

Special Report 87

**EXPERIMENTS ON THE DISSIPATION
OF
WARM FOG BY HELICOPTER-INDUCED
AIR EXCHANGE OVER THULE AB
GREENLAND**

by

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PREFACE

These studies were conducted over Thule AB, Greenland, in late summer 1964 by Mr. J. R. Hicks, meteorologist, Environmental Research Branch, U. S. Army Cold Regions Research and Engineering Laboratory (USA CRREL); under the general direction of Dr. R. W. Gerdel, Branch Chief, as part of the Arctic Whiteout Dispersal project.

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During mid and late summer, a shallow advection fog frequently forms over the open water of North Star Bay just north of Thule Air Base, Greenland. Light northerly winds, 4-6 knots, move this fog inland between North and South mountains over Thule AB. Occasionally the fog dissipates as it progresses inland over the runways due to radiational heating of the land. During these periods, one end of the field is operating under Visual Flight Rules for light aircraft and helicopters, but the field is closed for larger aircraft which must make their approach from the sea. It is not uncommon for incoming air traffic to be halted for as long as a week or more.

This situation is particularly troublesome because it occurs at times when air transportation is needed most; i. e., when major research projects are being activated and personnel replacement and area resupply are being completed before the long arctic night sets in. The need for keeping this base open for air traffic is therefore great.

Theoretical considerations

One approach to the problem of clearing such fogs appears to be that of replacing the fog layer with a volume of relatively dry and warm air which would reduce the relative humidity and allow the fog droplets to evaporate and disappear. This approach has been tried by introducing heat which had been generated on the ground by burning fuel in great quantities (the "FIDO" system). Such procedures were used to clear fog from airfields in Great Britain during World War II. Later tests in the United States proved the system to be too unreliable and economically unfeasible.

A second approach to the problem is to replace the fog with warmer air from the inversion layer usually found above. This might be accomplished by helicopters such as the U. S. Army's H-34.

Another approach using the warm air principle was used in a series of tests performed in Japan*. The system used there was to release water droplets from a helicopter above the fog. These falling droplets were thought to cause sufficient air movement downward to dissipate the fog through the process of adiabatic heating by compression.

The experiments conducted in Japan met with considerable success in the case of thin fogs, but little or no effect was noted on thick fogs, or fogs which were in a stable equilibrium condition. Furthermore, the possibility of the clearing being caused by the downwash from the helicopter was never really eliminated. Many scientists felt that it was probably the helicopter downwash which caused the air exchange rather than the falling droplets.

*Magono, Kikuchi, Nakamura and Kimura (1963) An experiment on fog dispersion by use of downward air current caused by fall of water drops, Journal of Applied Meteorology, vol. 2, no. 4, p. 484-493.

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Design of experiments

A study to determine the presence of warm air directly over the fog, and to estimate the chance of success in replacing the fog with this warm air was made during the period 1 July to 23 August 1963.

Arbitrarily, only two parameters were considered to be important in this study: the potential temperature (θ_{sfc}) and the height of the top of the fog.

Potential temperature (θ_{sfc}). This was considered to be the temperature which a parcel of air would achieve if it were moved adiabatically from a point 280 ft above the top of the fog down to the height of the runway. A potential temperature of 1.5C or more above the surface temperature was determined to be sufficient to evaporate the liquid water contained in the fog ($\approx 0.10 \text{ g/m}^3$) and to keep it in the vapor state. Calculations show that a drop in air temperature of $\approx 0.2\text{C}$ could be expected due to the vaporization of the liquid water, and that an increase in temperature of 0.3C would be needed to maintain the total water content of the fog in the vapor state.

Height of the top of the fog. It was believed that if the top of the fog was 1000 ft or less, the chance of successful dissipation was good. These temperature and height parameters were selected intuitively since it was not known to what depth a helicopter could cause downward displacement of air under different conditions of atmospheric stability.

A third parameter, stability with respect to the dry adiabatic lapse rate within the fog layer, was studied but did not enter into the prediction; however, a layer having unstable equilibrium would be set in motion more easily and, hence, air would be exchanged to greater depths than could be accomplished in a layer having stable equilibrium.

Data analysis

Sixty-four radiosonde ascents made during actual periods of fog over the Thule area were analyzed and, using the criteria described in the preceding section, estimates were made on the probability of clearing the fog by the air-exchange method. The results of these studies are shown below.

| <u>Prediction of success</u> | <u>Stability characteristics</u> |
|------------------------------|--|
| Yes = 41 | stable = 13 unstable = 16 neutral = 12 |
| No = 8 | stable = 7 unstable = 1 neutral = 0 |
| Marginal = 15 | stable = 6 unstable = 6 neutral = 3 |

The tabulated data for these soundings are contained in Table I (p. 6) and a sample plot of one sounding is shown in Figure 1.

Flight tests

Several flights were made over the Thule area in July 1964 to test the effectiveness of the H-34 helicopter as an air exchanger. The results of these flights follow.

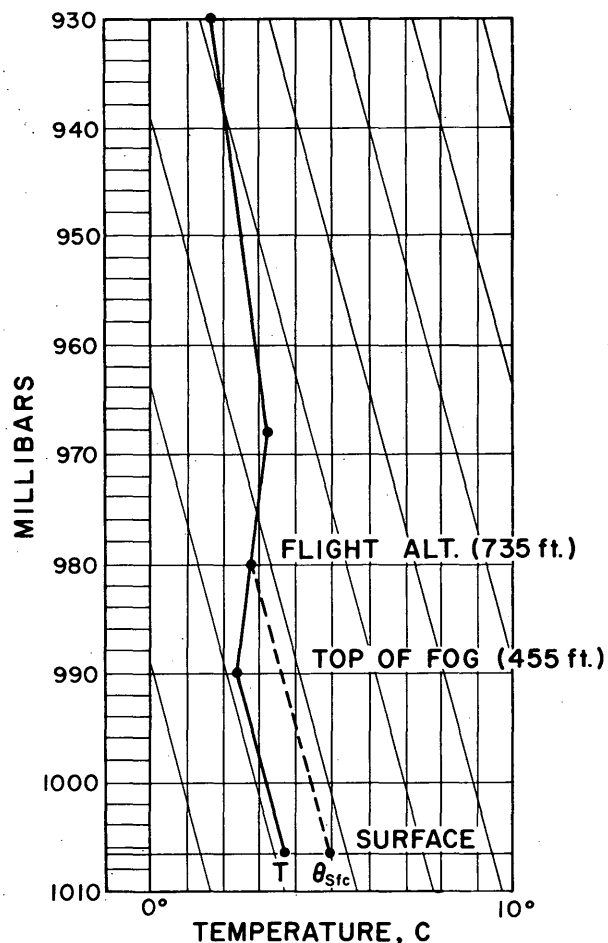


Figure 1. Radiosonde plot showing method for deriving potential temperature. Thule AB, 6 July 1963, 0700 LST. Diagonal lines are dry adiabats.

Flight 1.

| | |
|-----------------------|-------------------------|
| Date: | 19 July 1964 |
| Time: | 1430-1434 hours |
| *Temp (sfc): | 0C |
| Temp (top of fog): | 0C |
| *Wind (sfc): | 270/04 |
| *R. H.: | 79% |
| Visibility (sfc): | estimated 300 ft in fog |
| Height of top of fog: | approximately 250 ft |

A 4-min flight at an altitude of 270 ft was made at an airspeed of about 4 knots. The direction of the flight was almost upwind. A clear path about 75 yards wide and 500 yards long was observed immediately after the run. This path was in an

*These data were taken at the Thule AB weather observation station and do not necessarily represent the conditions where the flight was made.

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area in which the fog was quite thin, i. e., not dense; some nearby areas contained holes through which the ground could be seen.

Flight 2.

| | |
|-----------------------|-------------------------|
| Date: | 19 July 1964 |
| Time: | 1436-1440 hours |
| *Temp (sfc): | 0C |
| Temp (top of fog): | 0.5C |
| *Wind (sfc): | 270/04 |
| *R. H.: | 79% |
| Visibility (sfc): | estimated 200 ft in fog |
| Height of top of fog: | estimated 280 ft |

A 4-min flight, similar to Flight 1 of this series, was made over a denser area of fog on North Star Bay near Thule Air Base. As before, clearing occurred in the wake of the helicopter. The downdraft from the helicopter reached the surface of the water and ripples were observed on an otherwise smooth water surface.

Flight 3.

| | |
|-----------------------|-------------------------|
| Date: | 19 July 1964 |
| Time: | 1442-1446 hours |
| *Temp (sfc): | 0C |
| Temp (top of fog): | 2.0C |
| *Wind (sfc): | 270/04 |
| *R. H. (sfc): | 79% |
| Visibility (sfc): | estimated 300 ft in fog |
| Height of top of fog: | 280 ft |

This flight was made at the level of the top of the fog about midway between Dundas Mountain and Thule AB. The area was covered by a thin layer of fog in which some openings already existed. Clearing was noted in the wake of the H-34. No doubt this hole was caused by the helicopter but it was not much different in appearance from some of the other nearby openings in the fog layer.

Flight 4.

| | |
|-----------------------|-------------------------|
| Date: | 19 July 1964 |
| Time: | 1450-1455 hours |
| *Temp (sfc) | 0C |
| Temp (top of fog): | 2.0C |
| *Wind (sfc): | 260/03 |
| *R. H. (sfc): | 79% |
| Visibility (sfc): | estimated 200 ft in fog |
| Height of top of fog: | 300 ft |

This flight was made at an altitude of about 325 ft, i. e., approximately 25 ft above the fog. An airspeed of 4-6 knots was maintained and a flight path over the entire length of the pier at Thule AB was used. A clear path about 75 yards wide was established for the entire length of the pier (Fig. 2). This clear area remained for about 10 minutes, after which it began to fill in and become ragged at the sides.

*These data were taken at the Thule AB weather observation station and do not necessarily represent the conditions where the flight was made.

Twenty minutes after clearing had been accomplished, the area had drifted away from the pier and had filled in almost completely.

Conclusions and Recommendations

These tests have demonstrated that certain types of shallow fogs can be dispersed by the downwash created by helicopters flying at near-hovering airspeeds at altitudes a few feet above the top of the fog. One helicopter can clear an area about 75 yards wide by a mile long every 10-15 minutes.

This system requires unsafe flying techniques, i. e., near-hovering airspeeds during which time the helicopter is operating at almost full power, low altitudes, and positions where an engine failure would probably result in a crash since the aircraft would have to descend through the fog to an unknown landing area. Therefore, this technique is recommended for emergency use only.



Figure 2. Results of one pass by helicopter over a 300 ft thick "warm" fog. Cleared strip is about 75 yards wide by 500 yards long.

Table I. Radiosonde data taken during periods of fog at Thule AB for the summer of 1963.

| Date 1963 | Time LST | Surface | | Top of fog | | Ht. 280 ft above top of fog (ft) | Stability S.U.N. | Potential temp θ_{sfc} (°C) | Poss? | Remarks |
|--------------|-------------|--------------------------------|--------------|----------------|----------------|--|---------------------|--|-------|--|
| | | Press. (mb) | Temp (°C) | Press. (mb) | Height (ft) | | | | | |
| 1 July | 1300 | 1014 | +1.8 | 1002 | 336 | 616 | X | + 1.0 | No | |
| 2 | 0100 | 1007 | +1.5 | 962 | 1232 | 1512 | X | + 5.5 | Yes | |
| 2 | 1902 | 1007 | -1.0 | 970 | 1008 | 1288 | X | + 6.0 | ? | |
| 3 | 0100 | 1005 | -0.6 | 970 | 960 | 1240 | X | + 4.5 | Yes | |
| 5 | 0700 | 1008 | +0.9 | 996 | 616 | 896 | X | + 3.0 | Yes | |
| 6 | 0700 | 1007 | +3.5 | 990 | 455 | 735 | X | + 5.0 | Yes | |
| 6 | 1303 | 1006 | +4.4 | 988 | 500 | 780 | X | + 6.0 | Yes | |
| 6 | 1904 | 1st significant level = 600 mb | | | | | X | | No | $\theta_{sfc} > T_{sfc}$ for all levels. |
| 14 | 1900 | 1007 | +4.2 | 972 | 970 | 1250 | X | + 7.5 | Yes | |
| 15 | 0102 | 1006 | +2.3 | 975 | 860 | 1140 | X | + 8.6 | Yes | Inversion from surface. |
| 15 | 0711 | 1006 | +1.0 | 986 | 560 | 840 | X | + 2.8 | Yes | |
| 15 | 1310 | 1003 | +1.8 | 978 | 695 | 975 | X | + 3.1 | ? | |
| 15 | 1910 | 1002 | +0.6 | 973 | 810 | 1090 | X | + 3.1 | Yes | |
| 16 | 0100 | 1001 | +0.9 | 978 | 635 | 915 | X | + 3.4 | Yes | |
| 16 | 0701 | 1008 | +0.4 | 983 | 700 | 980 | X | + 2.8 | Yes | |
| 16 | 1301 | 1006 | +1.8 | 995 | 300 | 580 | X | + 3.7 | Yes | |
| 16 | 1915 | 1007 | +0.2 | 998 | 249 | 529 | X | + 2.0 | Yes | |
| 17 | 0100 | 1010 | -1.4 | 988 | 616 | 896 | X | + 3.0 | Yes | |
| 17 | 0737 | 1012 | +1.0 | 1002 | 280 | 560 | X | + 3.5 | Yes | |
| 17 | 1304 | 1014 | +3.0 | 997 | 475 | 755 | X | + 6.8 | Yes | |
| 17 | 1900 | 1014 | 0.0 | 958 | 1568 | 1848 | X | +11.0 | ? | Deep inversion |
| 18 | 0103 | 1014 | 0.8 | 975 | 1095 | 1375 | X | + 7.0 | ? | |
| 18 | 0703 | 1013 | +1.2 | 1002 | 310 | 590 | X | + 3.6 | Yes | |
| 18 | 1333 | 1013 | +1.2 | 998 | 410 | 690 | X | + 1.4 | ? | Inv at 980 mb |
| 18 | 1900 | 1013 | +1.0 | 992 | 580 | 860 | X | + 2.8 | Yes | |
| 19 | 0100 | 1011 | +0.8 | 992 | 530 | 810 | X | + 4.0 | Yes | |
| 19 | 0701 | 1011 | 0.0 | 1002 | 255 | 535 | X | + 1.5 | ? | Steep inv at 1002 mb |
| 19 | 1302 | 1011 | +2.2 | 1001 | 280 | 560 | X | + 4.0 | Yes | Steep inv at 1000 mb |
| 19 | 1901 | 1013 | -1.0 | 987 | 728 | 1008 | X | + 1.8 | Yes | |
| 20 | 0101 | 1013 | -0.2 | 986 | 760 | 1040 | X | + 4.0 | Yes | |
| 20 | 0704 | 1015 | +1.0 | 1000 | 420 | 700 | X | + 3.5 | Yes | |
| 20 | 1350 | 1016 | +0.5 | 984 | 896 | 1176 | X | + 3.6 | Yes | |

Table I(Cont'd). Radiosonde data taken during periods of fog at Thule AB for summer of 1963.

| Date 1963 | Time LST | <u>Surface</u> | | <u>Top of fog</u> | | Ht. 280 ft above top of fog (ft) | Stability S.U.N. | Potential temp θ_{sfc} (°C) | Poss? | Remarks |
|--------------|-------------|----------------|--------------|-------------------|----------------|--|---------------------|--|-------|-------------------------|
| | | Press. (mb) | Temp (°C) | Press. (mb) | Height (ft) | | | | | |
| 20 July | 1900 | 1018 | -1.5 | 1000 | 504 | 784 | X | + 1.5 | Yes | |
| 21 | 0157 | 1018 | 0.0 | 996 | 616 | 896 | X | + 3.0 | Yes | |
| 21 | 0713 | 1018 | +0.5 | 1008 | 280 | 560 | X | + 1.3 | ? | Sharp inv above 1008 mb |
| 21 | 1301 | 1019 | +1.0 | 1010 | 250 | 530 | X | + 3.5 | Yes | |
| 21 | 1901 | 1019 | +0.6 | 968 | 1440 | 1720 | X | + 1.6 | ? | Inv from sfc |
| 22 | 0100 | 1019 | +0.3 | 1008 | 300 | 580 | X | + 3.0 | Yes | |
| 22 | 0702 | 1018 | +0.8 | 1007 | 310 | 590 | X | + 4.0 | Yes | |
| 22 | 1301 | 1020 | +1.7 | 1010 | 280 | 560 | X | + 3.6 | Yes | |
| 22 | 2003 | 1021 | +0.4 | 1002 | 550 | 830 | X | + 3.0 | Yes | |
| 23 | 0100 | 1021 | +0.4 | 1005 | 448 | 728 | X | + 2.0 | Yes | |
| 23 | 0700 | 1021 | +1.0 | 1007 | 392 | 672 | X | + 2.8 | Yes | |
| 23 | 1304 | 1021 | +1.6 | 1011 | 570 | 850 | X | + 3.4 | Yes | |
| 23 | 1901 | 1019 | -0.9 | 990 | 810 | 1090 | X | + 3.6 | Yes | |
| 24 | 0107 | 1016 | +1.1 | 996 | 560 | 840 | X | + 5.8 | Yes | |
| 24 | 0729 | 1013 | 0.0 | 990 | 640 | 920 | X | +12.5 | Yes | Inv from sfc |
| 29 | 1301 | 1001 | +4.7 | 991 | 280 | 560 | X | + 6.8 | Yes | |
| 6 Aug | 1300 | 1006 | +4.4 | 983 | 640 | 920 | X | + 5.8 | ? | |
| 6 | 1900 | 1007 | +3.4 | 827 | 5000 | 5280 | X | | No | Layer too deep |
| 7 | 0701 | 1010 | +5.4 | 932 | 2184 | 2464 | X | + 6.7 | No | Too deep |
| 8 | 0103 | 1007 | +3.5 | 948 | 1904 | 2184 | X | + 7.0 | No | Too deep |
| 9 | 1306 | 1009 | +3.8 | 963 | 1260 | 1540 | X | + 6.5 | ? | Deep layer |
| 10 | 0100 | 1018 | +3.1 | 943 | 2100 | 2380 | X | + 7.5 | No | Deep layer |
| 13 | 0700 | 1012 | +4.5 | 850 | >4500 | | X | | No | Too deep |
| 14 | 0101 | 1015 | +2.8 | 902 | 3164 | | X | | No | Too deep |
| 14 | 0750 | 1012 | +4.5 | 980 | 896 | 1176 | X | + 5.5 | ? | Deep layer |
| 17 | 0101 | 998 | +2.9 | 967 | 810 | 1090 | X | + 4.8 | Yes | |
| 17 | 1300 | 999 | +3.1 | 958 | 1140 | 1420 | X | + 4.5 | ? | Deep layer |
| 18 | 0101 | 1002 | +1.0 | 976 | 728 | 1008 | X | + 2.5 | Yes | |
| 19 | 0700 | 1005 | +4.2 | 974 | 870 | 1150 | X | + 9.0 | Yes | |
| 20 | 0101 | 1006 | +2.5 | 934 | 2045 | 2325 | X | +11.0 | ? | Deep layer |
| 23 | 0102 | 1016 | +3.4 | 970 | 1288 | 1568 | X | + 8.2 | ? | Inv from sfc |
| 23 | 1314 | 1011 | +3.8 | 938 | 2020 | 2300 | X | + 8.5 | ? | Deep layer |