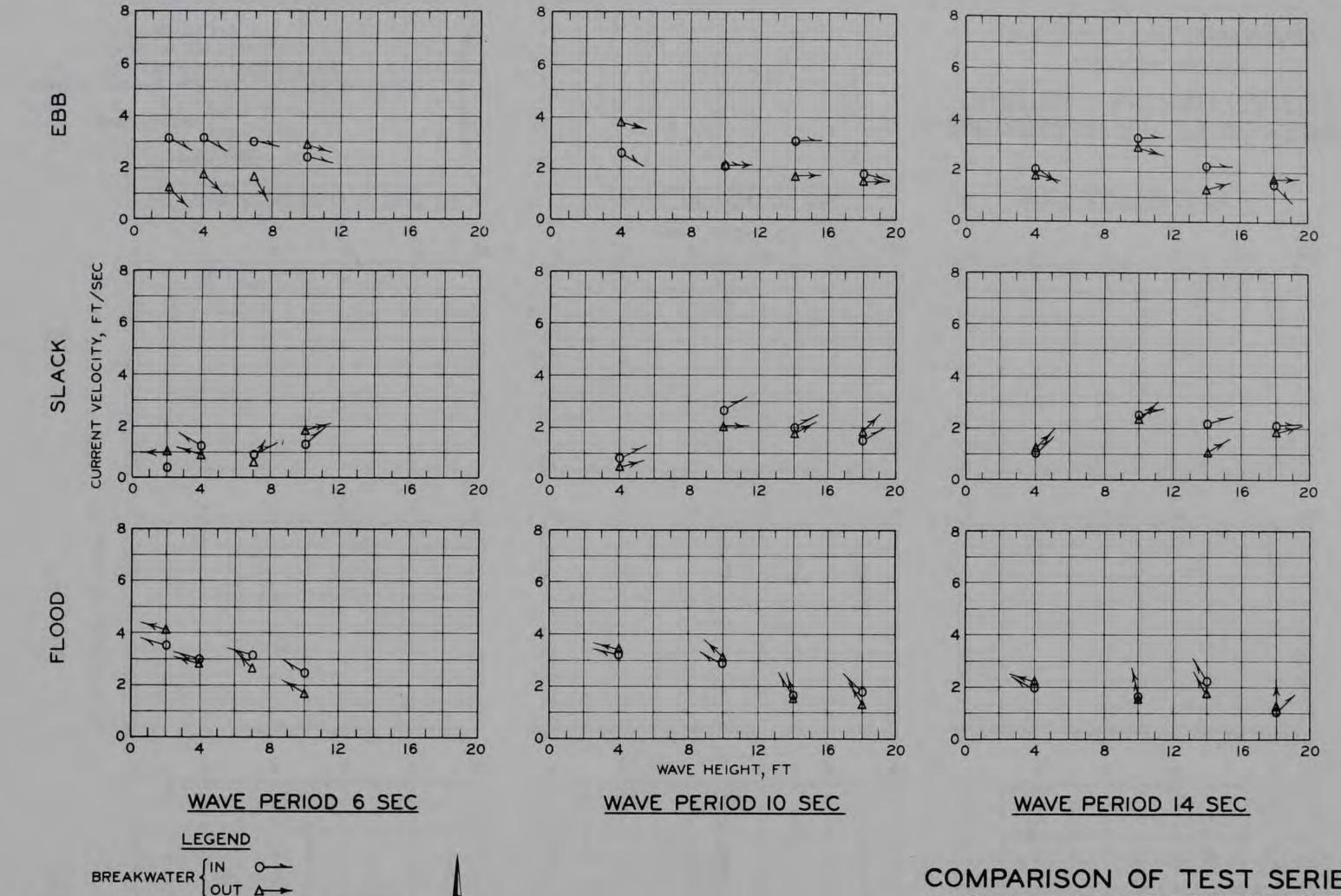
STATION NO. 6A WAVE DIRECTION: SOUTHEAST



NOTES: ARROWS INDICATE DIRECTION REFERRED TO NEW JERSEY GRID SYSTEM

VELOCITY STATION LOCATIONS

GIVEN ON PLATE 2



COMPARISON OF TEST SERIES I CURRENT MEASUREMENTS

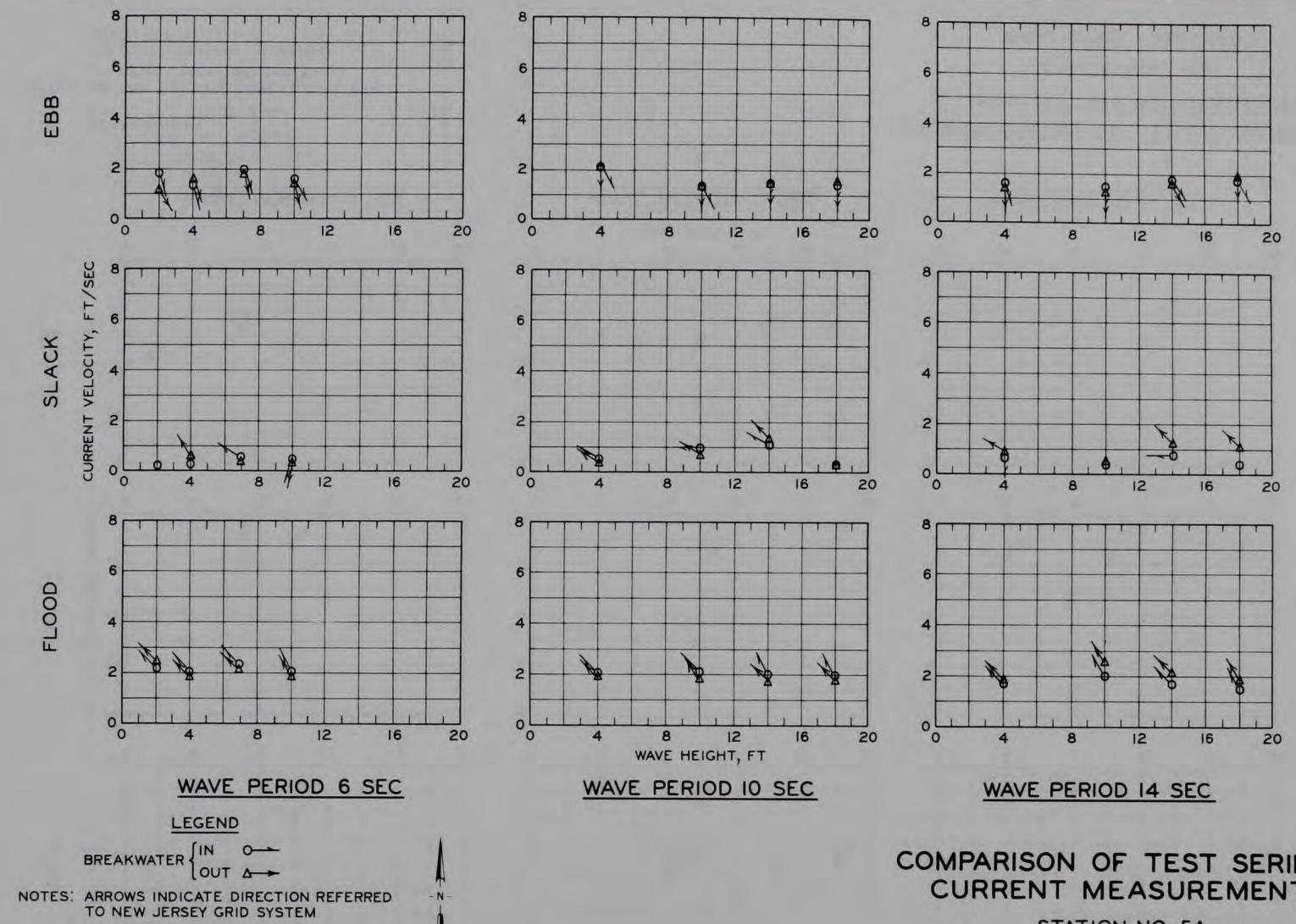
STATION NO. 4A
WAVE DIRECTION: EAST

WAVE DIRECTION : EAST

LATE 23

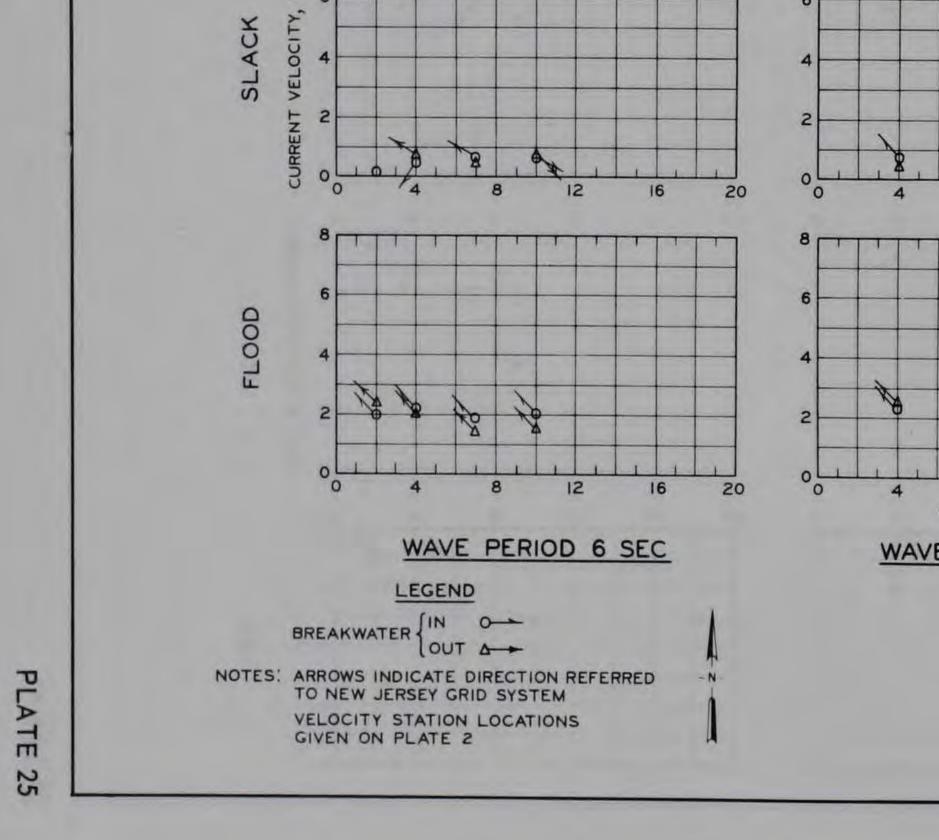
VELOCITY STATION LOCATIONS

GIVEN ON PLATE 2



COMPARISON OF TEST SERIES I CURRENT MEASUREMENTS

STATION NO. 5A WAVE DIRECTION: EAST



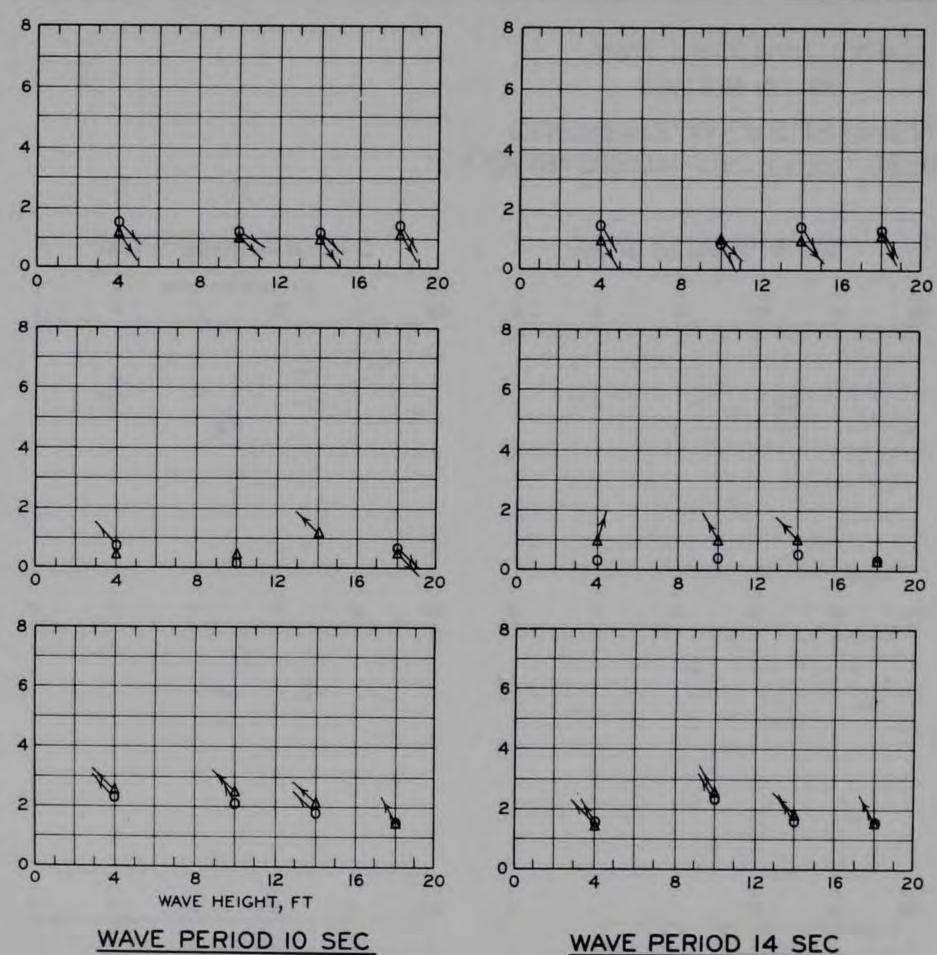
12

16

20

EBB

FT/SEC



WAVE PERIOD 14 SEC

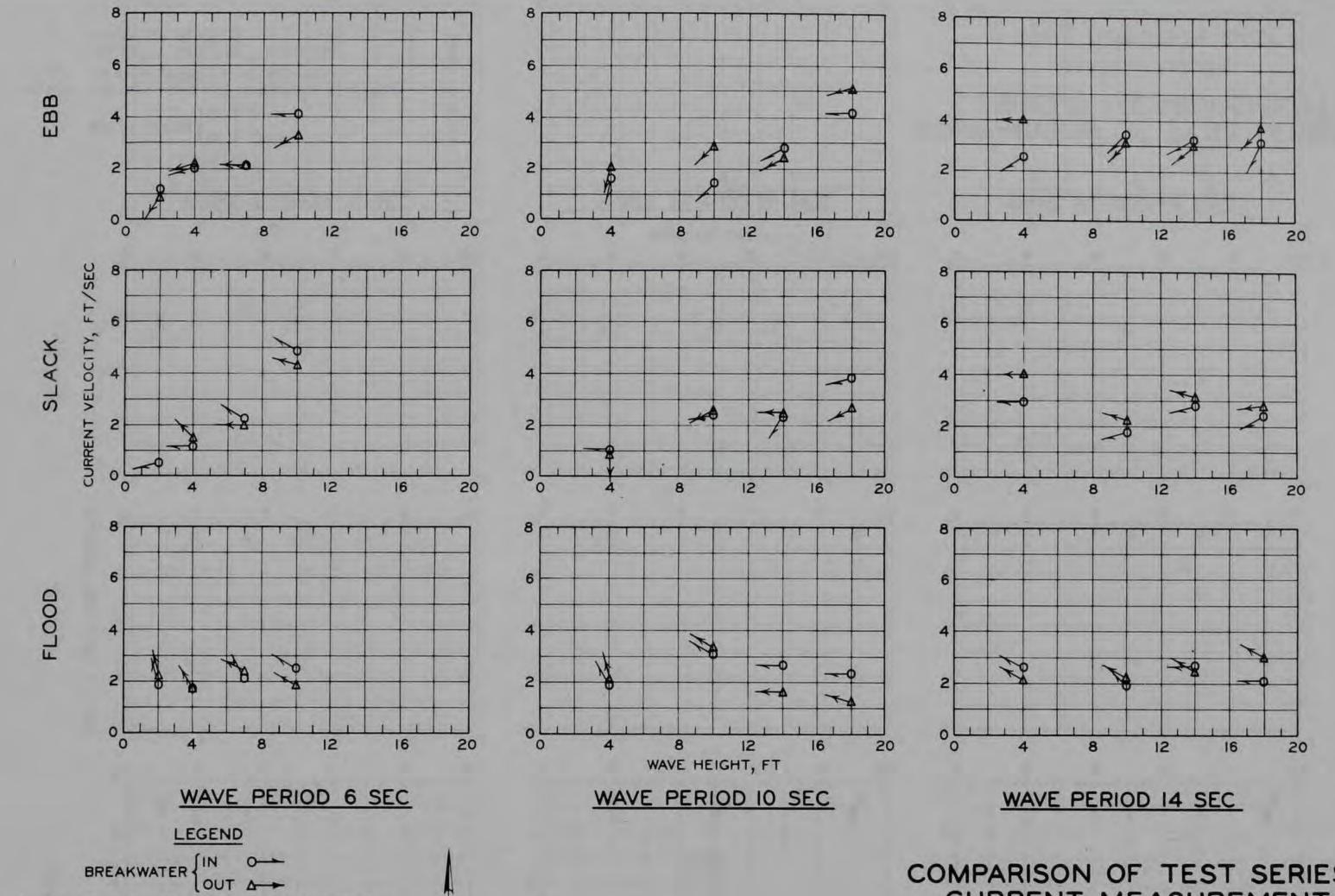
COMPARISON OF TEST SERIES I CURRENT MEASUREMENTS

STATION NO. 5B WAVE DIRECTION : EAST

NOTES: ARROWS INDICATE DIRECTION REFERRED TO NEW JERSEY GRID SYSTEM

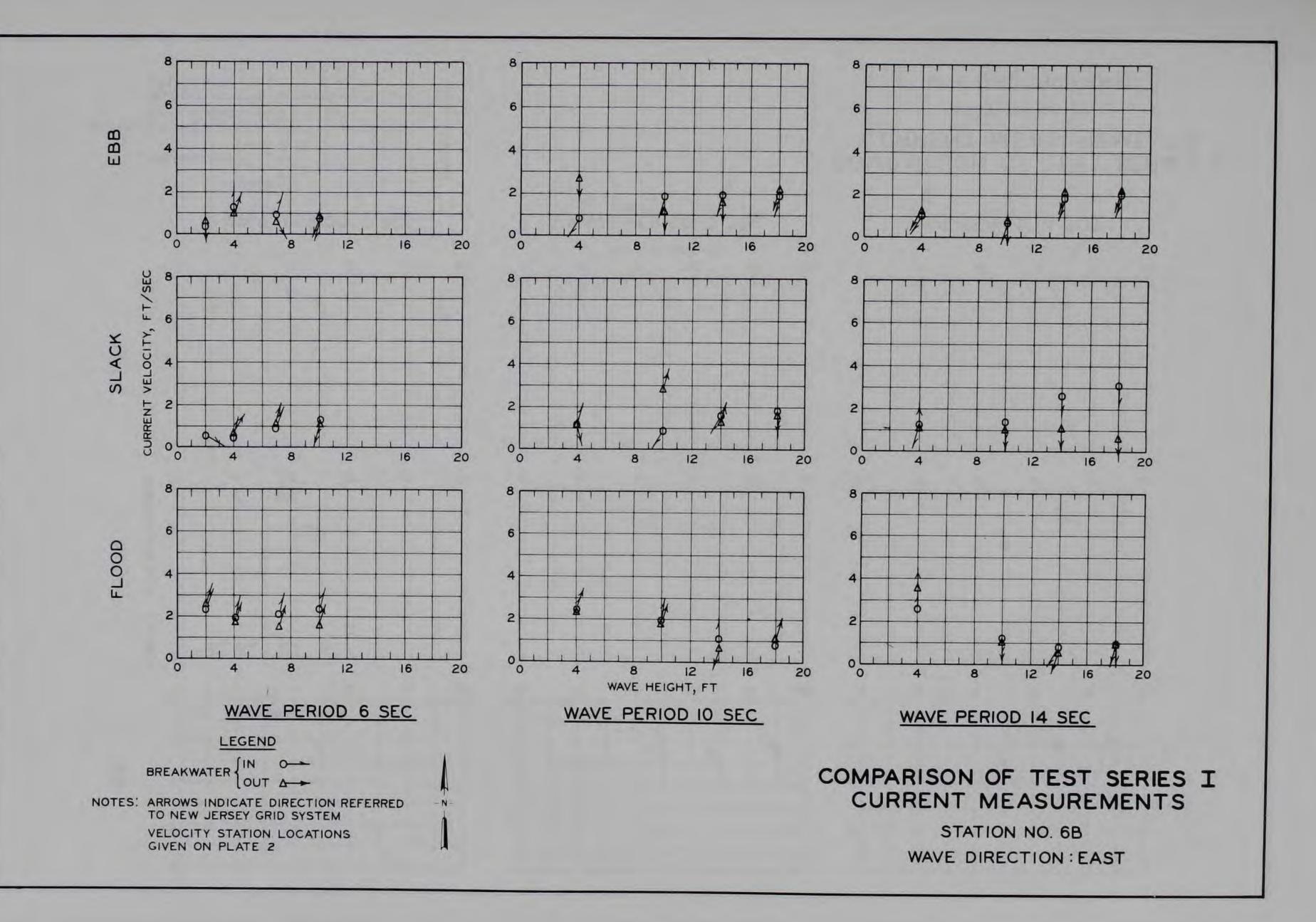
VELOCITY STATION LOCATIONS

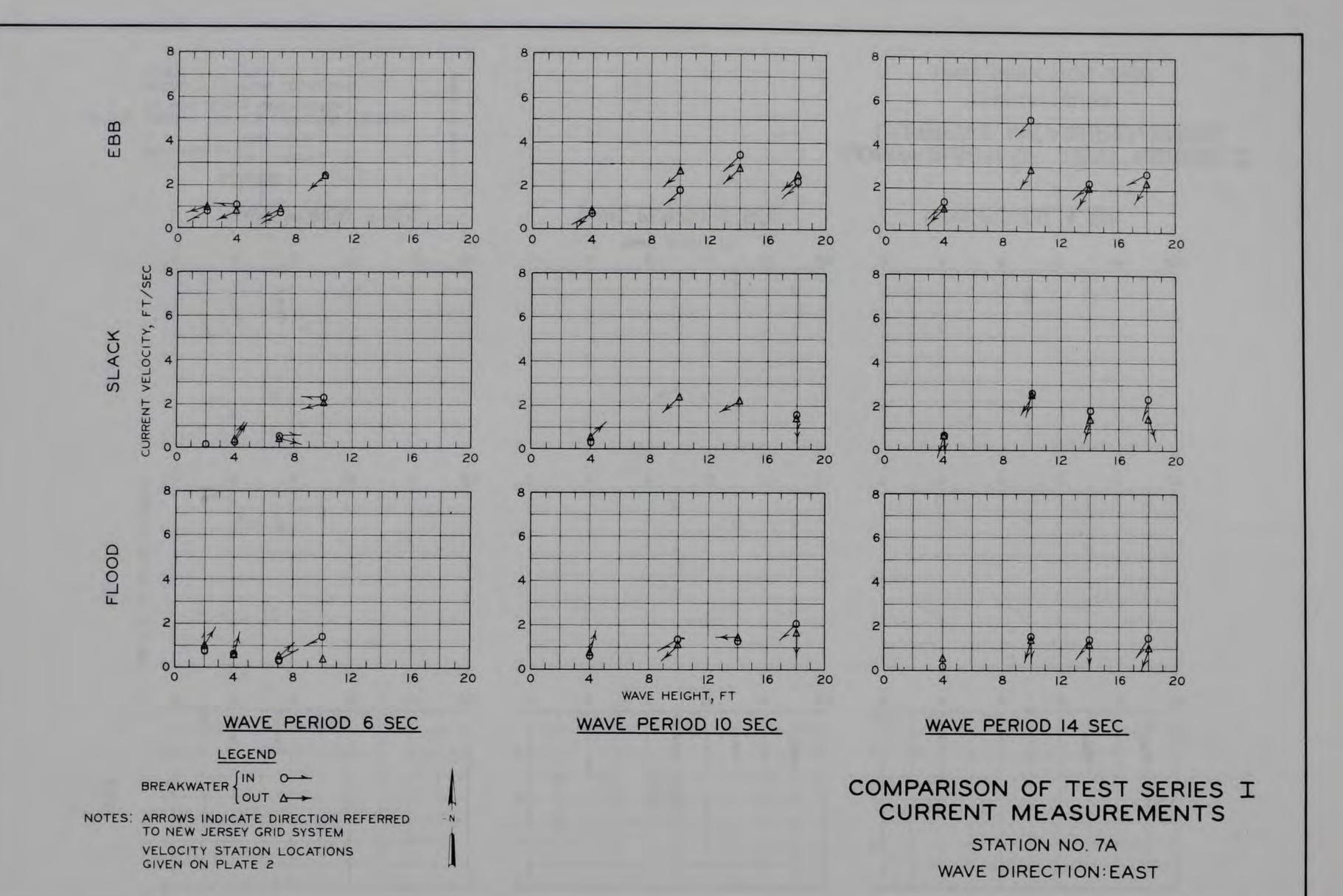
GIVEN ON PLATE 2

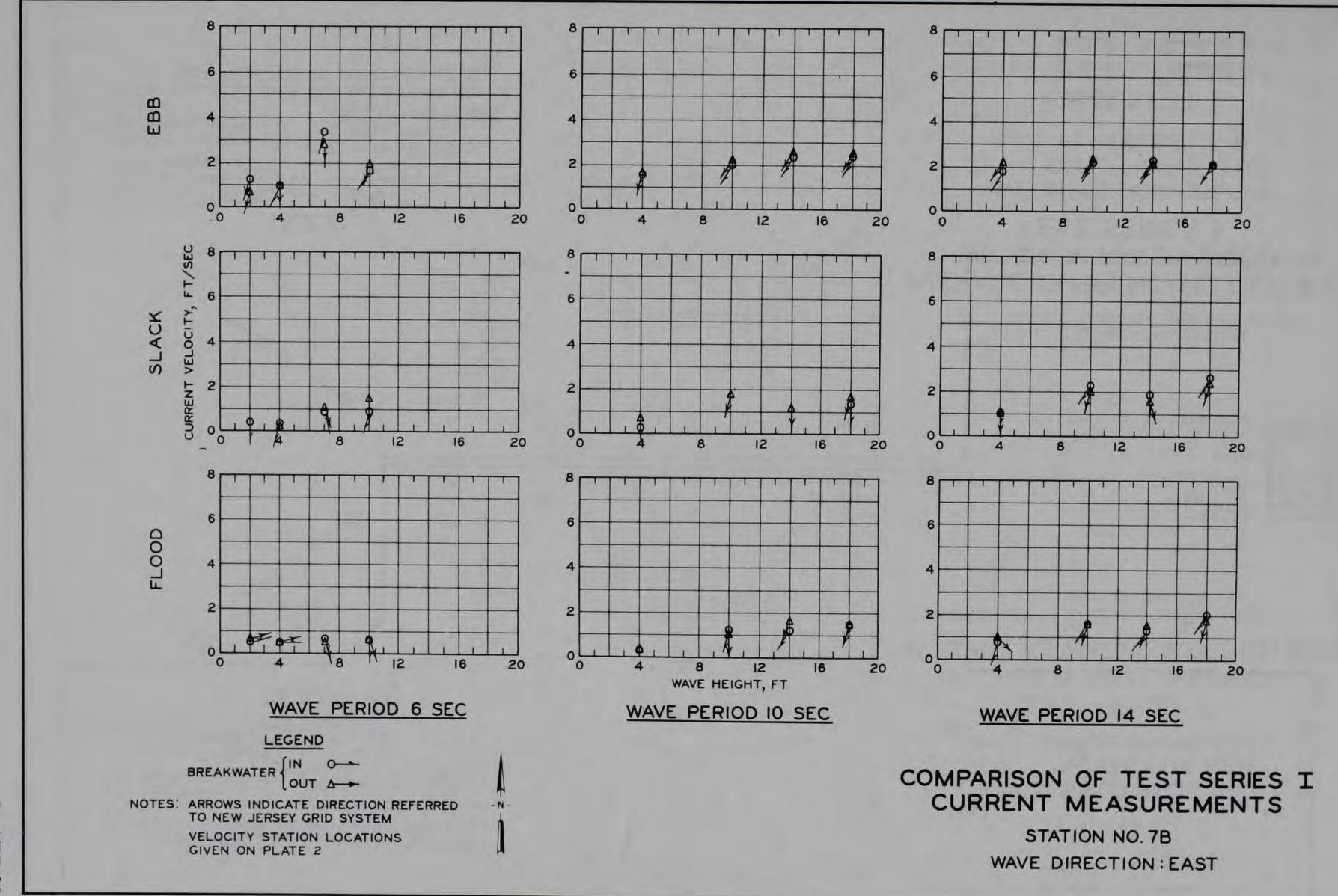


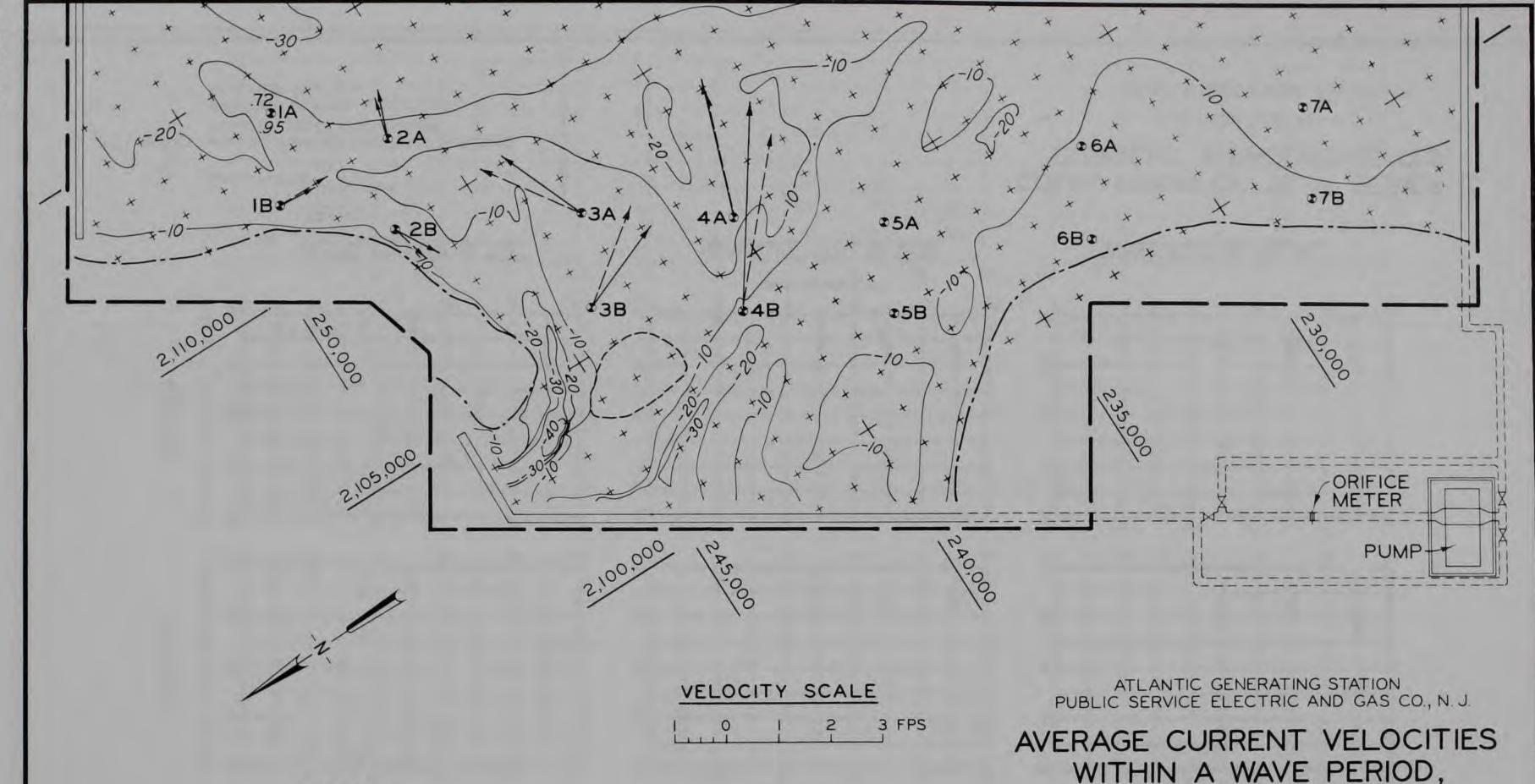
COMPARISON OF TEST SERIES I CURRENT MEASUREMENTS

STATION NO. 6A WAVE DIRECTION : EAST









LEGEND

WAVE HEIGHTS, FT: 2, 4, 7, & 10 WITHOUT BREAKWATER WITH BREAKWATER

VELOCITY (FT/SEC), NO PREDOMINANT DIRECTION DEFINABLE 1.65 BREAKWATER OUT 1.65 BREAKWATER IN

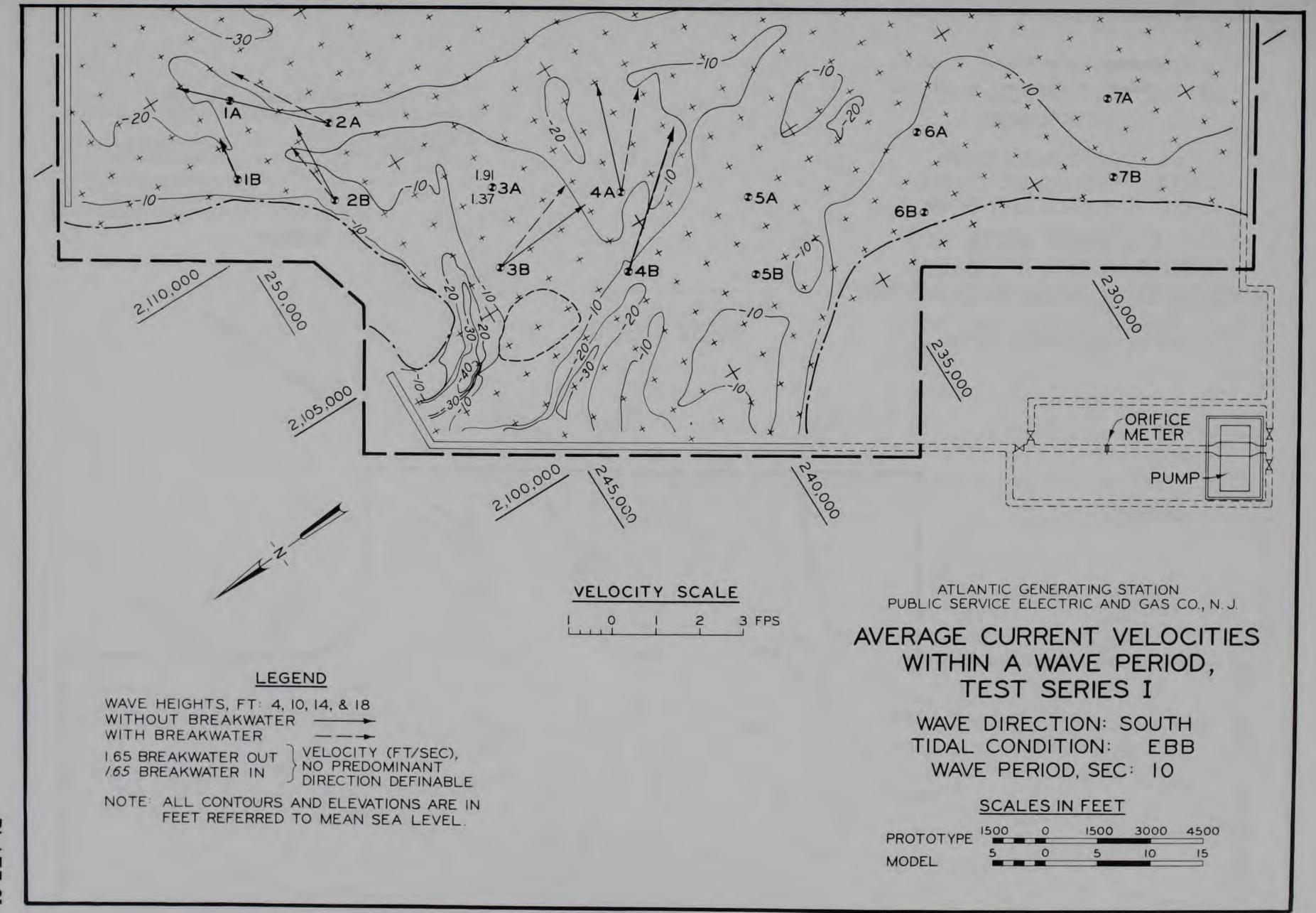
NOTE: ALL CONTOURS AND ELEVATIONS ARE IN

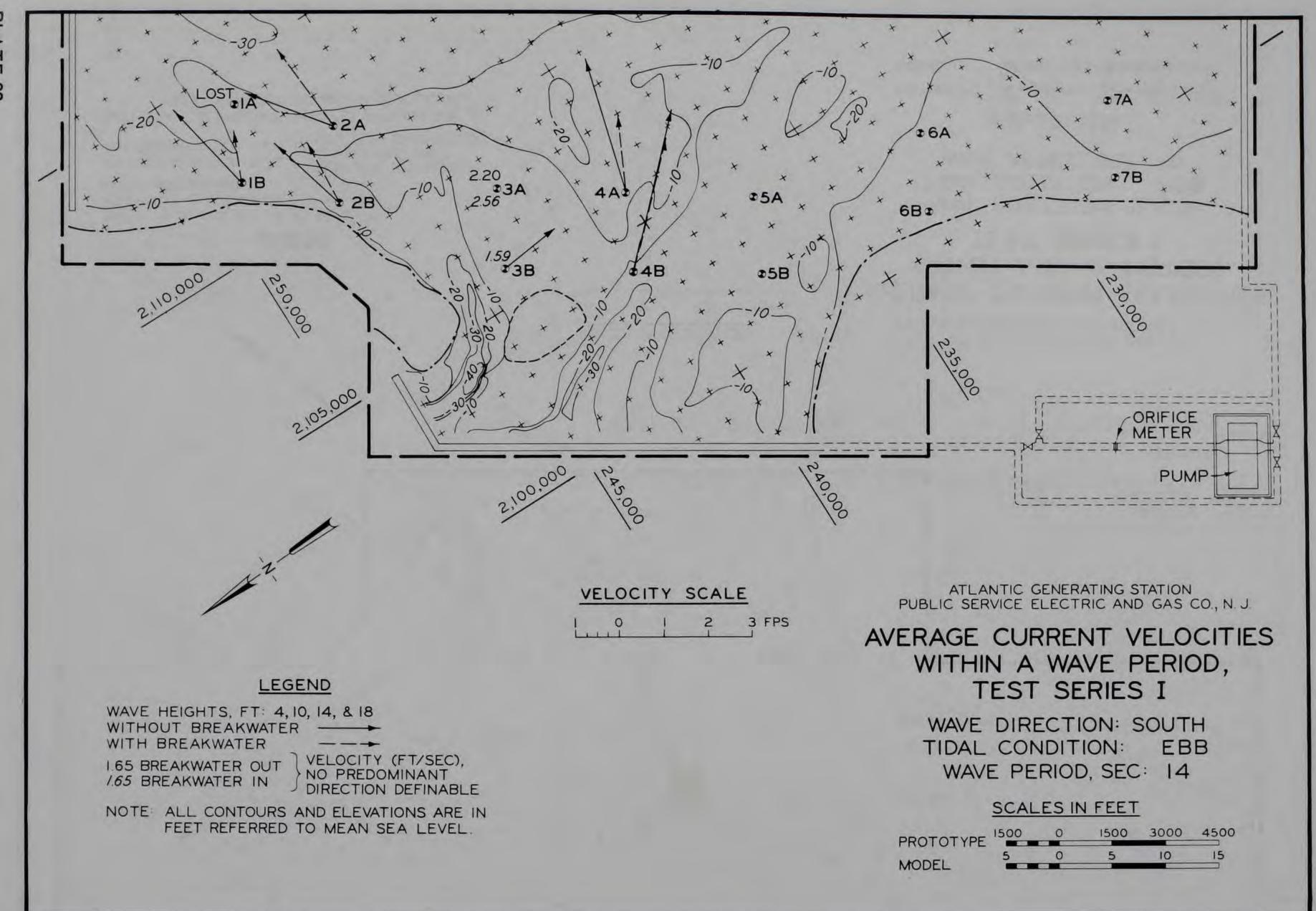
WITHIN A WAVE PERIOD, TEST SERIES I

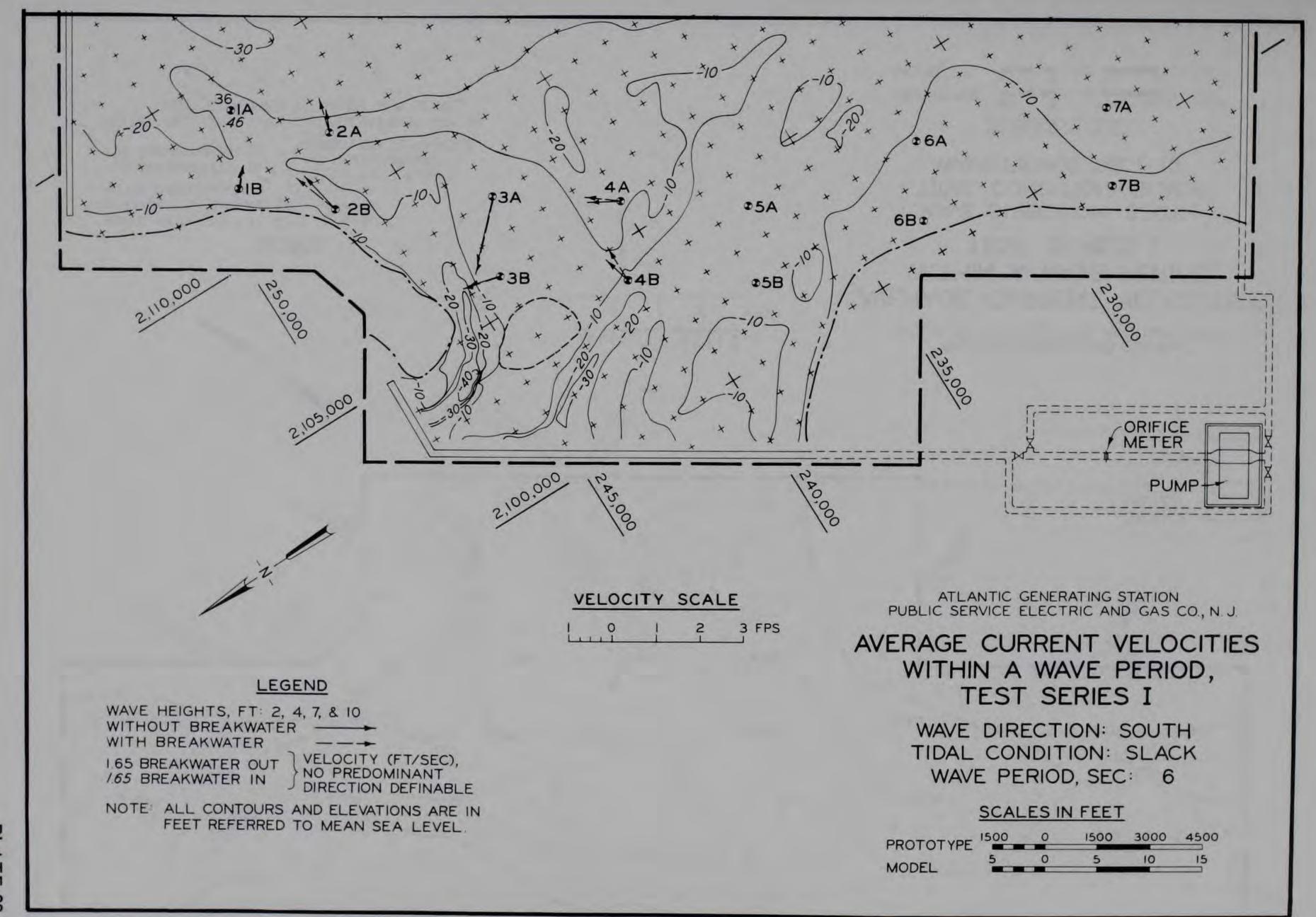
WAVE DIRECTION: SOUTH TIDAL CONDITION: EBB WAVE PERIOD, SEC:

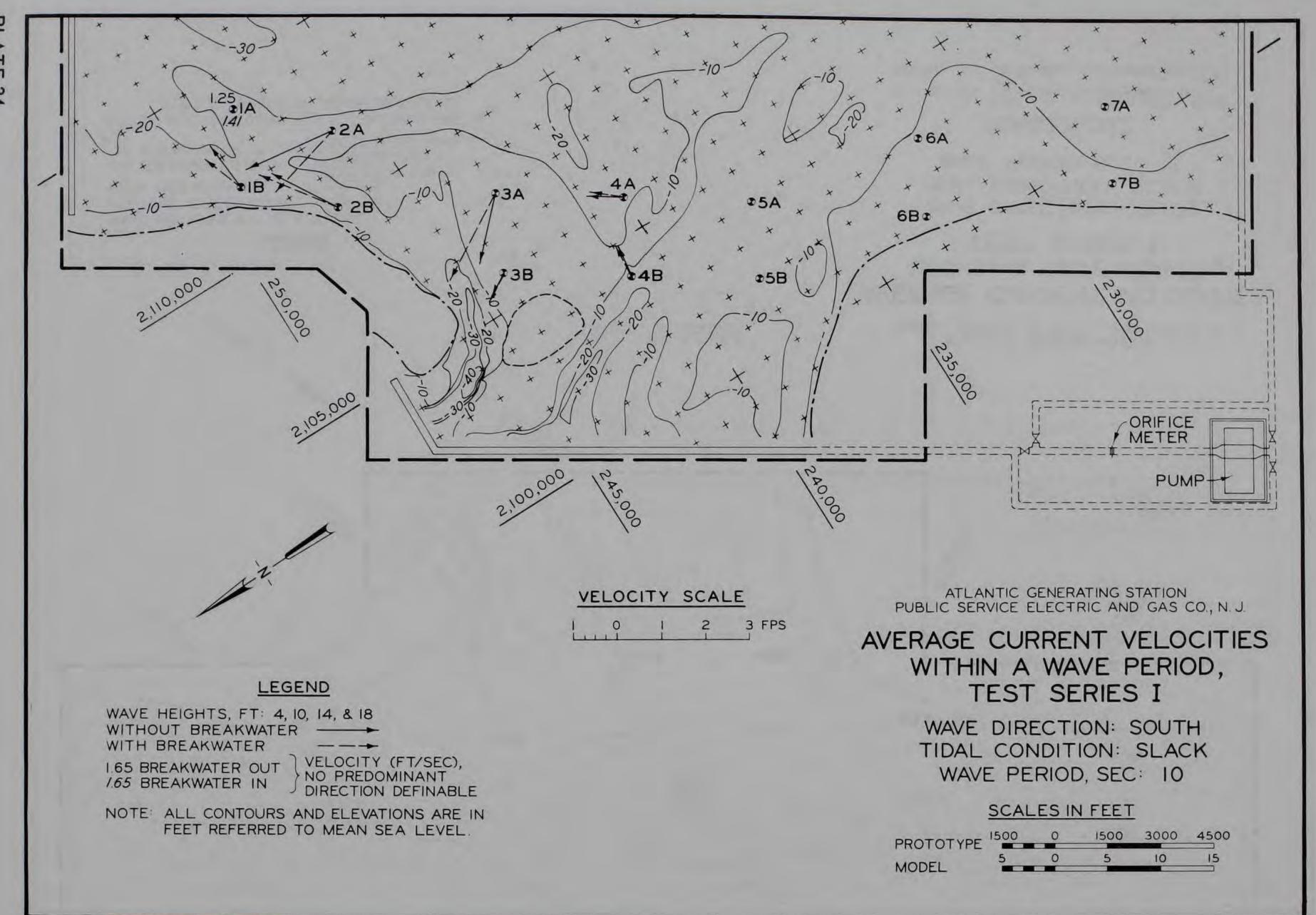
SCALES IN FEET

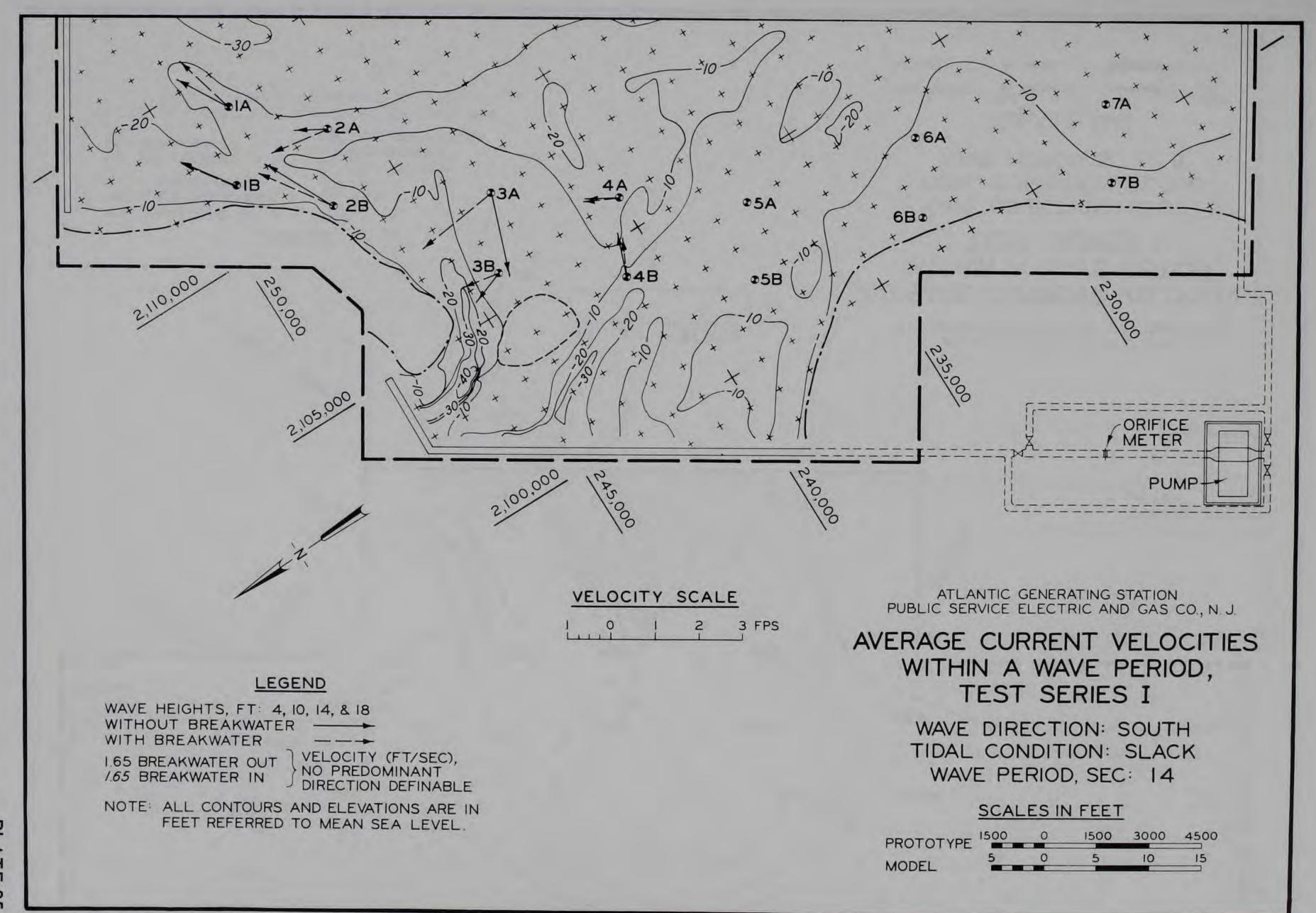
| PROTOTYPE 1 | 1500 | 0 | 1500 | 3000 | 4500 |
|-------------|------|---|------|------|------|
| | 5 | 0 | 5 | 10 | 15 |
| MODEL | | | | | |

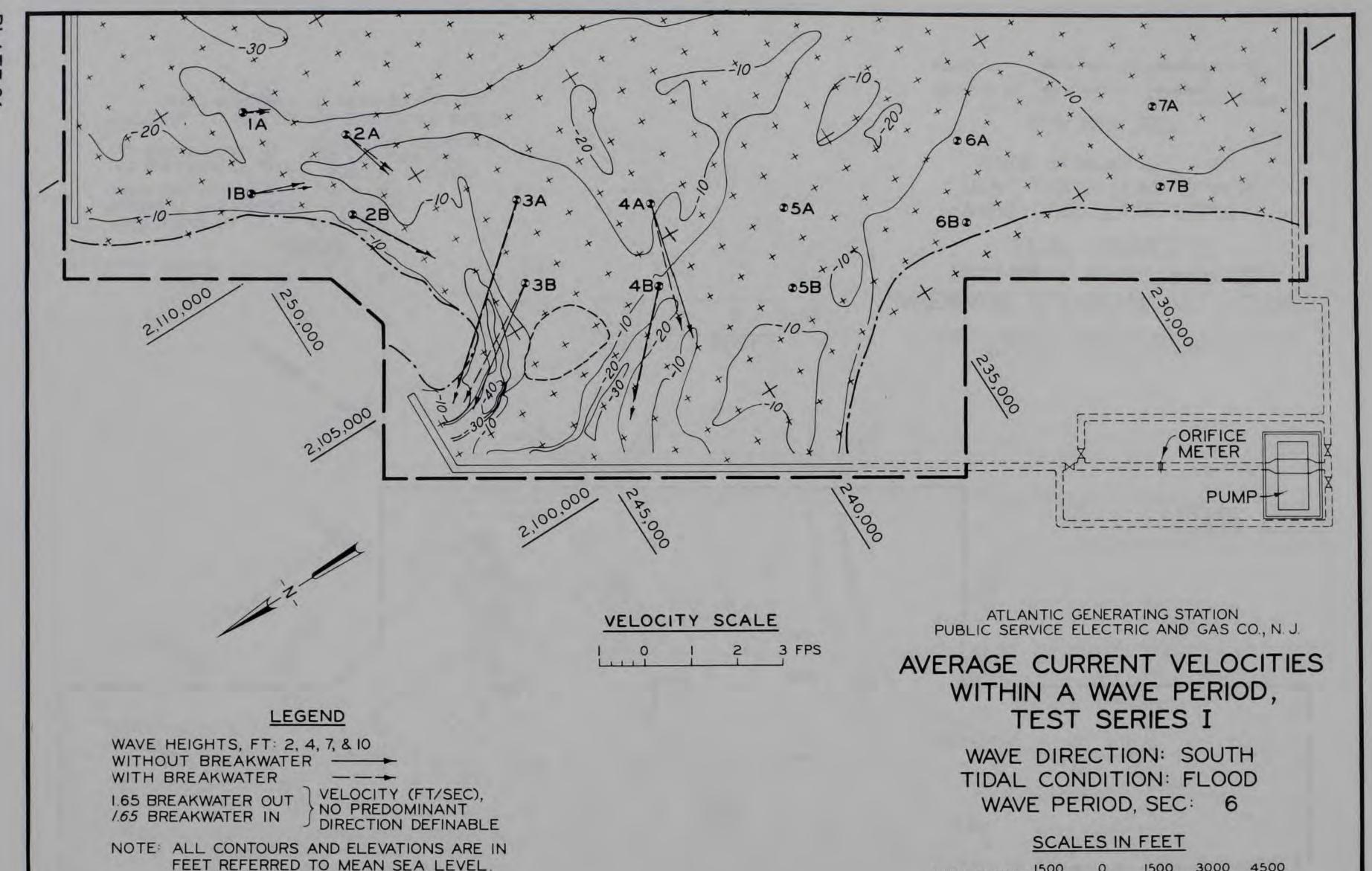






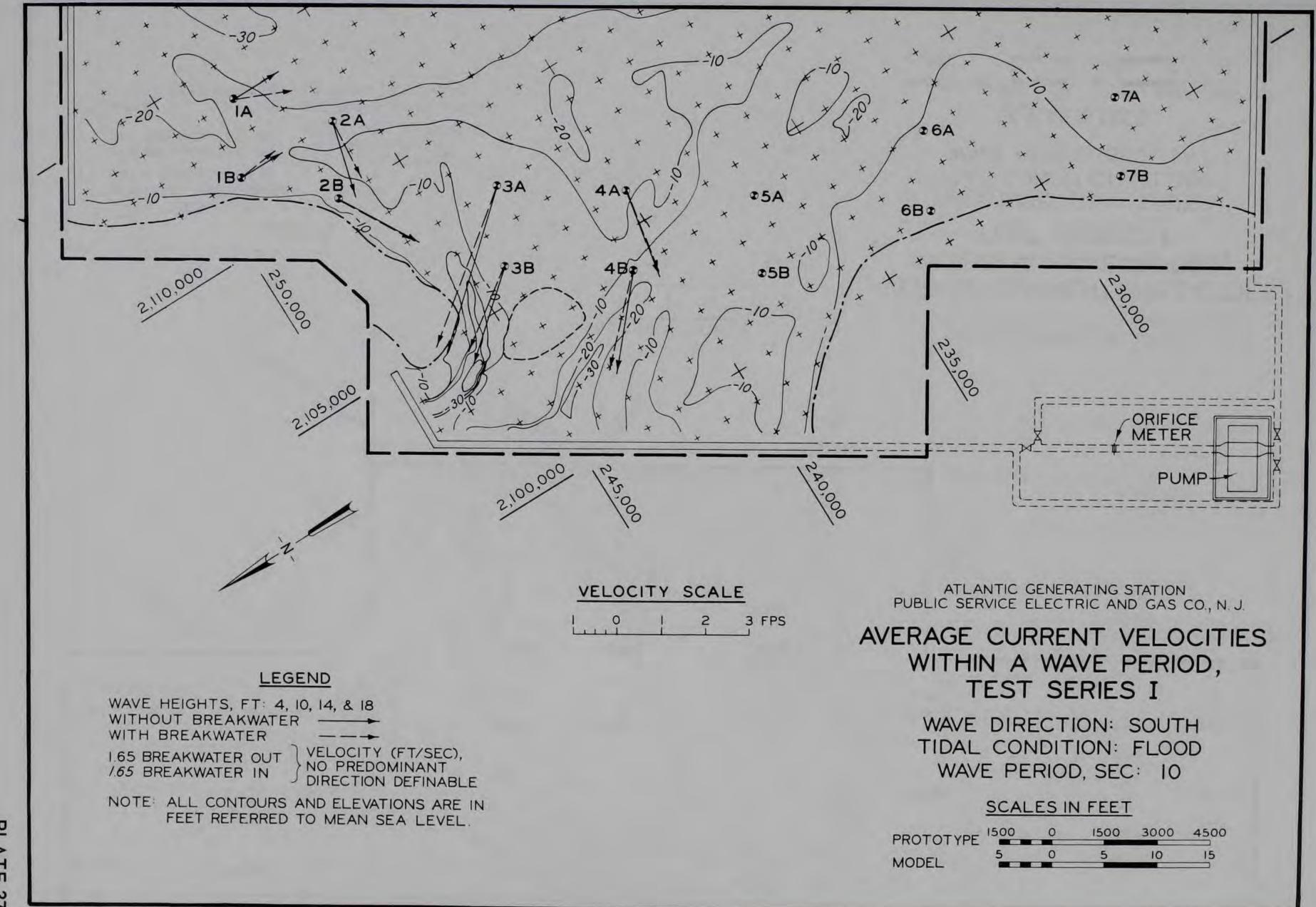


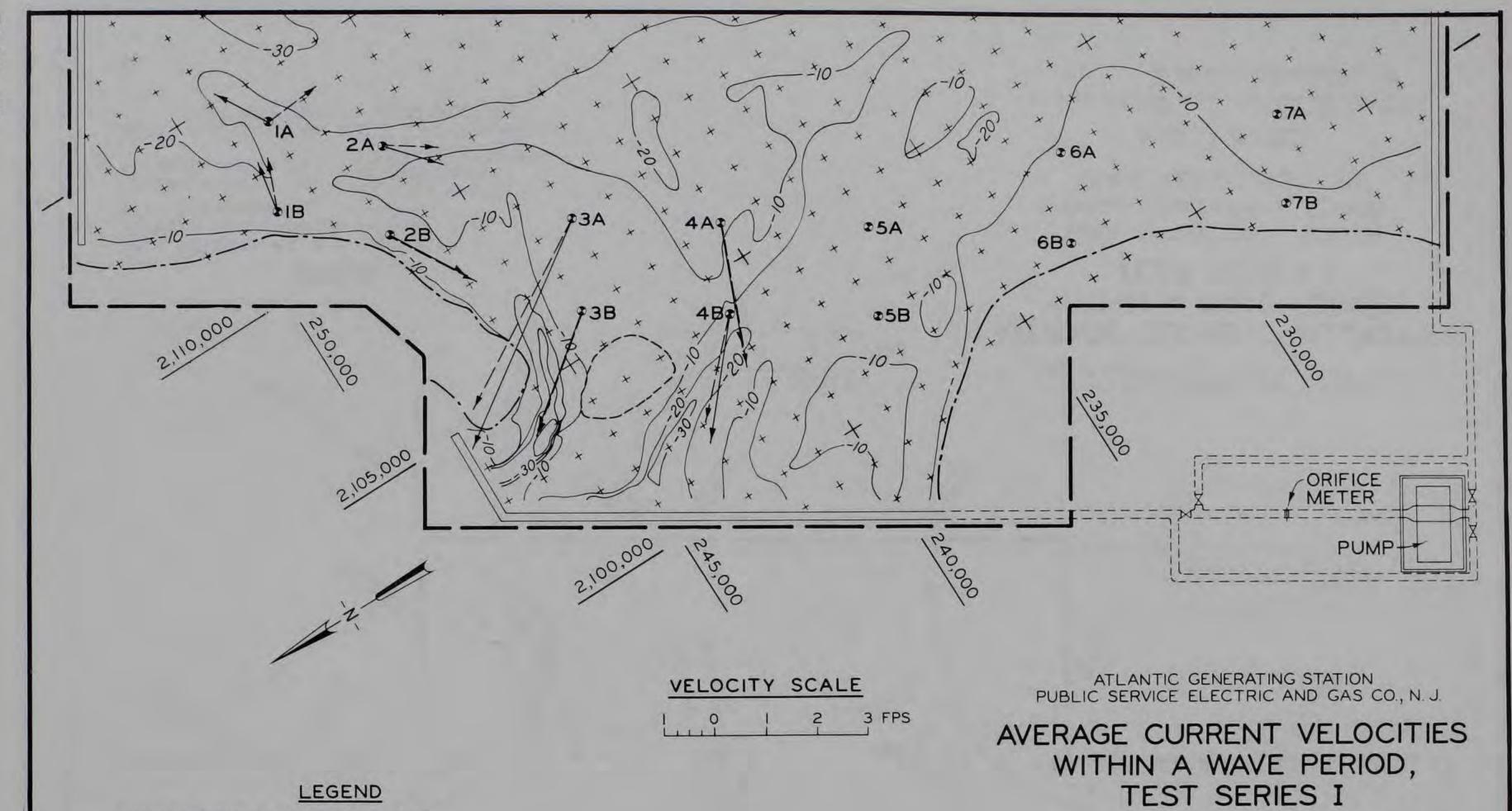




PROTOTYPE

MODEL





WAVE HEIGHTS, FT: 4, 10, 14, & 18
WITHOUT BREAKWATER

WITH BREAKWATER

→

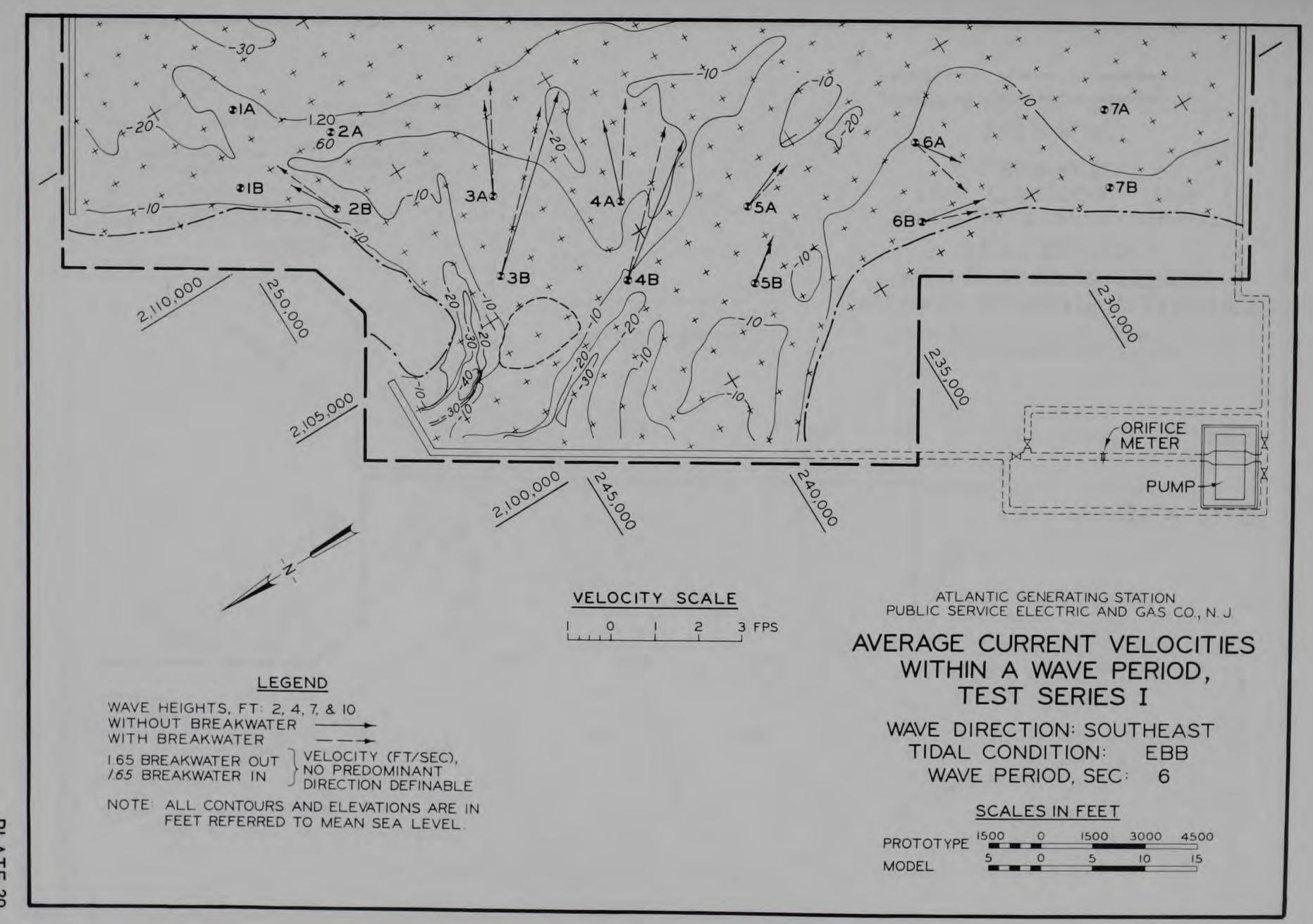
1.65 BREAKWATER OUT / VELOCITY (FT/SEC), NO PREDOMINANT DIRECTION DEFINABLE

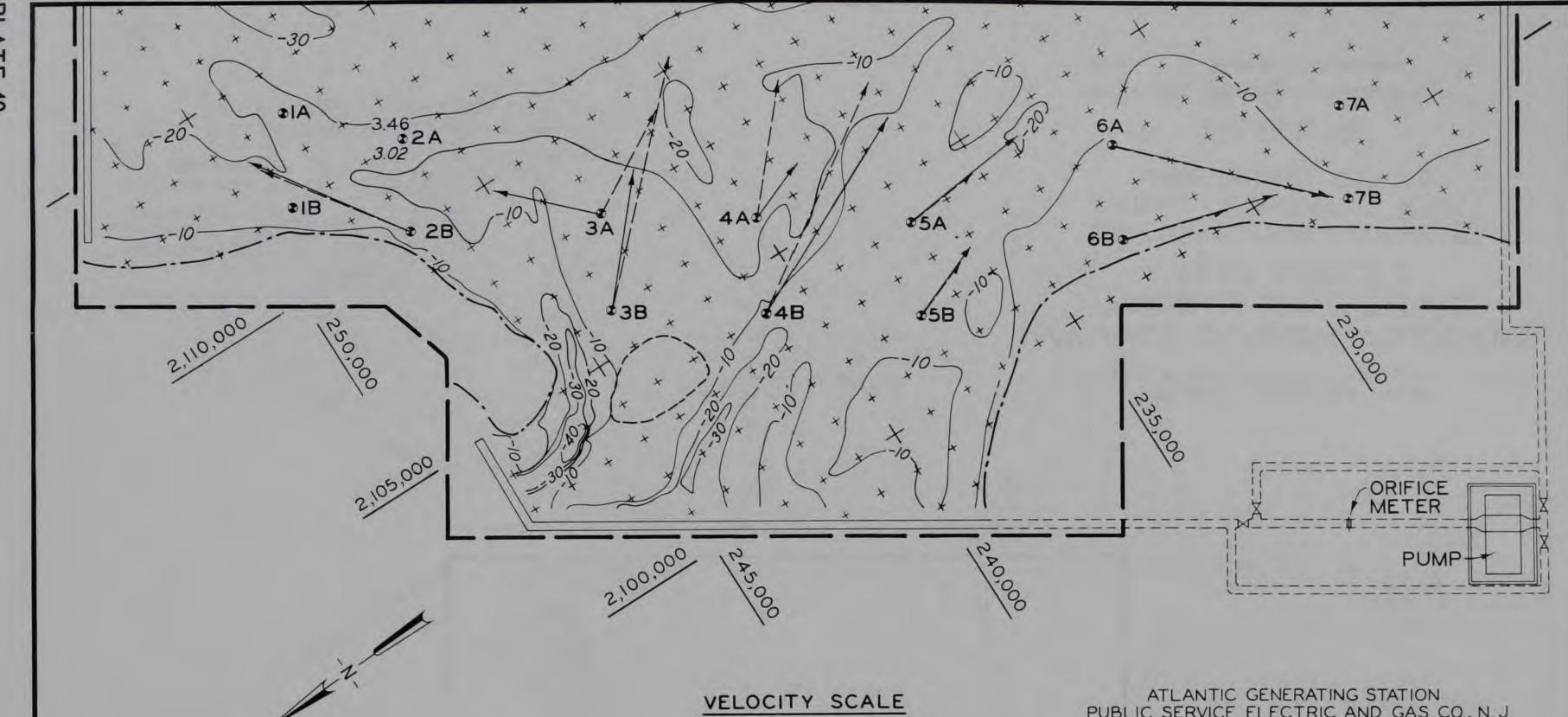
NOTE: ALL CONTOURS AND ELEVATIONS ARE IN FEET REFERRED TO MEAN SEA LEVEL.

WAVE DIRECTION: SOUTH TIDAL CONDITION: FLOOD WAVE PERIOD, SEC: 14

SCALES IN FEET

| PROTOTYPE | 1500 | 0 | 1500 | 3000 | 4500 |
|-----------|------|---|------|------|------|
| INOTOTIL | 5 | 0 | 5 | 10 | 15 |
| MODEL | | | | 10 | |





3 FPS

LEGEND

WAVE HEIGHTS, FT: 4, 10, 14, & 18 WITHOUT BREAKWATER WITH BREAKWATER

VELOCITY (FT/SEC), NO PREDOMINANT 1.65 BREAKWATER OUT 1.65 BREAKWATER IN DIRECTION DEFINABLE

NOTE: ALL CONTOURS AND ELEVATIONS ARE IN FEET REFERRED TO MEAN SEA LEVEL.

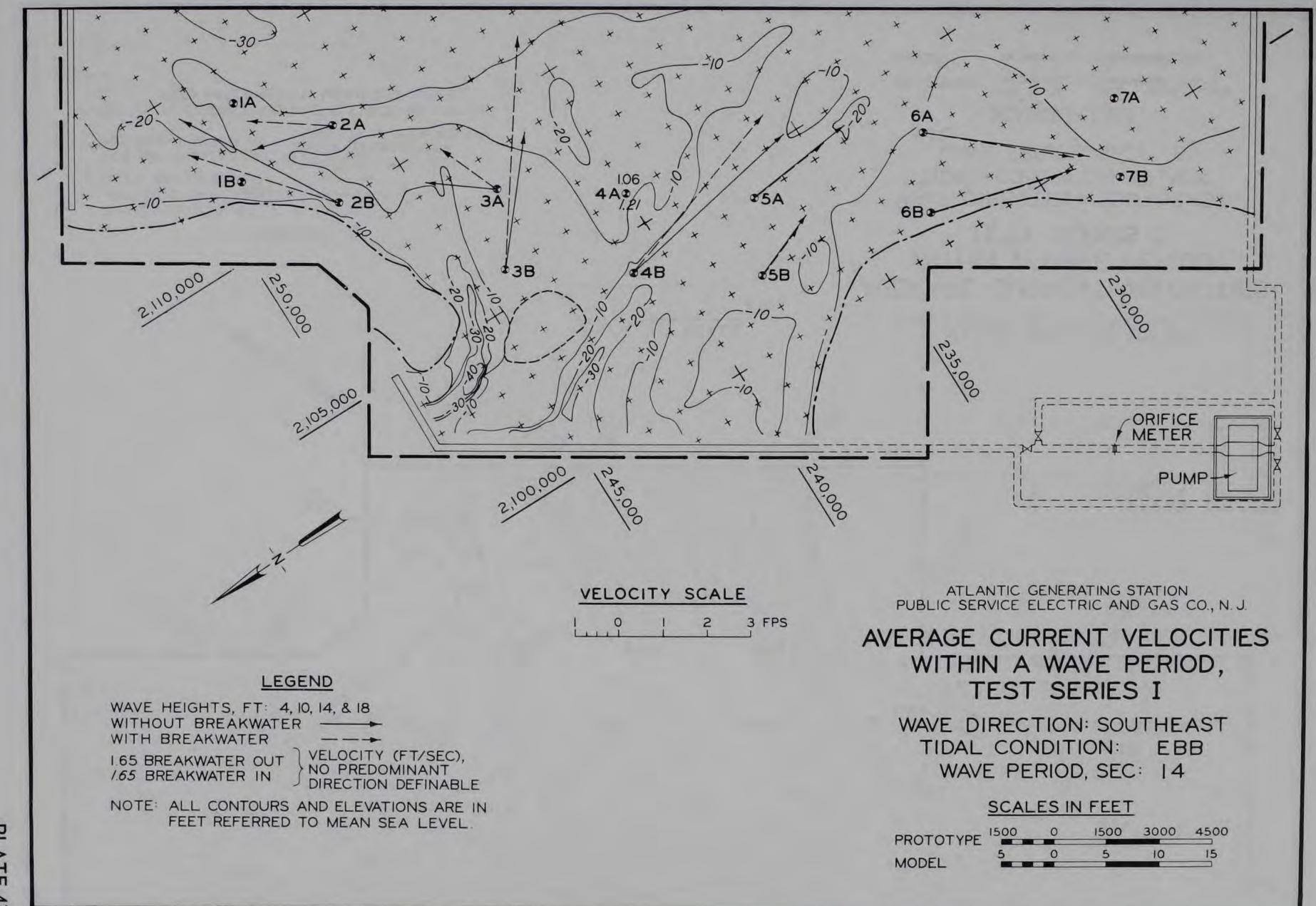
ATLANTIC GENERATING STATION PUBLIC SERVICE ELECTRIC AND GAS CO., N. J.

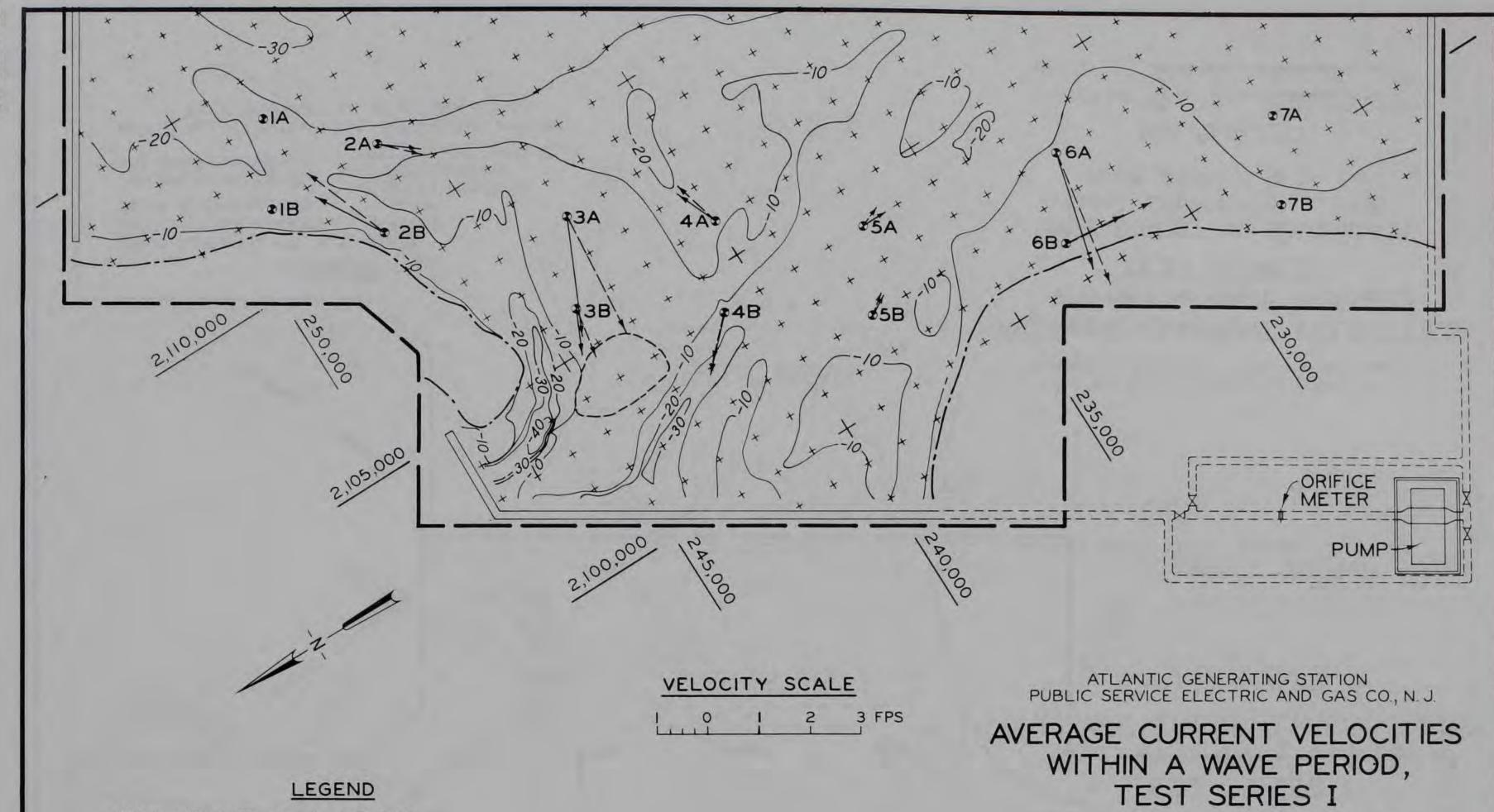
AVERAGE CURRENT VELOCITIES WITHIN A WAVE PERIOD, TEST SERIES I

WAVE DIRECTION: SOUTHEAST TIDAL CONDITION: EBB WAVE PERIOD, SEC: 10

SCALES IN FEET

| PROTOTYPE | 1500 | 0 | 1500 | 3000 | 4500 |
|-----------|------|---|------|------|------|
| | 5 | 0 | 5 | 10 | 15 |
| MODEL | | | | | |





WAVE HEIGHTS, FT: 2, 4, 7, & 10
WITHOUT BREAKWATER

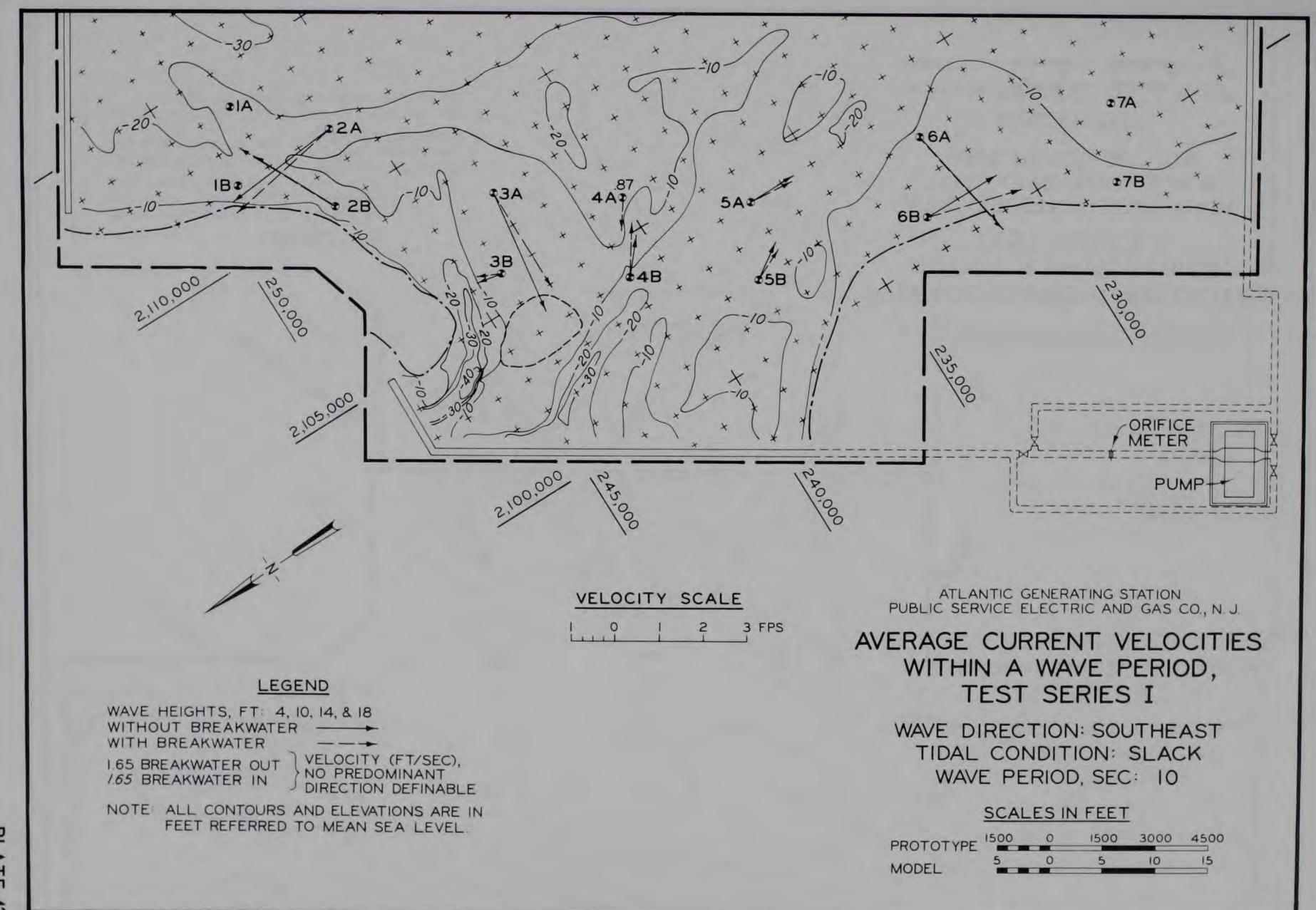
WITH BREAKWATER

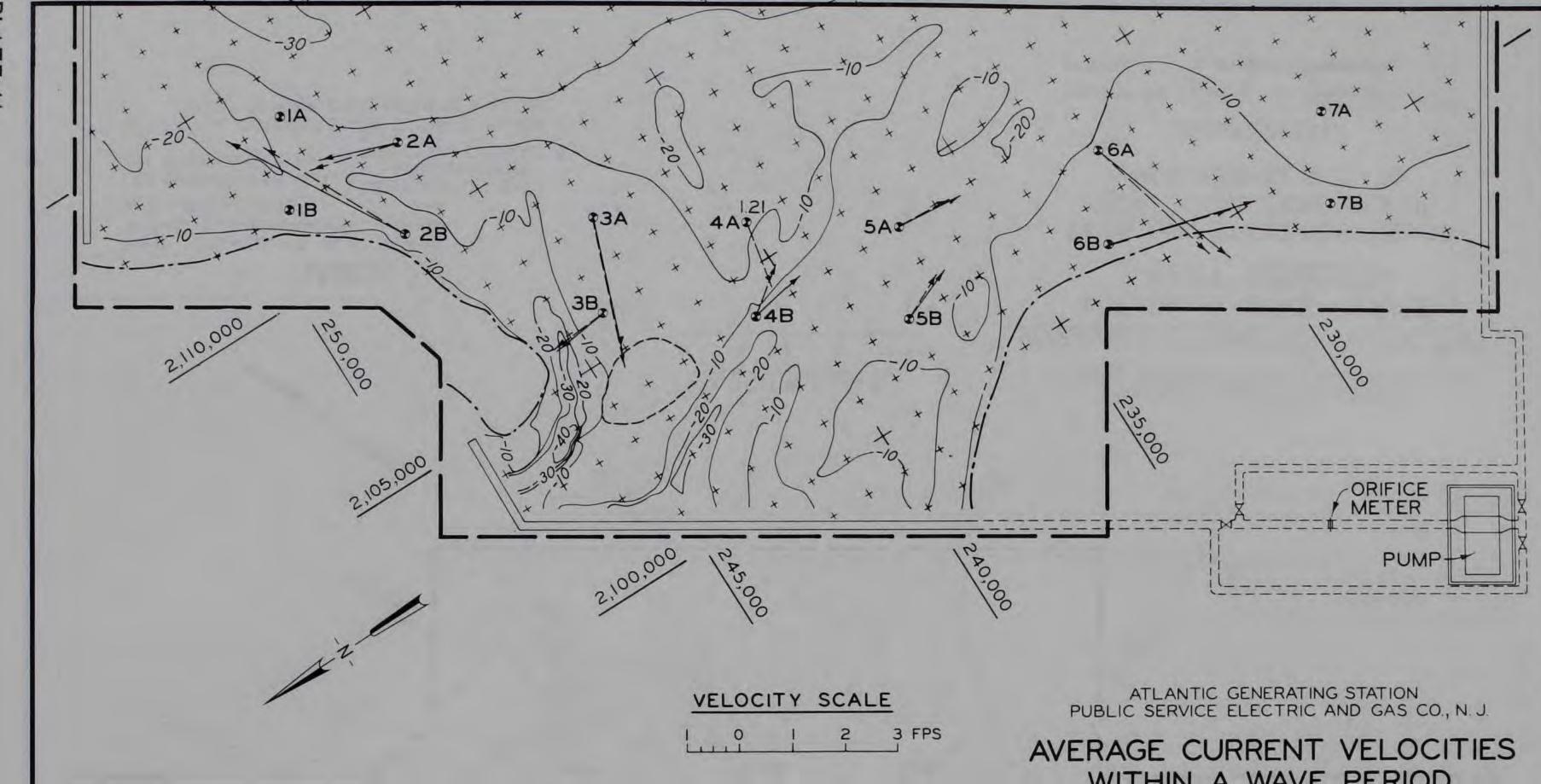
1.65 BREAKWATER OUT / VELOCITY (FT/SEC), NO PREDOMINANT DIRECTION DEFINABLE

NOTE: ALL CONTOURS AND ELEVATIONS ARE IN FEET REFERRED TO MEAN SEA LEVEL.

WAVE DIRECTION: SOUTHEAST TIDAL CONDITION: SLACK WAVE PERIOD, SEC: 6

| PROTOTYPE | 1500 | 0 | 1500 | 3000 | 4500 |
|-----------|------|---|------|------|------|
| PROTOTIFE | 5 | 0 | 5 | 10 | 15 |
| MODEL | | | | 10 | |





WAVE HEIGHTS, FT: 4, 10, 14, & 18 WITHOUT BREAKWATER WITH BREAKWATER

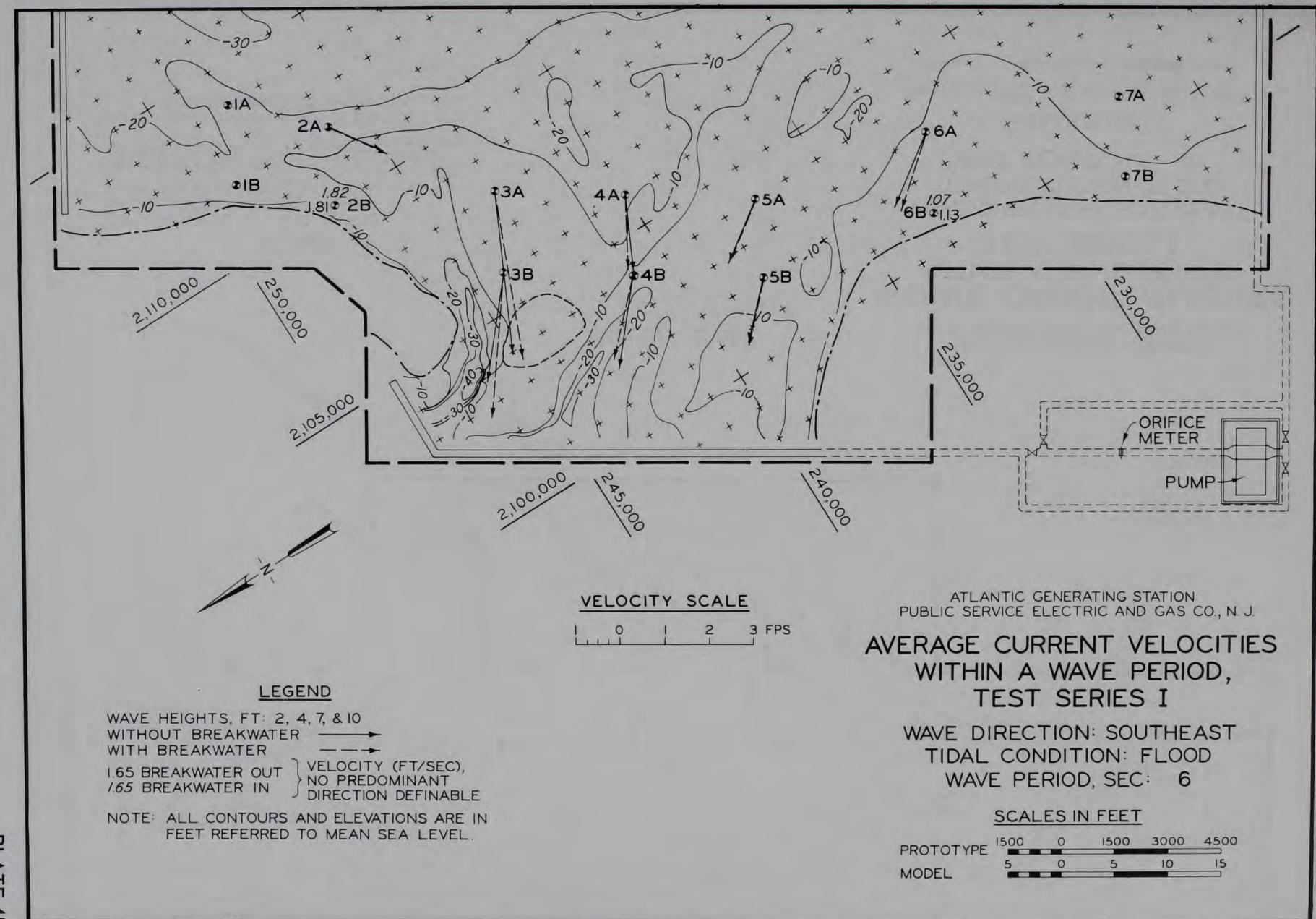
VELOCITY (FT/SEC), NO PREDOMINANT 1.65 BREAKWATER OUT 1.65 BREAKWATER IN

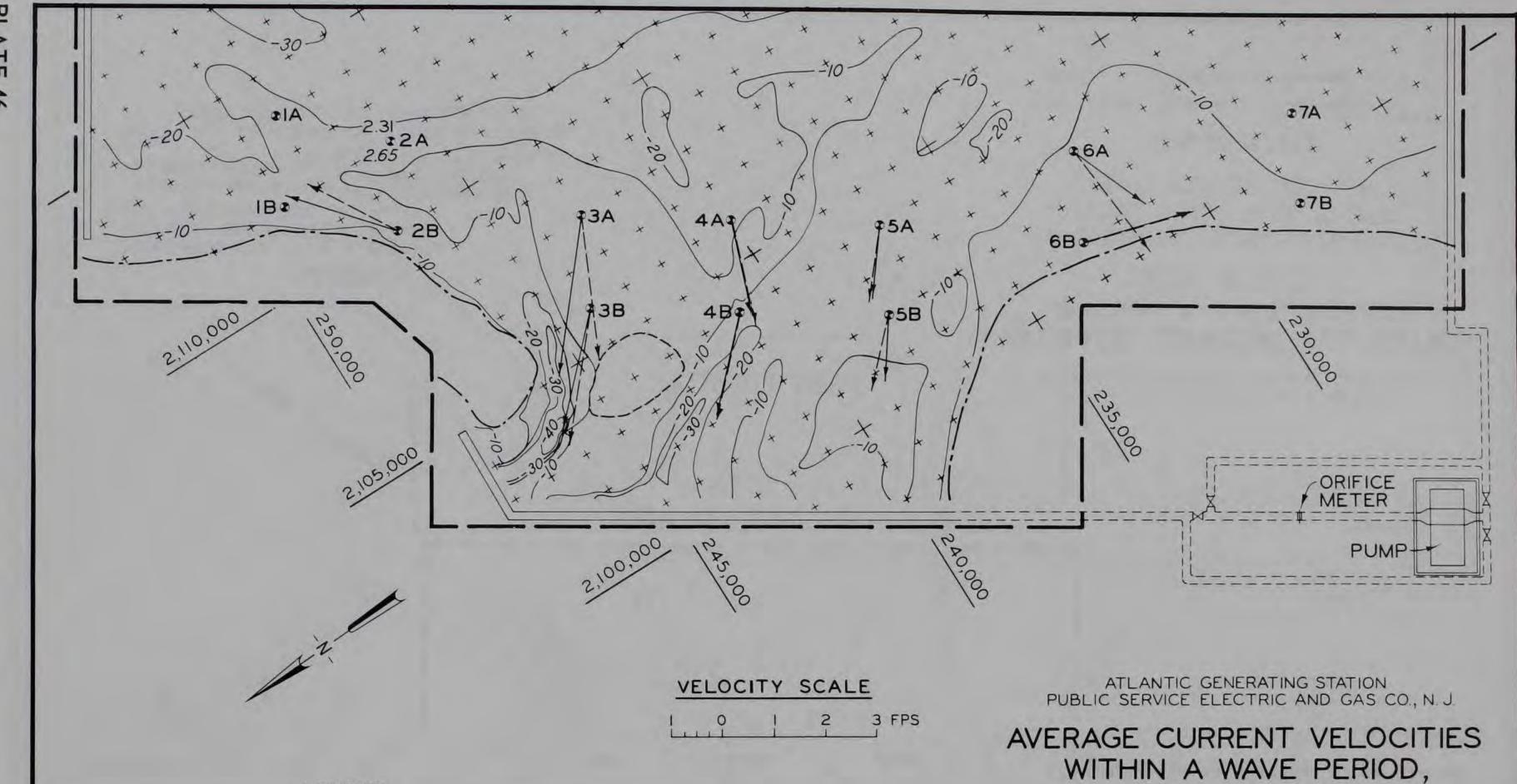
NOTE: ALL CONTOURS AND ELEVATIONS ARE IN FEET REFERRED TO MEAN SEA LEVEL.

WITHIN A WAVE PERIOD, TEST SERIES I

WAVE DIRECTION: SOUTHEAST TIDAL CONDITION: SLACK WAVE PERIOD, SEC: 14

| PROTOTYPE | 1500 | 0 | 1500 | 3000 | 4500 |
|-----------|------|---|------|------|------|
| INOTOTIL | 5 | 0 | 5 | 10 | 15 |
| MODEL | | | | 10 | |





WAVE HEIGHTS, FT: 4, 10, 14, & 18 WITHOUT BREAKWATER WITH BREAKWATER

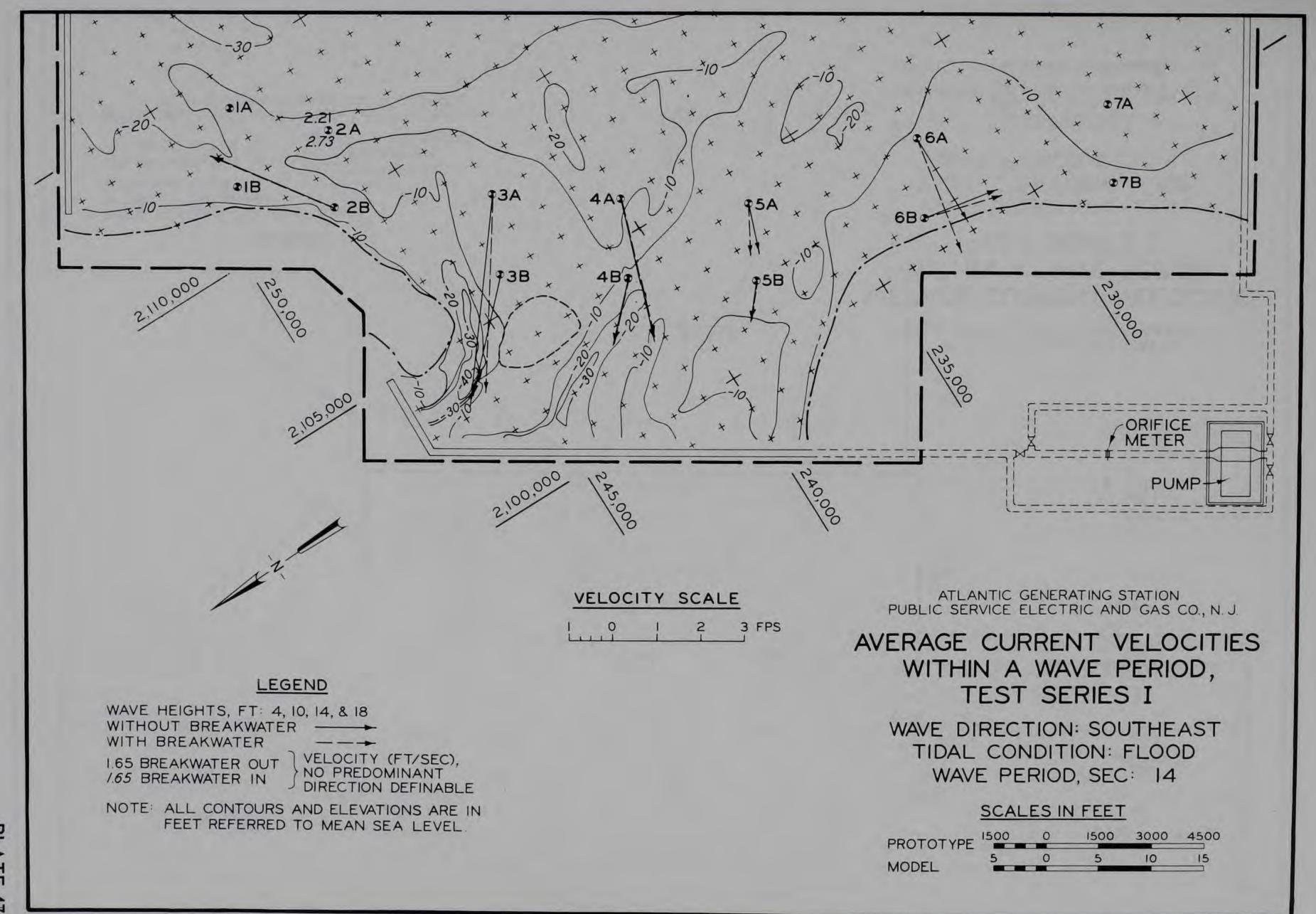
VELOCITY (FT/SEC), NO PREDOMINANT DIRECTION DEFINABLE 1.65 BREAKWATER OUT 1.65 BREAKWATER IN

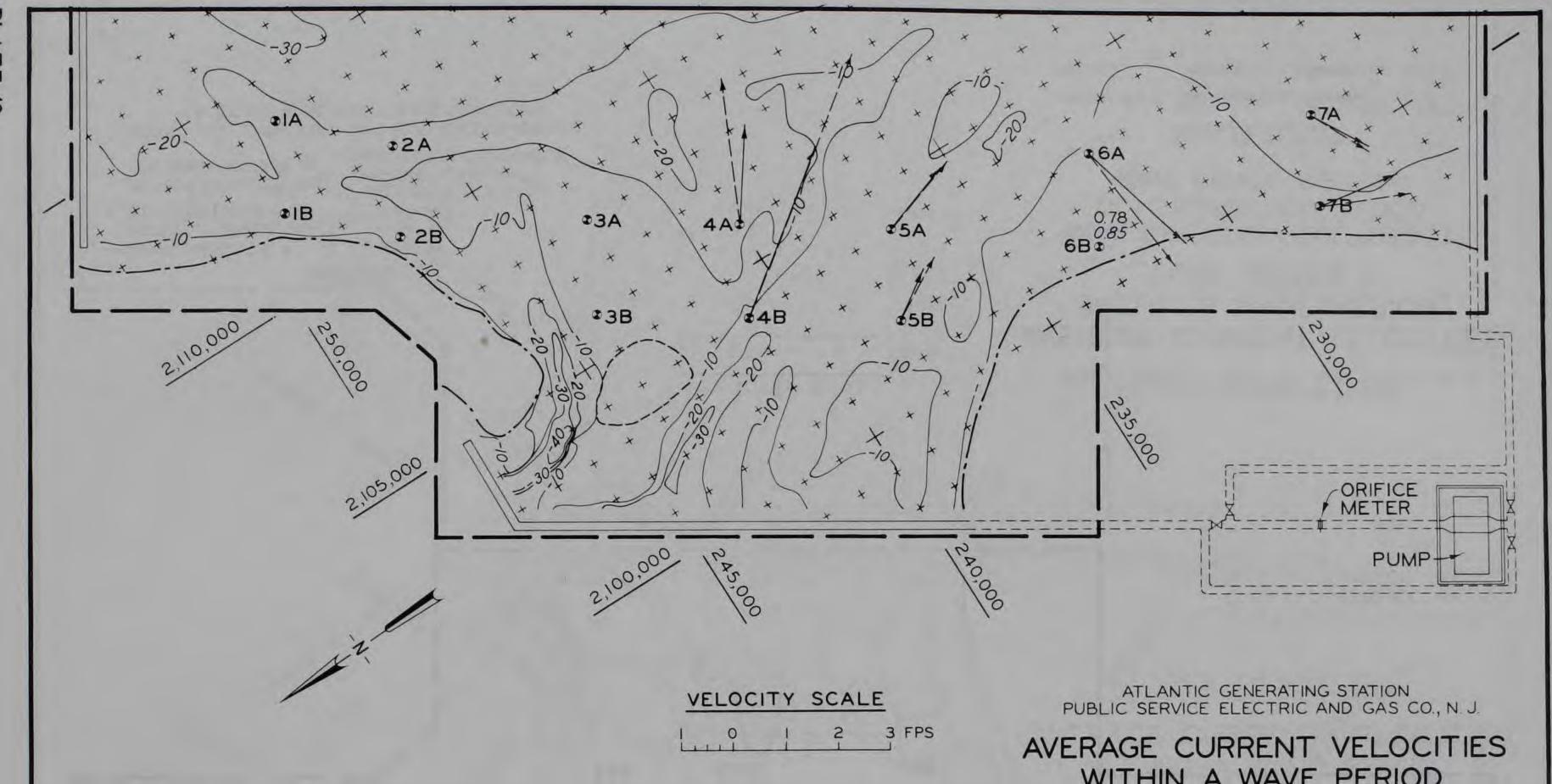
NOTE: ALL CONTOURS AND ELEVATIONS ARE IN FEET REFERRED TO MEAN SEA LEVEL.

WITHIN A WAVE PERIOD, TEST SERIES I

WAVE DIRECTION: SOUTHEAST TIDAL CONDITION: FLOOD WAVE PERIOD, SEC: 10

| PROTOTYPE | 1500 | 0 | 1500 | 3000 | 4500 |
|-----------|------|---|------|------|------|
| | 5 | 0 | 5 | 10 | 15 |
| MODEL | | | | | |





WAVE HEIGHTS, FT: 2, 4, 7, & 10 WITHOUT BREAKWATER WITH BREAKWATER

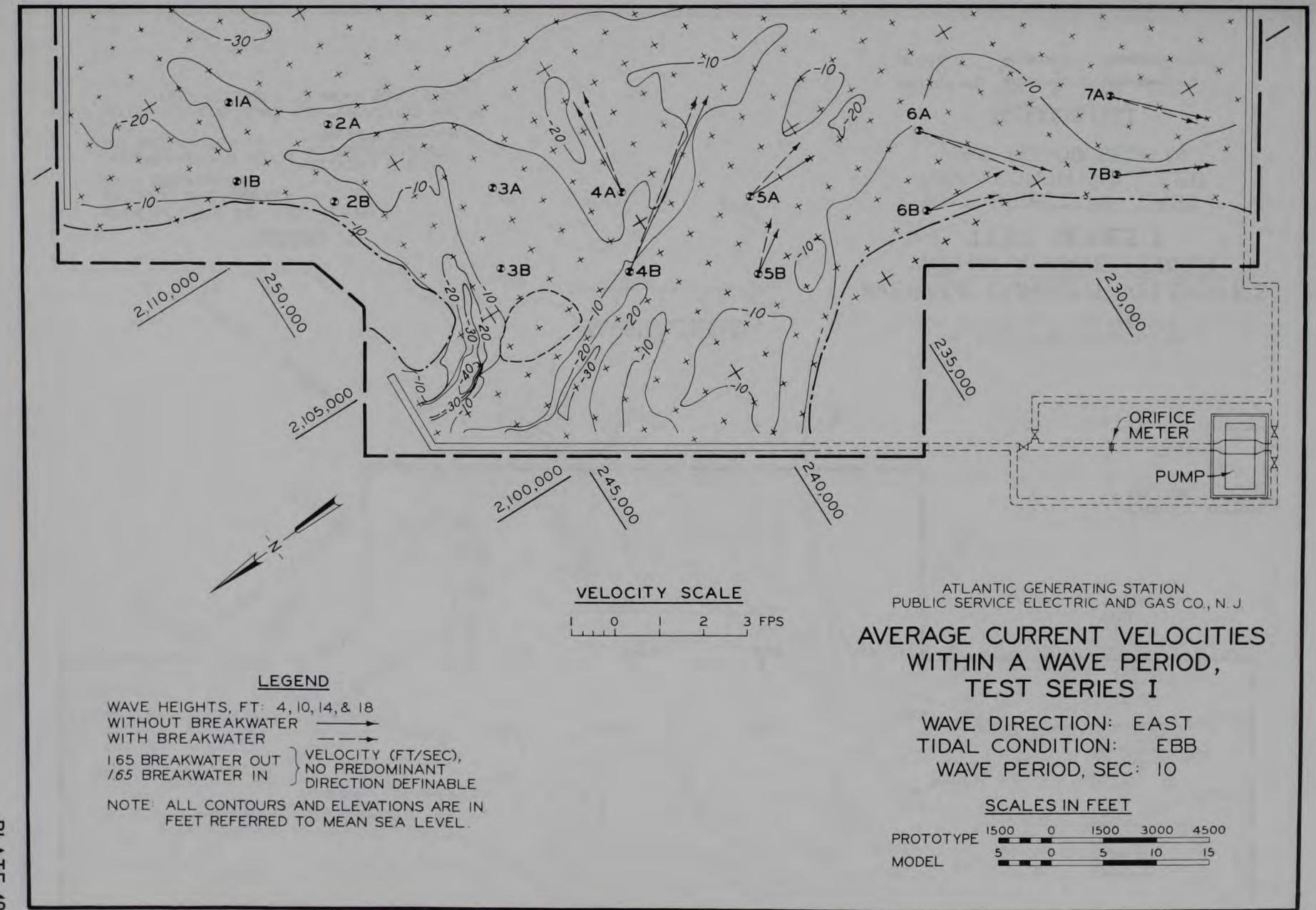
VELOCITY (FT/SEC), NO PREDOMINANT DIRECTION DEFINABLE 1.65 BREAKWATER OUT 1.65 BREAKWATER IN

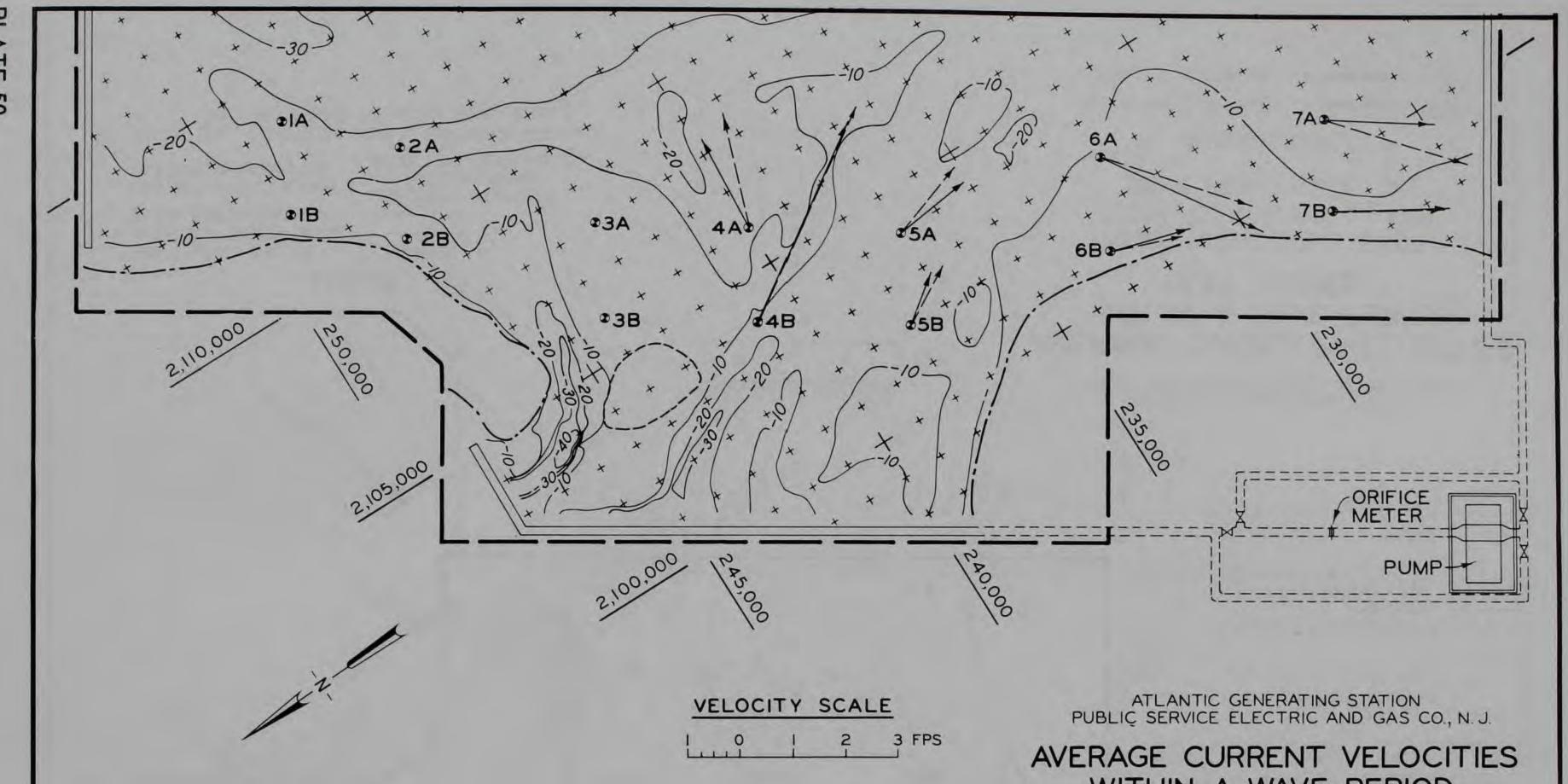
NOTE: ALL CONTOURS AND ELEVATIONS ARE IN FEET REFERRED TO MEAN SEA LEVEL.

WITHIN A WAVE PERIOD, TEST SERIES I

WAVE DIRECTION: EAST TIDAL CONDITION: EBB WAVE PERIOD, SEC: 6

| PROTOTYPE | 1500 | 0 | 1500 | 3000 | 4500 |
|-----------|------|---|------|------|------|
| | 5 | 0 | 5 | 10 | 15 |
| MODEL | | | | | |





WAVE HEIGHTS, FT: 4, 10, 14, & 18
WITHOUT BREAKWATER
WITH BREAKWATER

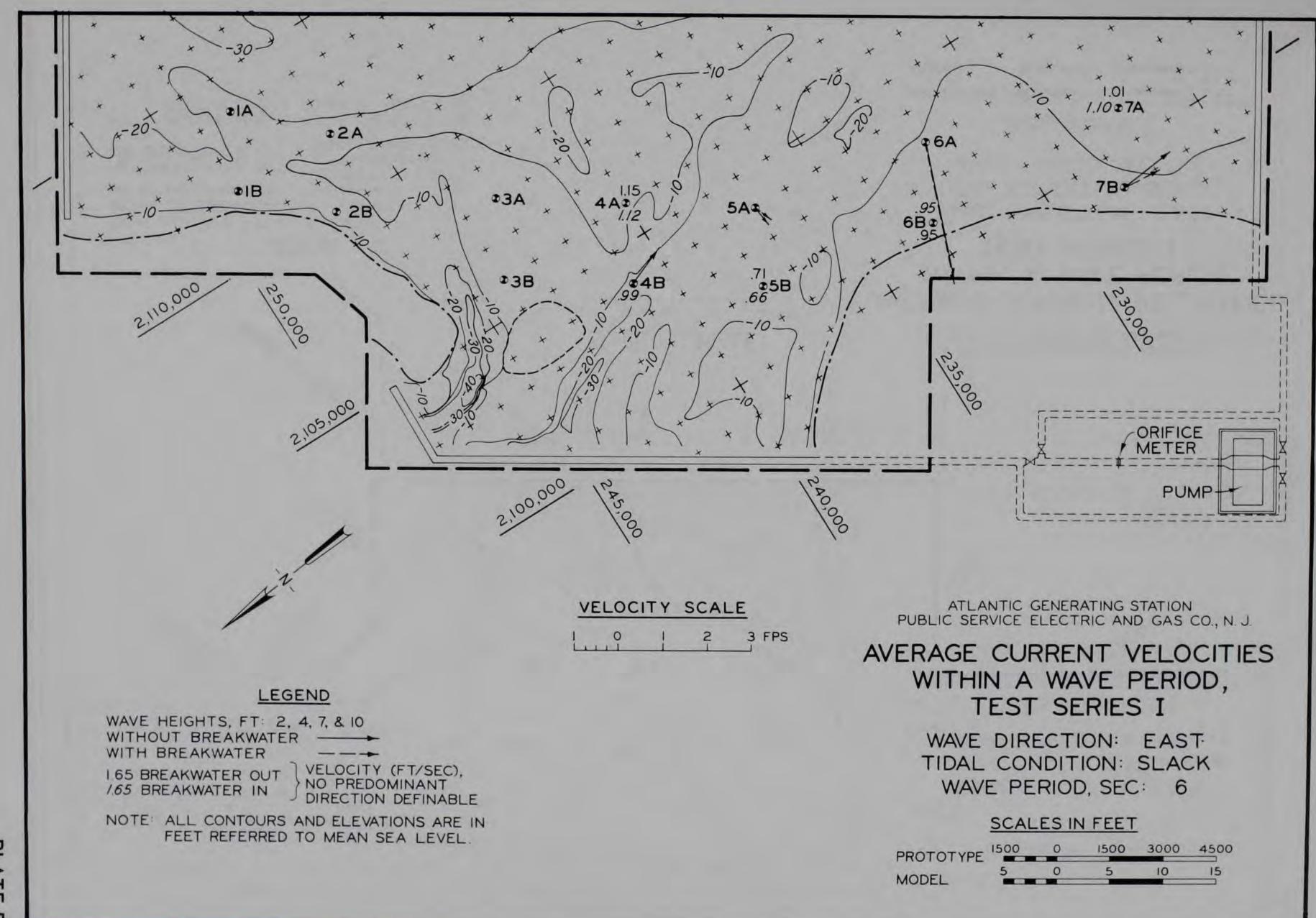
1.65 BREAKWATER OUT | VELOCITY (FT/SEC), NO PREDOMINANT DIRECTION DEFINABLE

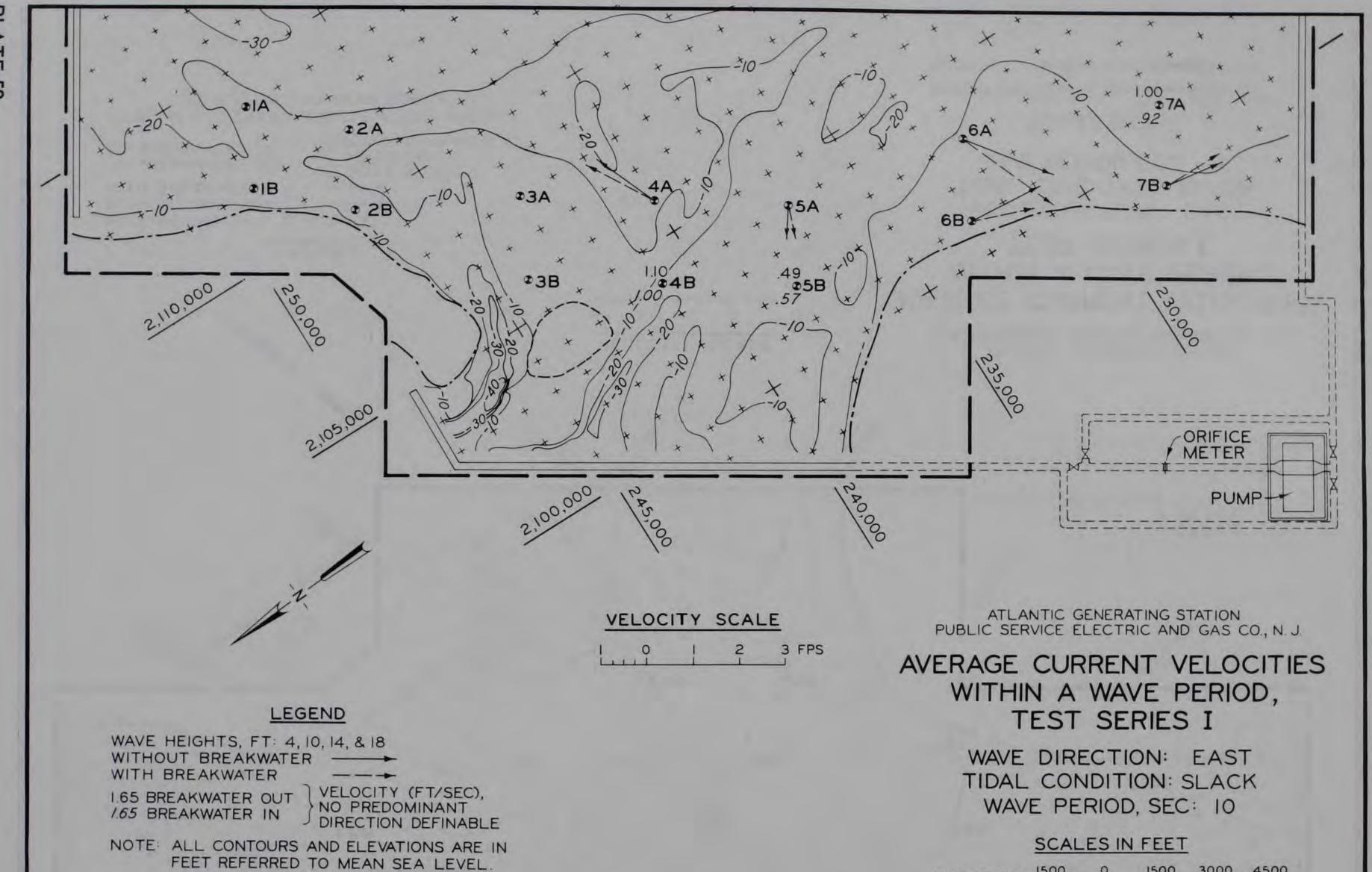
NOTE: ALL CONTOURS AND ELEVATIONS ARE IN FEET REFERRED TO MEAN SEA LEVEL.

AVERAGE CURRENT VELOCITIES WITHIN A WAVE PERIOD, TEST SERIES I

WAVE DIRECTION: EAST TIDAL CONDITION: EBB WAVE PERIOD, SEC: 14

| 1500 | 0 | 1500 | 3000 | 4500 | |
|------|------|------|----------------------|----------|--|
| | ^ | | 10 | | |
| 5 | 0 | 5 | 10 | 15 | |
| | 1500 | 5 0 | 1500 0 1500 5 0 5 | 5 0 5 IO | |

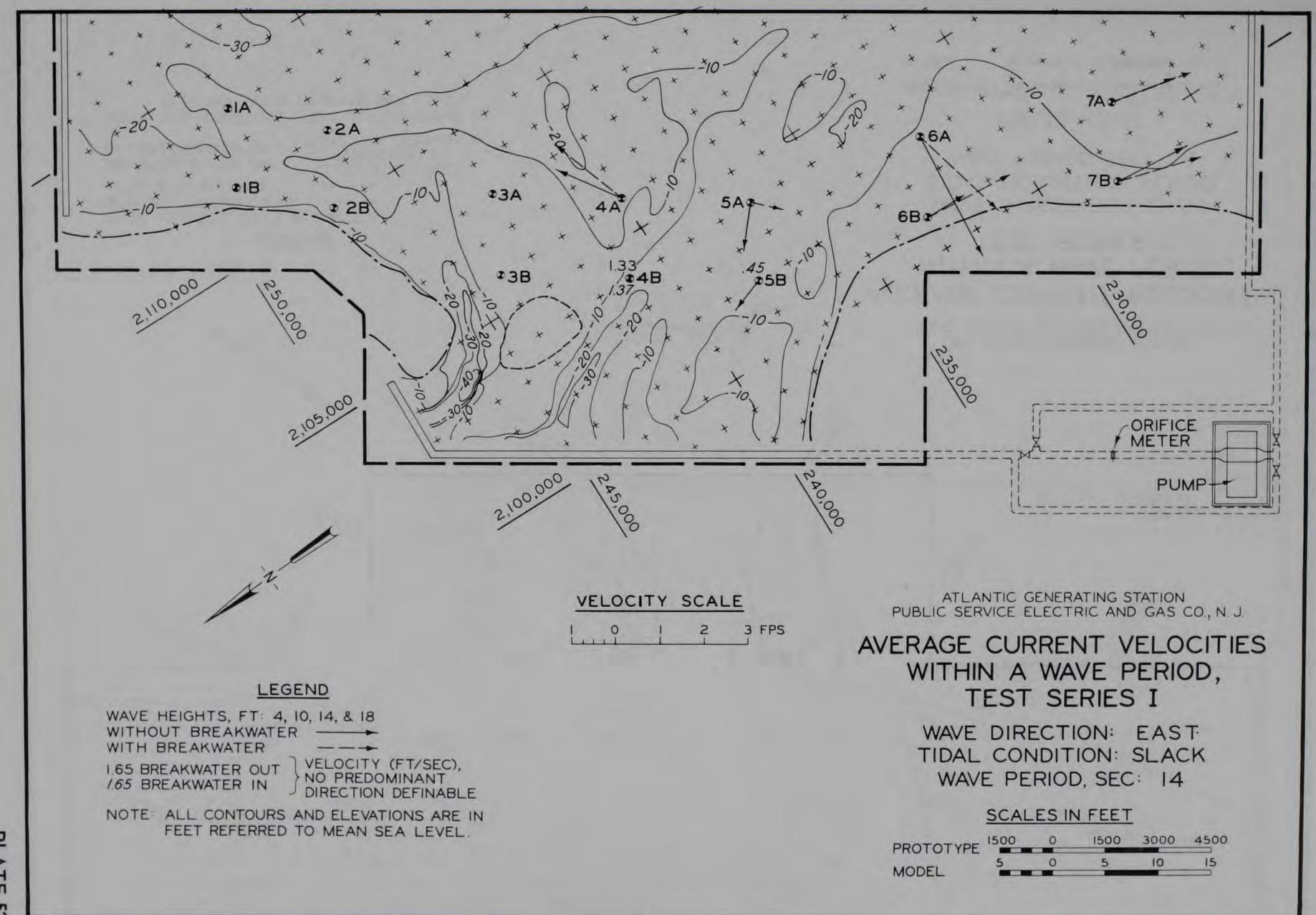


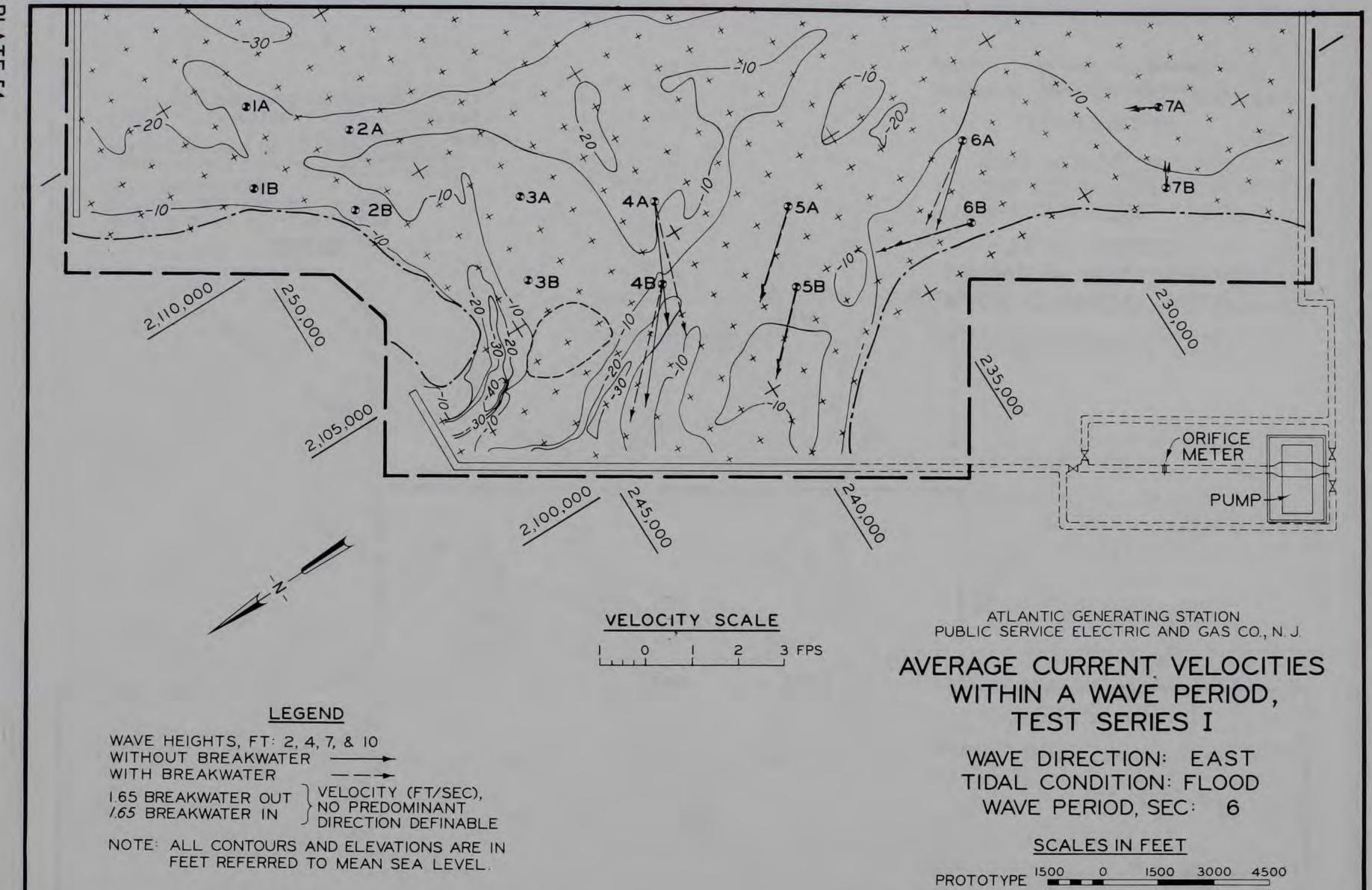


1500 3000 4500

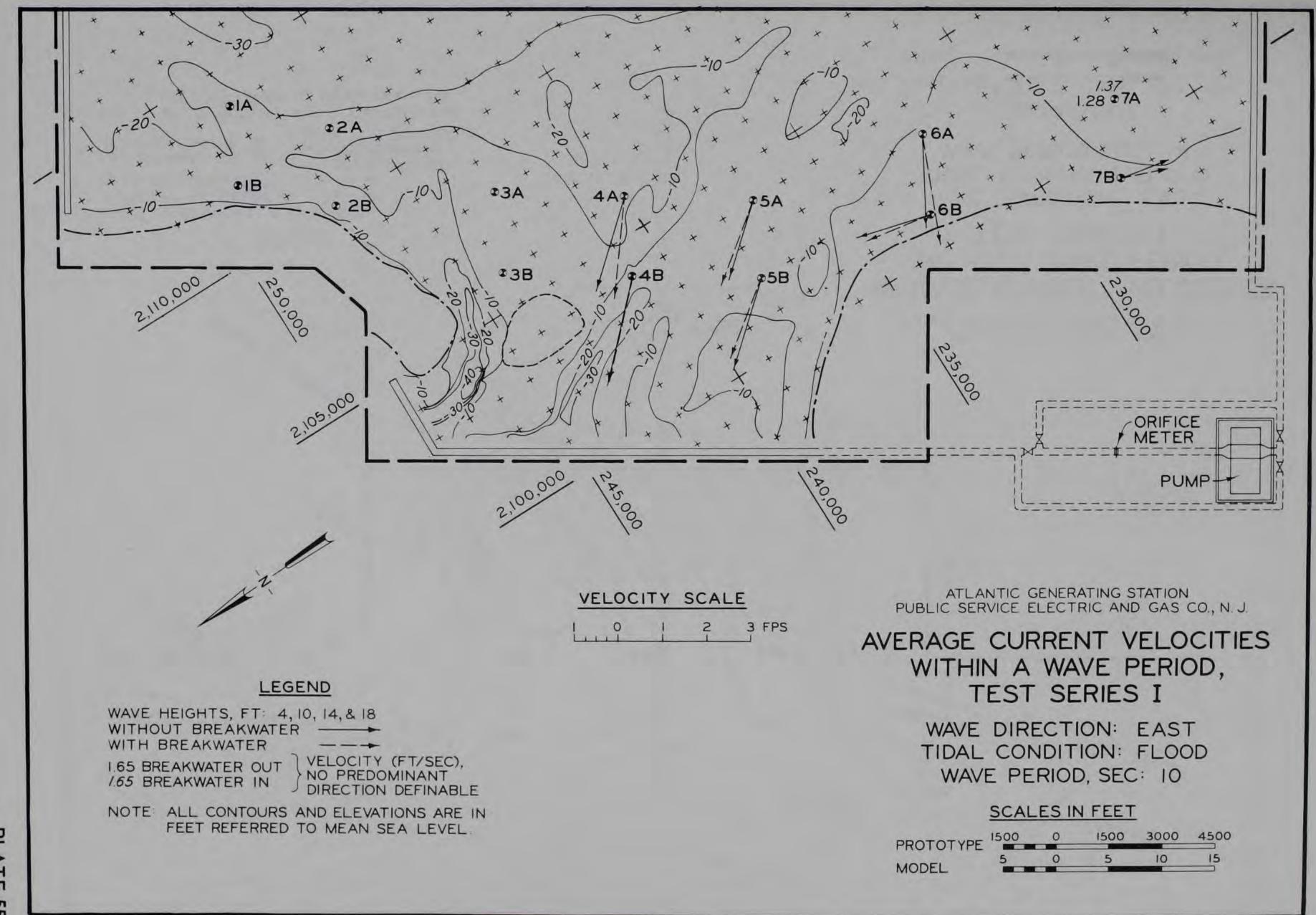
MODEL

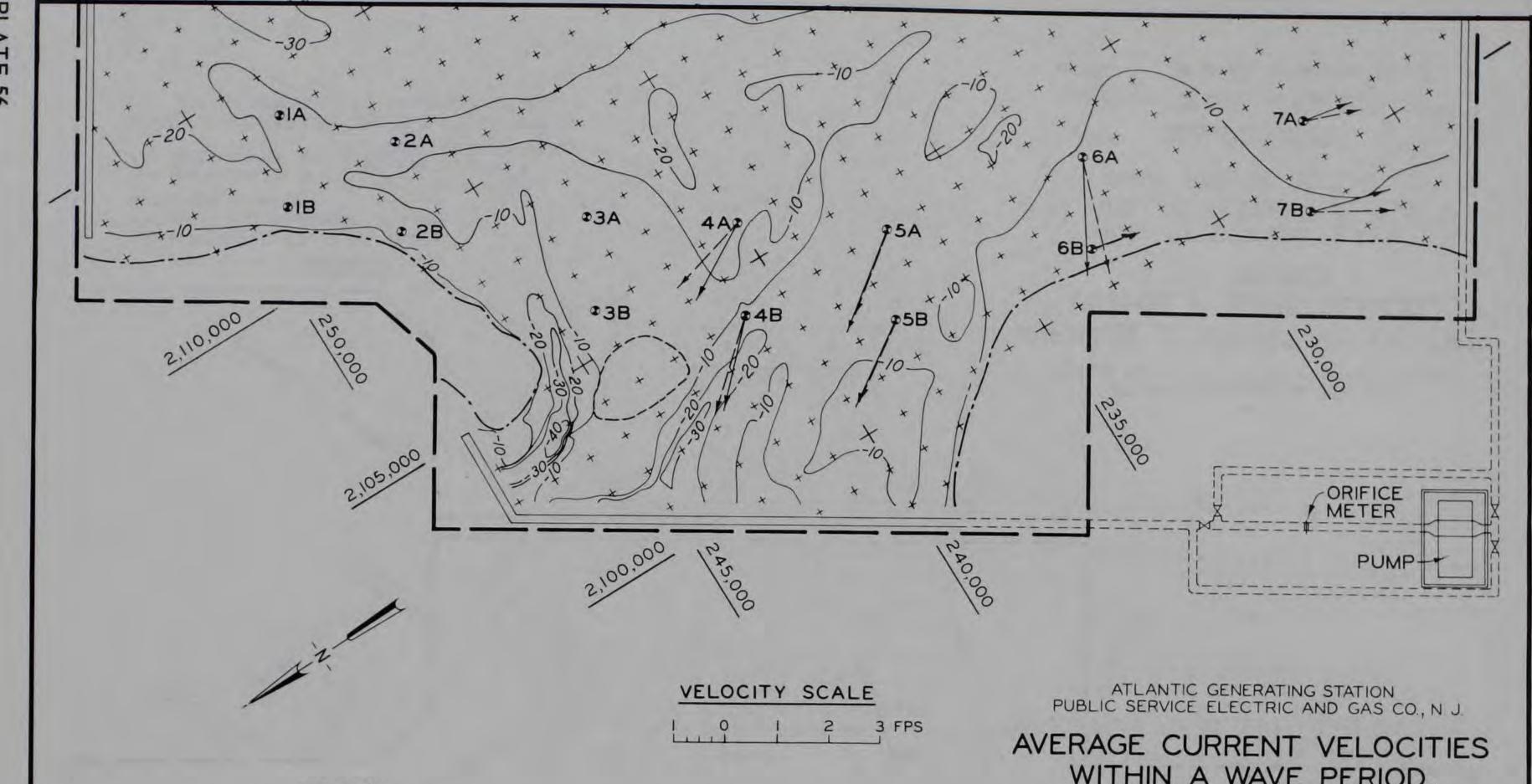
15





MODEL





WAVE HEIGHTS, FT: 4, 10, 14, & 18 WITHOUT BREAKWATER WITH BREAKWATER

VELOCITY (FT/SEC), NO PREDOMINANT 1.65 BREAKWATER OUT 1.65 BREAKWATER IN DIRECTION DEFINABLE

NOTE: ALL CONTOURS AND ELEVATIONS ARE IN FEET REFERRED TO MEAN SEA LEVEL.

WITHIN A WAVE PERIOD, TEST SERIES I

WAVE DIRECTION: EAST TIDAL CONDITION: FLOOD WAVE PERIOD, SEC: 14

| | | | - | | |
|-----------|------|-------|------|------|------|
| PROTOTYPE | 1500 | 0 | 1500 | 3000 | 4500 |
| | 5 | 0 | 5 | 10 | 15 |
| MODEL | - | (III) | | | |

APPENDIX A: BEACH HAVEN-LITTLE EGG INLET MORPHOLOGY STUDY

Historical Inlet Changes

- 1. A crude British map published in 1769 (Figure Al) shows Beach Haven and Little Egg Inlets as a single opening, "Little Egg Harbour," in the barrier island adjacent to the mouth of the "Mullicus River." 11*

 The inlet separated "Old Barnigate Beach" (now Long Beach Island) and "Barnigate Inlet" to the north from "Mikannow Shoal" and "Brigantine Inlet" to the south. Mikannow Shoal was breached in 1800 and the subsequent new channel called "New Inlet." The two resulting islands were renamed, the northern to "Tucker's Island" and the southern to "Little Beach." The single original entrance, Little Egg Harbour, also was renamed, and became "Old Inlet." Plusquellac 11 suggests that the opening of New Inlet compensated for a reduction of tidal flow into "Flat Bay," the area now occupied by both Little Egg Harbour and Great Bay, caused both by a pre-1800 closing of Brigantine Inlet and choking of Old Inlet by southerly spit growth at the tip of Old Barnigate Beach.
- 2. The first detailed map of the area was published in 1840. Geomorphic changes between then and 1932, outlined in Shepard and Wanless, ¹² are reproduced herein (Figure A2). Configurational changes of shorelines and tidal deltas have been so extensive and complex that the inlet history is best understood by an analysis of smaller areas. Consider first the vicinity of Old Inlet near the southern end of Long Beach Island (Old Barnigate Beach). Between 1840 and 1885, the tip of Long Beach migrated approximately 3 miles southward, overlapping the seaward edge of Tucker Island, and in effect eliminating Old Inlet (Figure A2a-c). During the same time, Tucker Island had lost half of its 2-mile length, such that its southern tip lay adjacent to the tip of Long Beach. By 1885, Long Beach and Tucker Island had welded together and extended an additional mile southward. This spit growth continued until sometime after the 1904 survey when, sometime prior to 1932, Long Beach Island was breached near the site of the original Old Inlet (d in

^{*} Raised numbers refer to similarly numbered items in "References" at end of main text.

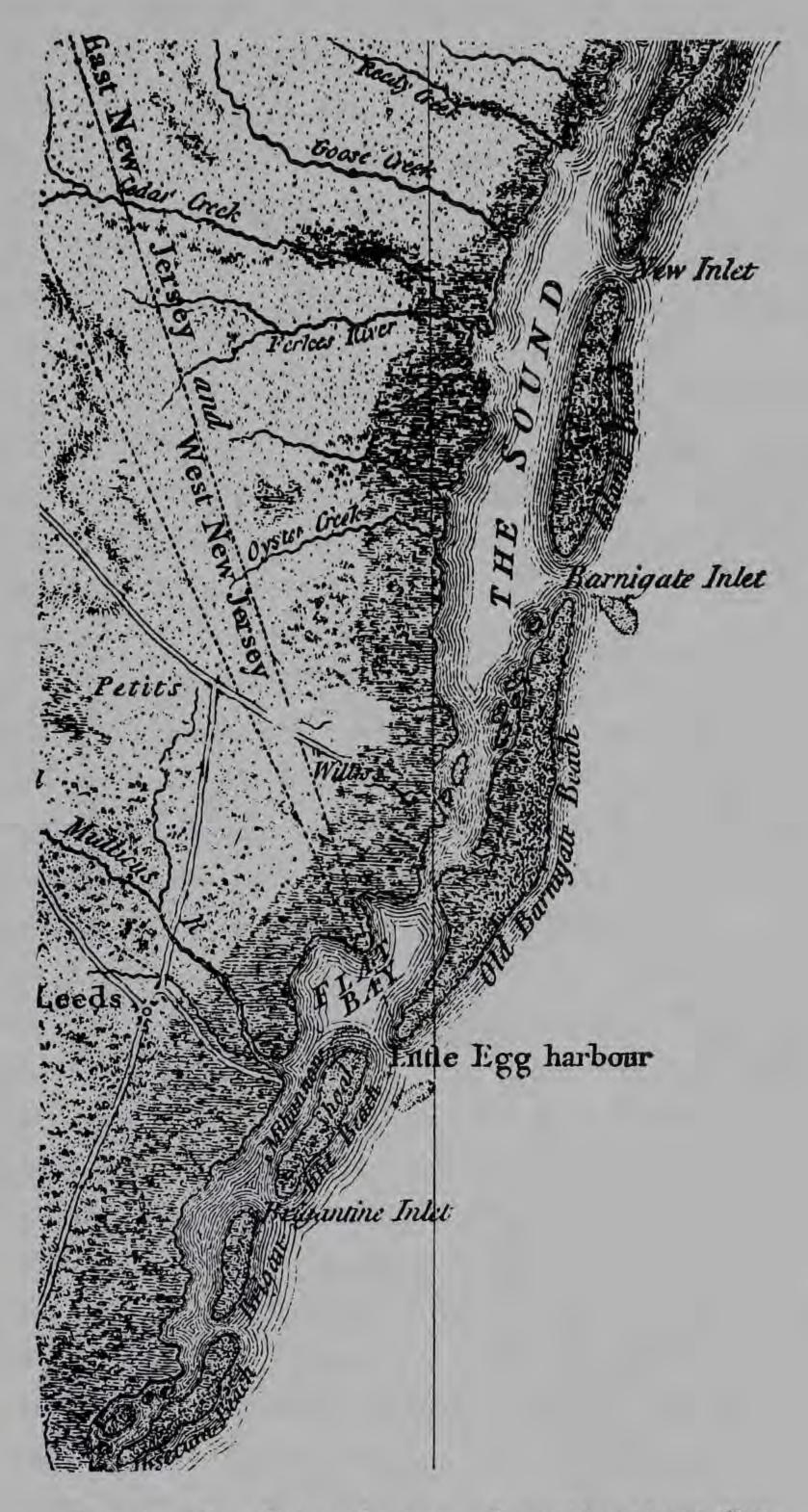


Figure Al. Ratzer's map of southeastern New Jersey in 1769 (from Plusquellac 11)

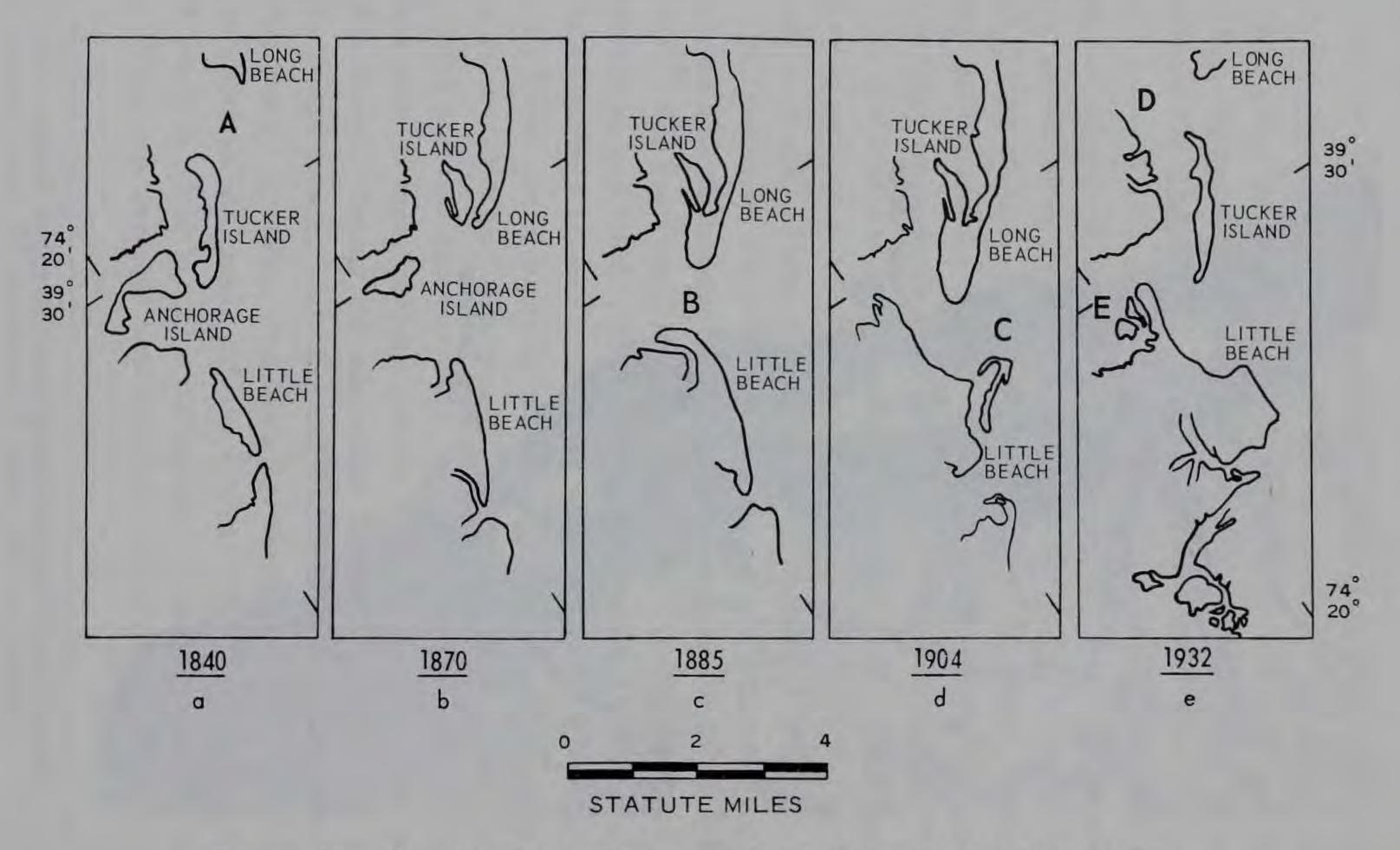


Figure A2. Morphological changes at Beach Haven-Little Egg Inlets, 1840-1932 (after Shepard and Wanless12)

- Figure A2e). Tucker Island was thereby reestablished by the new Beach Haven Inlet, although its seaward shoreline was approximately 0.5 mile west of the welded Long Beach-Tucker Island shoreline. The southerly longshore transport sediment supply was cut off by the opening of Beach Haven Inlet and by 1940 the Tucker Island area had eroded to a little more than 0.5 mile in length (A in Figure A3). Tucker Island had nearly disappeared by 1950¹² as longshore transport being delivered to the area was deposited primarily on the tip of the lengthening Long Beach and on a flood-tidal delta in the southern end of Little Egg Harbor.
- 3. By 1962, although Tucker Island had been eroded completely away, Long Beach had accreted to nearly the position previously occupied by the island (Figure A4). The Ash Wednesday storm of March 1962 created considerable overwash on the southern end of Long Beach and caused a slight shortening of the spit but did not breach the island. The spit had continued to grow and was associated with a small proximal ebbtidal delta (A in Figure A4). Although flood-tidal delta configurations had changed considerably, the overall size of the Beach Haven Inlet flood-tidal delta had remained essentially constant since 1940.
- 4. Photographs taken in 1965 reveal a major redistribution of sediments at Beach Haven Inlet; the large recurved spit evident in the 1962 photographs had completely disappeared (Figure A5). At least part of this material undoubtedly contributed to substantial ebb-tidal delta growth (A in Figure A5), as well as to accretion on the long channel—margin shoal just inside the inlet. The smaller, more seaward spit, visible only as a slight bulge in the 1962 photograph, had by 1965 lengthened and begun to recurve to the position of the 1962 spit. Spit growth continued to 1973 and was accompanied by an apparent decrease in the volume of material on the flood-tidal delta (Figure A6).
- 5. Since the opening of New Inlet about 1800, Little Beach (the area between New Inlet and Brigantine Inlet) has exhibited significant accretion and associated configurational changes. Between 1840 and 1885, the north end of Little Beach occupied approximately the same position. The two islands shown on the 1840 survey were welded together and capped with a northeastward-growing recurved spit (Figure A2). By 1904 Little

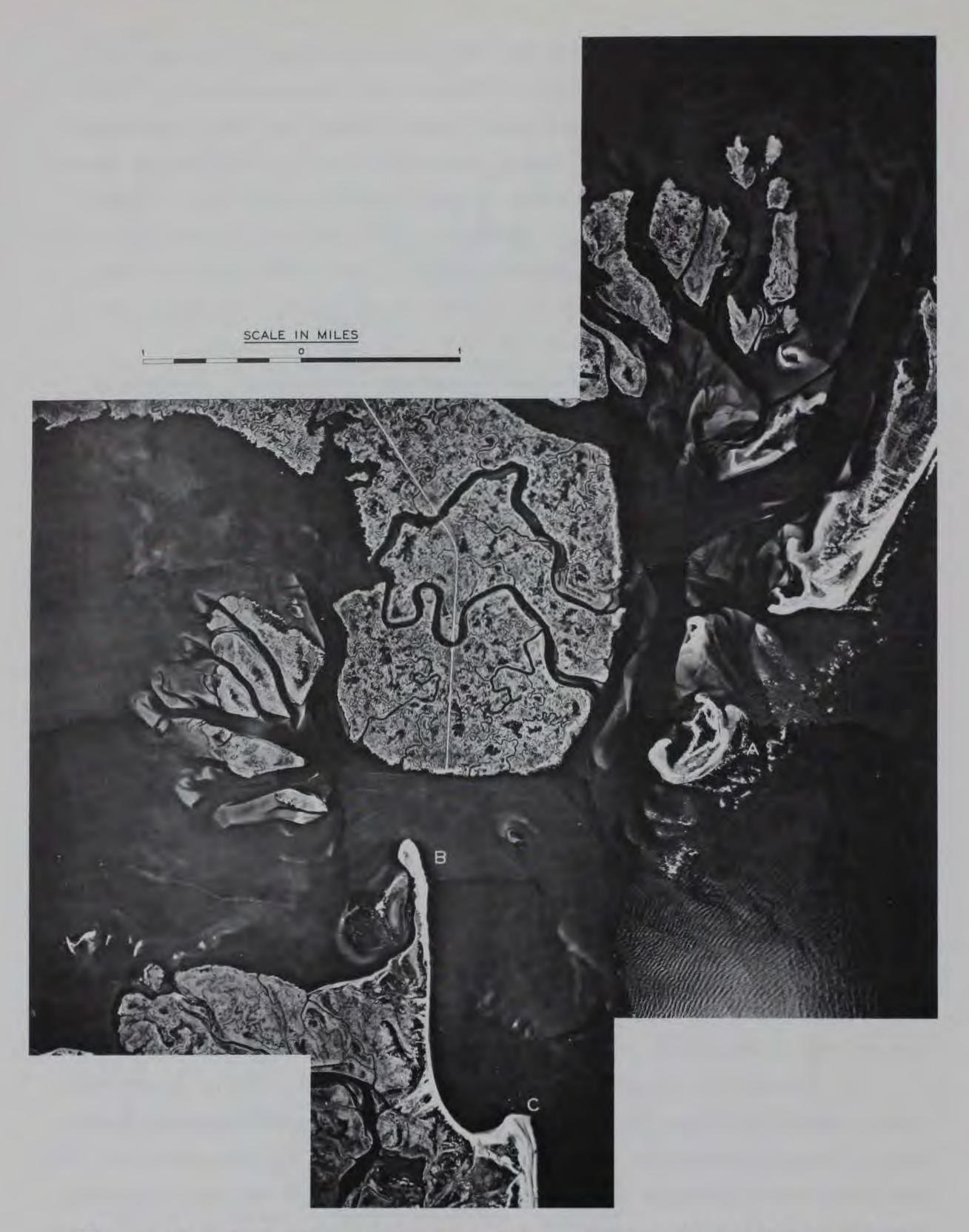


Figure A3. Coastal morphology of Beach Haven-Little Egg Inlets in April 1940 (photography by Aero Service Corp., Philadelphia, Pa.)

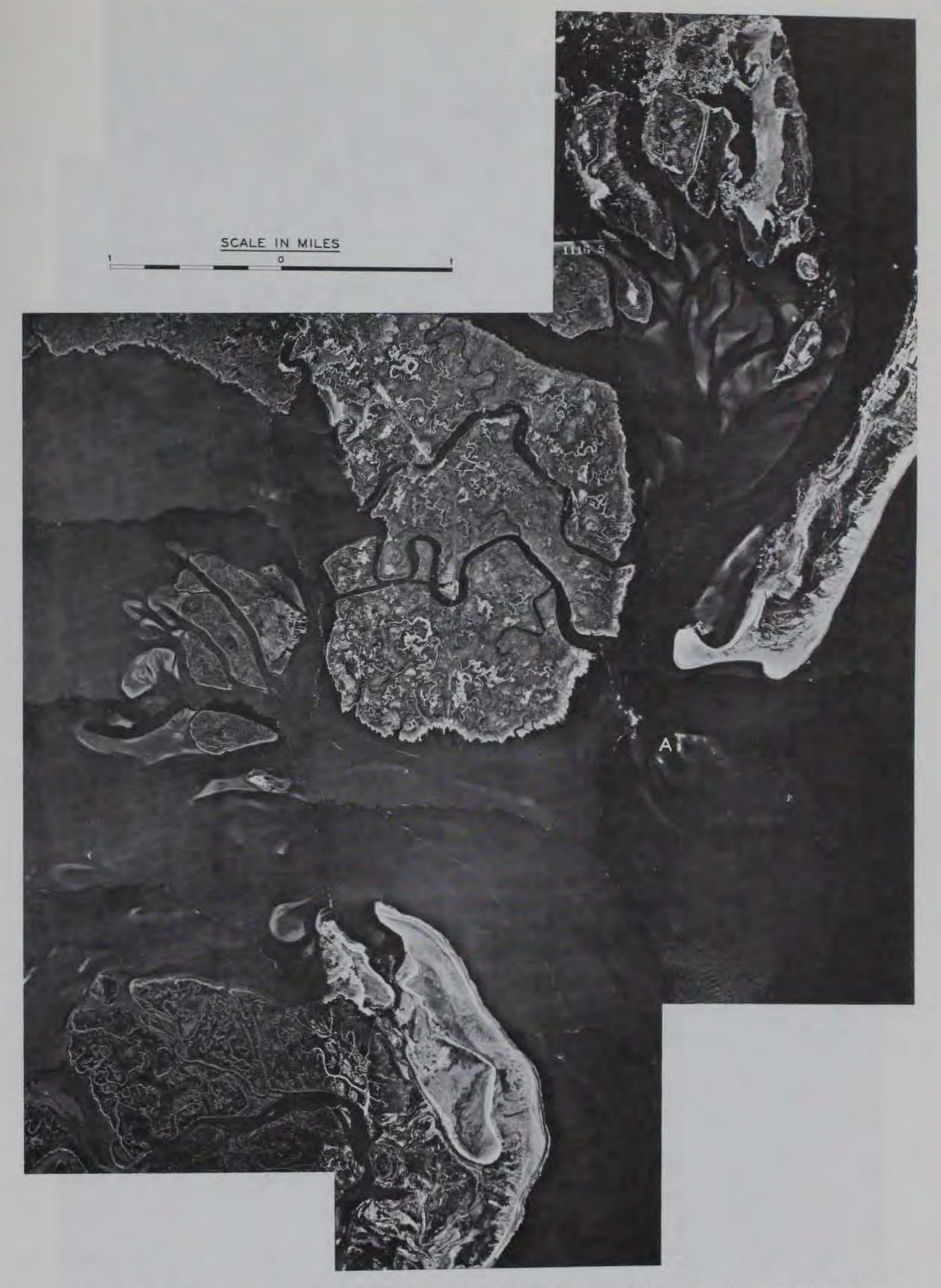


Figure A4. Coastal morphology of Beach Haven-Little Egg Inlets in January 1962; notice ice cover in marsh areas (photography by Aero Service Corp., Philadelphia, Pa.)



Figure A5. Coastal morphology of Beach Haven-Little Egg Inlets in April 1965 (photography by Aero Service Corp., Philadelphia, Pa.)



Figure A6. Coastal morphology of Beach Haven-Little Egg Inlets in March 1973 (photography by NASA)

Beach had continued its northward growth (B in Figure A2c). The shoreline was reoriented considerably, exhibiting a seaward concavity, the trend of which was truncated by a large offshore bar (C in Figure A2d). Northeastward progradation continued; by 1932, the 1904 offshore bar was incorporated into the main beach, and two islands had formed behind the beach's northern end.

- 6. Morphologic changes of Little Beach since 1932 have mostly been consumed in northward spit growth along two fronts. The northern-most spit (B in Figure A3) lengthened and by 1950 had curved around the two marsh islands. The southern spit (C in Figure A3) grew approximately 1 mile to the north by 1950, and by recurving to the west, created a small embayment. The embayment-enclosing spit continued its northward accretion, and in 1962 had reached the same latitude as the original northward spit, which, along with the associated two marsh islands, had nearly disappeared (Figure A4). The embayment was fed by a small inlet with an associated flood-tidal delta (B in Figure A5).
- 7. Little Beach has continued to reflect localized northward longshore transport. By 1973 the embayment behind the Little Beach spit had been extensively modified both by addition of sand to the small embayment flood-tidal delta and by continued northward spit growth (Figure A6). Shoreline concavity had been eliminated and the beach became essentially two-linear elements. In addition, the ebb-tidal delta system appears to have been better developed.

Present Processes

Tides

8. New Jersey tides are semidiurnal with little diurnal inequality. The accepted mean tidal heights are based on a 19-yr period (1924-1942) of observations at the Atlantic City Steel Pier. 13 Referred to ocean mean low water (mlw), the mean tidal heights are: mean high water (mhw), 4.08 ft; msl, 2.06 ft. Normally tide range varies from 3.2 ft (neap) to 5.0 ft (spring), with a mean tide range of 4.1 ft. Tidal durations, referred to lower and upper transits of the moon at Greenwich, are 6.12 hr (low water) and 12.24 hr (high water). 14 Mean

sea level has been increasing in the study area since at least 1912 by 0.014 ft/yr, and since 1953 at a possibly even greater rate. 13
Winds

9. Prevailing winds are from the south and west and of moderate speed (14-28 mph), although northeast winds have the greatest average velocity (19-20 mph). For speeds greater than 28 mph, northeast winds are more than twice as frequent as winds from any other direction. 13 Prevailing winds are generally southerly from April to September, and westerly to northwesterly during the rest of the year. High-velocity northeast winds usually occur in August through October.

Waves

- 10. In addition to the study of Glenn, 8 deepwater wave hindcasting was done by Saville 15 and Neumann and James 16 for Atlantic Coast locations that bracket the study area. The highest waves approach from the east-northeast. Fewer than one percent of the deepwater waves approach from counterclockwise of north-northeast; fewer than one percent approach from clockwise of south-southwest. 17 Because Long Island, New York, provides a sheltering effect from northeast waves along the northern New Jersey coast, the area south of the Barnegat Inlet vicinity is relatively more affected by northeasterly waves than is northern New Jersey. This results in a net southerly longshore transport for southern New Jersey. 14,18
- 11. Wave observations in 1935-1957 at Atlantic City and Brigantine indicate a median wave height of 1.9 ft, and a maximum of 12.8 ft. 19 Median wavelength was 105 ft (maximum 312 ft); median wave speed was 14.7 fps (maximum 25 fps). Only 6 percent of the waves observed approached normal to the beach; 61 percent approached from the north, and 33 percent from the south. Observations made from 1955-1959 are summarized in Reference 21. In general, the frequency of occurrence of high, short-period storm waves increased to a maximum in early autumn. Breakers approached from the southeast (nearly normal to the shoreline) 60.7 percent of the time, and from the northeast 16.8 percent of the time. Charlesworth also reports on wave observations made at Atlantic City by the Coastal Engineering Research Center from 1960 to 1965; the

mean significant wave height was 3.05 ft. Storms

New Jersey. The Corps of Engineers 13 lists 18 severe storms that significantly affected the area between 1933 and 1964. Increased wave heights and higher tides often associated with these storms may cause significant changes in the normal sedimentary processes and the resultant coastal geomorphology. Storm waves may reach heights of 12 ft once a year; during the Ash Wednesday storm of March 1962, 15-ft wave heights were recorded at the Atlantic City Steel Pier.

Currents

- 13. In 1936 and 1937 nontidal longshore currents averaged 0.22 fps southwest (downcoast). During this time westerly winds prevailed (19.2 percent of the time; average speed, 16.4 mph), but the predominant winds were northeasterly (14.7 percent at an average of 17.7 mph). Greaser and Wicker suggested that during an "average" year, longshore currents are most likely to flow downcoast at an average speed of 0.3 fps, as opposed to an average upcoast speed of 0.2 fps. Maximum expected speeds are 4.5 fps upcoast and 0.8 fps downcoast. A downcoast speed of 5 fps occurred during the 66-mph winds of the November 1935 storm, which generated 12.5-ft waves and caused tides 3.6 ft above those predicted.
- been documented by Charlesworth²¹ in his study of local sedimentary processes. Four current stations were occupied, and velocity versus depth was plotted for one tidal cycle. In the throats of both inlets, phase lags between ocean-bay tidal extremes and inlet slack water were essentially 30 deg. For Little Egg Inlet, this value is comparable to that used by Jarrett²² in computing the repletion coefficient, K,²³ for the Beach Haven-Little Egg system. Computed phase lags for Beach Haven Inlet,²² however, were somewhat higher than those measured by Charlesworth.²¹ Jarrett's computations place Beach Haven and Little Egg Inlets into two hydraulically distinct classes. Beach Haven Inlet, with longer phase lag and a repletion coefficient (K = 0.31), is associated with open, shallow bays fed by relatively small inlets. In effect,

inlets of this type are less "competent" in transmitting the tidal wave into their adjoining bays. On the other hand, Little Egg Inlet's shorter phase lag and higher repletion coefficient (K = 0.78) make it intermediate between inlets like Beach Haven and inlets feeding deeper, more channelized bays with bay-tidal phase ranges closer to ocean tides. Longshore transport

15. The net alongshore component of wave energy increases in either direction from a point near Barnegat Inlet, 24 changing from 3.34×10^8 ft-1b/ft/yr southward at Barnegat to 65.29×10^8 ft-1b/ft/yr southward at Cape May. Charlesworth, 21 in a linear interpolation between these two points, suggests that the total net wave energy at Beach Haven-Little Egg Inlet is 24×10^8 ft-1b/ft/yr southward. Estimates of net longshore transport rates in the area vary from $400,000 \text{ yd}^3/\text{yr}$ south 25 to $50,000 \text{ yd}^3/\text{yr}$ south.

Process-Response Relationships and Future Changes

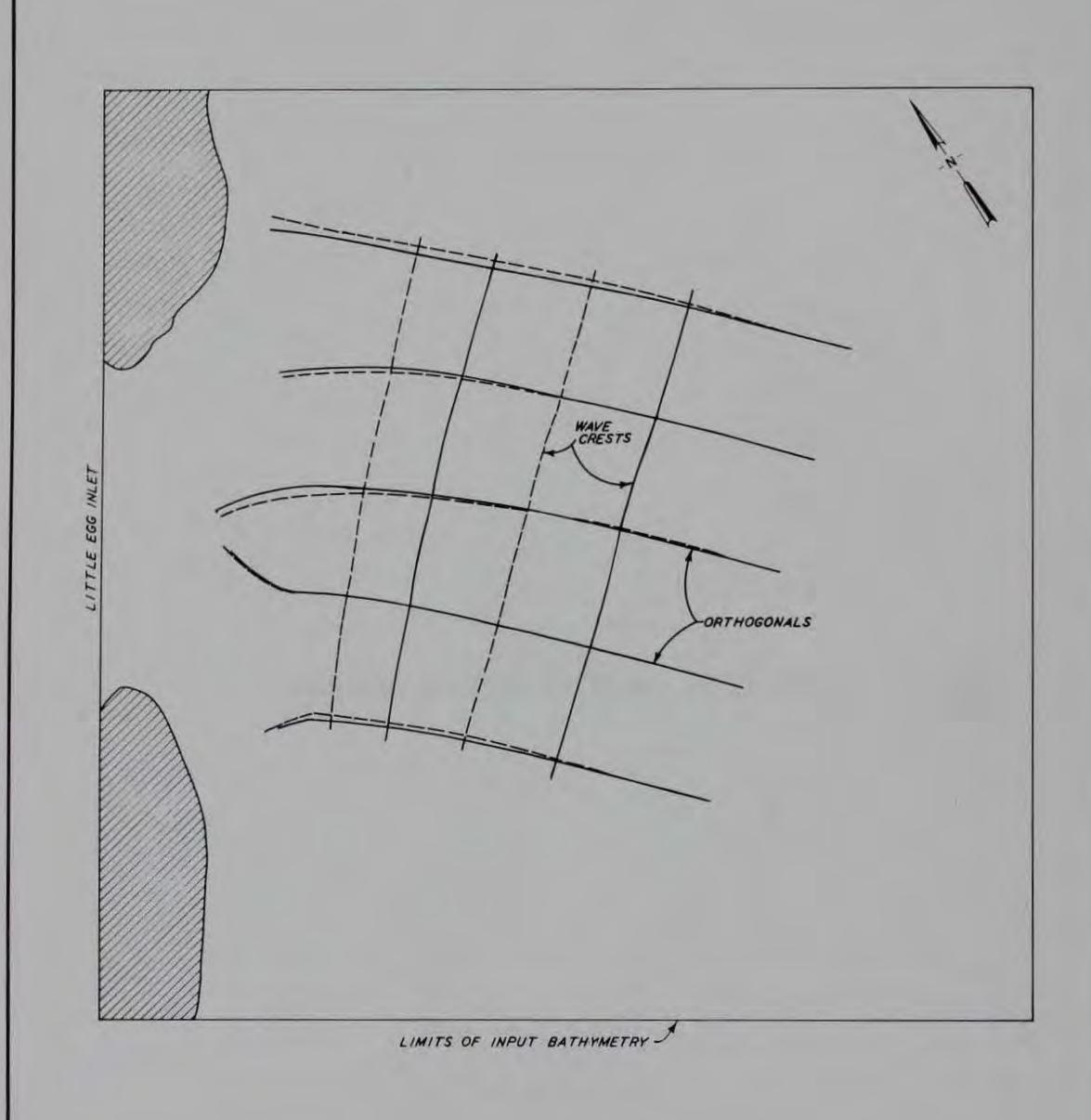
- 16. The Beach Haven-Little Egg Inlet shoal-shoreline configurational history accurately reflects local and regional sedimentologic processes superimposed on the larger scale process of marine transgression. The major geomorphic features of the inlet are the result of an interaction of tidal flow with a regional net southerly longshore transport of sand. These features are modified by local variations caused by wave refraction and current diversion.
- 17. Since at least 1840, Beach Haven Inlet has undergone a cyclic migration process. As the southern end of Long Beach migrated southward by accretion of littoral drift, the inlet entrance channel was forced to migrate also. Storms eventually opened a shorter, more efficient channel, whether by overwash or lagoonal storm surge, through the comparatively new portion of Long Beach as yet unstabilized by dune vegetation. Remains of resultant cutoff portions of Long Beach have formed the islands and shoals occupying the position of Tucker Island. Although considerable quantities of sand are transported to the flood tidal delta behind the inlet, aerial photographs indicate no long-term net influx.

- Spit accretion in the Little Beach area reflects a local northward transport probably caused by wave refraction around an often sizeable ebb-tidal delta. The absolute quantity of this accretion is limited both by the ability of the offshore bar to protect the area from direct wave attack, and by the erosive capability of Little Egg Inlet tidal currents, e.g., Figure A2. The concave-outward shoreline of point C reflects significant erosion over the 1885 conditions (Figure A2c). This erosion was in all probability caused by Beach Haven Inlet ebb-tidal currents impinging directly on Little Beach as a result of the channel being forced southward by accretion at the tip of Long The reopening of a more northern Beach Haven Inlet channel after 1904 and the subsequent elimination of Tucker Island relieved this erosive tendency allowing the progradation by spit development as shown by the 1962 and 1965 photographs (Figures A4 and A5). Similarly, the disappearance of the two marsh islands behind the northern tip of Little Beach spit, although possibly caused by subsidence, 12 is due more probably to erosion by Little Egg Inlet ebb-tidal currents.
- 19. Shepard and Wanless 12 suggest three possibilities for future geomorphic developments of the inlets:
 - a. Tidal currents will probably maintain the inlets in some form for a long time, although further filling of the bays by tidal deltas will decrease the tidal prism and may eventually allow the inlets to be closed.
 - b. A succession of new spits is likely to develop from Little Beach growth to the north, becoming wrapped around earlier spits by hooking to the west.
 - c. New inlets are likely to develop on the southern end of Long Beach, particularly if it grows to the south.
- 20. It is doubtful that, under the present conditions of marine transgression, the tidal prisms associated with Beach Haven and Little Egg Inlets will ever be decreased significantly to allow closing of the inlets. Any net influx of sediment to the bays is extremely small, and could be more than offset by the presently rising sea level. New spit growth on Little Beach does appear to be a likelihood, but may be halted should the channels of the two inlets become too proximal by extensive Long Beach spit growth. Should a future attempt be made to stabilize

Long Beach to a point below 39°40' latitude, Little Beach will more than likely resemble the pre-1932 conditions.

21. It should be emphasized that over the relatively short span of 100 yr and even though its geographic position has been relatively constant, Beach Haven-Little Egg Inlet has displayed a very low configurational stability. To show that the construction of any offshore structure had caused any changes in geomorphology over and above those presently being experienced, one would have to demonstrate that wave conditions were altered in an amount necessary to significantly reduce the net longshore transport rate.

APPENDIX B: WAVE REFRACTION DIAGRAMS



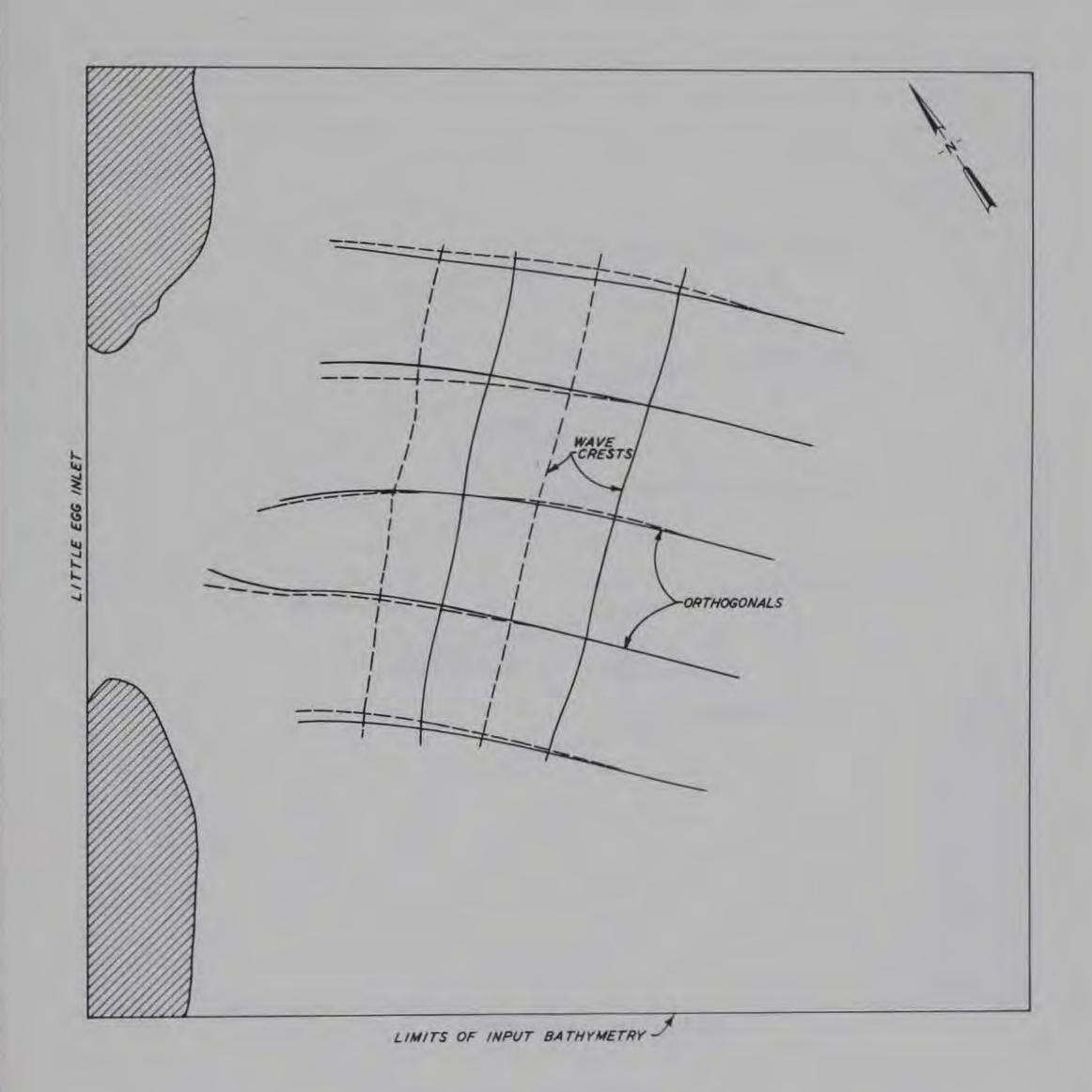
LEGEND

NATURAL BATHYMETRY

TRANSITION INSTALLED

WAVE REFRACTION DIAGRAM
RAYS ORIGINATING FROM SOUTHEAST
WAVE GENERATOR POSITION
6-SEC WAVE PERIOD

2500 0 2500 5000 7500 10,000



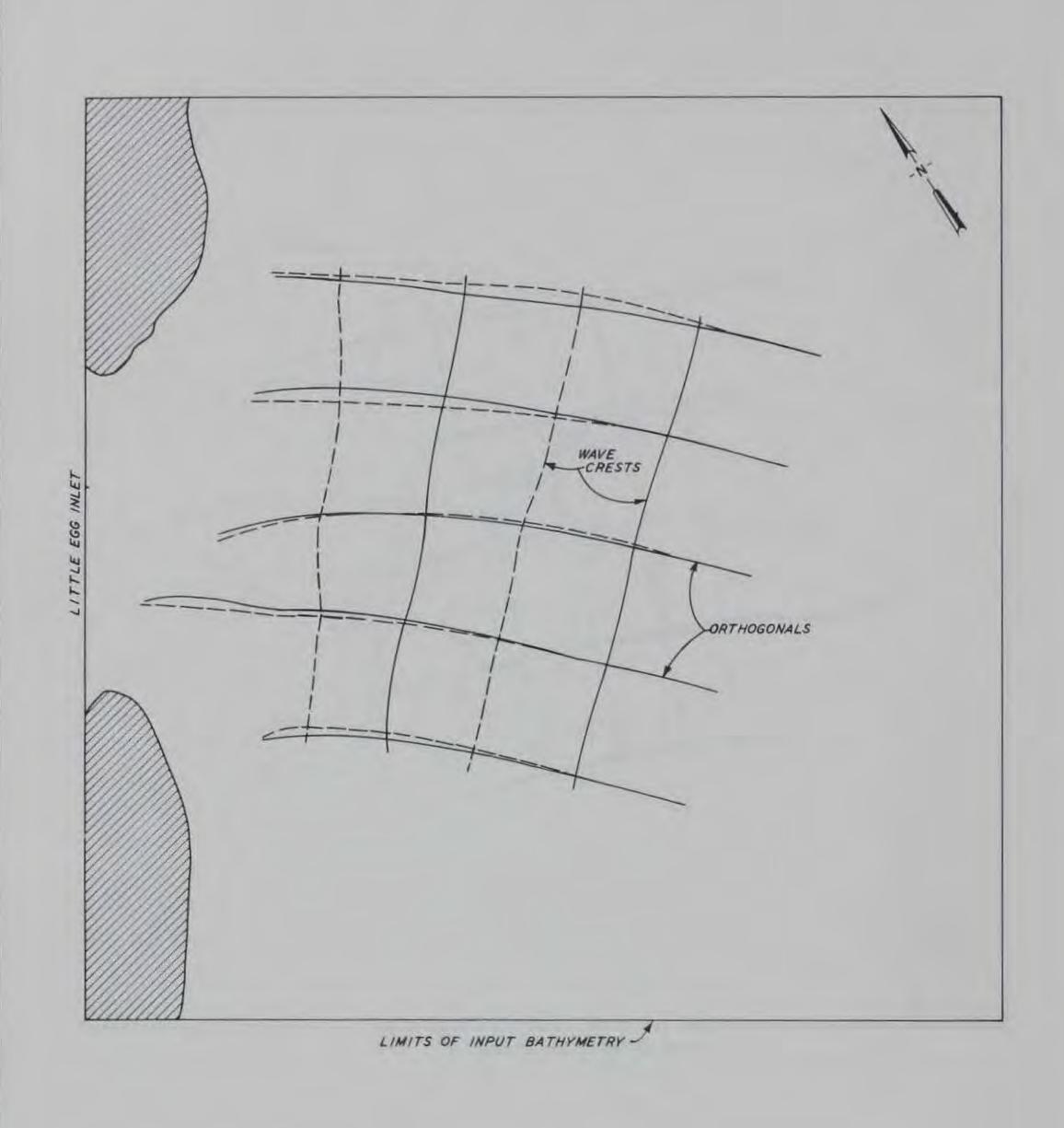
LEGEND

NATURAL BATHYMETRY

TRANSITION INSTALLED

WAVE REFRACTION DIAGRAM
RAYS ORIGINATING FROM SOUTHEAST
WAVE GENERATOR POSITION
10-SEC WAVE PERIOD

2500 0 2500 5000 7500 10,000



LEGEND

NATURAL BATHYMETRY

---- TRANSITION INSTALLED

WAVE REFRACTION DIAGRAM
RAYS ORIGINATING FROM SOUTHEAST
WAVE GENERATOR POSITION
14-SEC WAVE PERIOD

2500 0 2500 5000 7500 10,000

APPENDIX C: NOTATION

```
Orthogonal spacing in shallow water, ft
   b
        Orthogonal spacing in deep water, ft
        Refraction coefficient (dimensionless)
        Depth, ft
   d
        Depth of water a wave breaks in, ft
  do
        Total longshore energy per foot of beach, ft-lb/ft
  EL
        Total longshore energy per foot of beach per day,
  EL
        ft-lb/ft/day
   H
        Wave height at a given location, ft
        Wave height at breaking, ft
  Hb
  Hb
        Average breaking wave height for all waves considered, ft
        Wave height in deep water, ft
  Ho
        Ratio of wave heights (model to prototype)
  Hr
 H/d
        Relative wave height (dimensionless)
 H/L
        Relative wave steepness (dimensionless)
  H
        Incident wave height, ft
        Wave height after wave has propagated a distance AX
  H<sub>2</sub>
   K
        Shoaling coefficient (dimensionless)
   L
        Wavelength at a given location, ft
        Wavelength at breaking, ft
  Lb
        Ratio of wavelengths (model to prototype)
  Lr
Perr
        Ratio of wave periods (model to prototype)
        Volumetric longshore transport rate, yd3/day
  Q_{L}
        Ratio of volumetric flow rates (model to prototype)
   T
        Wave period, sec
  Tr
        Ratio of times (model to prototype)
Vel
        Ratio of velocities (model to prototype)
Volr
        Ratio of volumes (model to prototype)
   X
        A horizontal distance, ft
  Xr
        Ratio of horizontal distances (model to prototype)
        Ratio of vertical distances (model to prototype)
        Angle between breaking-wave crest and shoreline, deg
   a
        Specific weight of water, 1b/ft3
   Y
  ΔX
        An incremental distance, ft
        Kinematic viscosity, ft2/sec
```

V