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# **Special Report 96**

# EVALUATION OF THE AASHO PROFILOMETER FOR MEASURING AIRFIELD PAVEMENT PROFILES

b y

E. J. Yoder and R. D. Walker

**APRIL 1966** 

Conducted for CORPS OF ENGINEERS, U. S. ARMY

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U.S. ARMY MATERIEL COMMAND COLD REGIONS RESEARCH & ENGINEERING LABORATORY HANOVER, NEW HAMPSHIRE

**Purdue University** 



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## PREFACE

Authority for the investigation reported herein is contained in FY 1959 Instructions and Outline, Military Construction Investigations, Engineering Criteria and Investigations and Studies, Studies of Construction in Areas of seasonal Frost: Field Investigations.

The study was conducted for the Office, Chief of Engineers, Directorate of Military Construction by the Purdue Research Foundation, School of Civil Engineering, Purdue University, Lafayette, Indiana, under a contract awarded by the former Arctic Construction and Frost Effects Laboratory (ACFEL). \* Project responsibility was transferred to the U. S. Army Cold Regions Research and Engineering Laboratory (USA CRREL) after completion of the study. Professor Eldon J. Yoder was the principal investigator for the Purdue Research Foundation. Cooperation of personnel of the AASHO Road Test, Ottawa, Illinois, in conducting the field tests, and assistance in interpreting the results is gratefully acknowledged.

This report was prepared by the Construction Engineering Branch, Mr. E. F. Lobacz, Chief (Former Coordinator, ACFEL), as a project of the Experimental Engineering Division, Mr. K. A. Linell, Chief (Former Director, ACFEL), USA CRREL. Mr. G. D. Gilman of the Construction Engineering Branch was responsible for coordination of the final report.

Colonel Philip G. Krueger was Commanding Officer of USA CRREL during the preparation and publication of this report, and Mr. W. K. Boyd was Technical Director.

USA CRREL is an Army Materiel Command laboratory.

\*ACFEL and U. S. Army Snow, Ice and Permafrost Research Establishment (USA SIPRE) were merged into the Cold Regions Research and Engineering Laboratory (USA CRREL), Hanover, New Hampshire, in 1961.

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## EVALUATION OF THE AASHO PROFILOMETER FOR MEASURING AIRFIELD PAVEMENT PROFILES

#### by

## E. J. Yoder and R. D. Walker

### INTRODUCTION

#### Background

Under an earlier contract with the former Arctic Construction and Frost Effects Laboratory of the U. S. Army Engineer Division, New England, the Purdue Research Foundation conducted a literature search and evaluation of methods which have been employed for measuring pavement profiles and roughness. Results of the study are contained in ACFEL Technical Report 73, "Pavement Profile and Roughness Measurements (A Review of Methods)" by E. J. Yoder and D. Hampton, June 1960.

Under the previous contract, existing instruments were reviewed in terms of mobility, durability, accuracy of both profile and roughness measurements, and usability of data produced. No instrument was found to be completely satisfactory in these respects and it was considered that the method of greatest potential was a profilometer that measures slope angles using an inertial system to maintain a suitable vertical or horizontal reference plane. At the time the study was being conducted, such an instrument was under development at the AASHO Road Test, Ottawa, Illinois, and liaison with AASHO regarding this device was recommended.

Subsequent liaison between ACFEL and AASHO Road Test personnel indicated that an evaluation of the capability of the AASHO profilometer to measure airfield pavement profiles was warranted. Accordingly the cooperation of AASHO was obtained and, in April 1959, ACFEL awarded contract DA-19-016-Eng-6554, "Study and Report on Applicability of the AASHO Profilometer for Measuring Airfield Pavement Profiles," to the Purdue Research Foundation, School of Civil Engineering, Purdue University. This report summarizes studies conducted under the contract.

### Purpose and scope

The purpose of this study was to determine the capability of the AASHO profilometer to measure airfield pavement profiles. To accomplish this, a number of test tracks were established on pavements at Chanute AFB, Rantoul, Illinois, and profiles obtained with the AASHO instrument were compared with those obtained using standard precise level procedures.

#### THE AASHO PROFILOMETER

Figure 1 shows the profilometer and towing vehicle, containing electronic recording instrumentation, in operation. Profiling is normally accomplished at a speed of about 5 mph.

The instrument contains an inertial system for continuous horizontal reference and two reference slope or "feeler" wheels, mounted in tandem between each of two pairs of motorcycle wheels (Fig. 1), which measure abrupt changes in profile. The inertial horizontal reference system adopted for the AASHO profilometer is based upon the principle of a floating, spinning disk. The disk is mounted on a center pivot through which air is permitted to escape at high velocity which in turn acts as a lubricant between disk and pivot.

The disk is caused to rotate at high speed and, since it is lifted from the pivot by the air pressure, it in effect acts as a gyroscope.

Referring to the schematic diagram on Figure 2, the inertial system "R" detects the angle "B" between the trailer and an imaginary horizontal reference; and the slope wheels "S" measure the angle "A" between the axle of the slope wheels and the frame. Prior tests by AASHO Road Test personnel of the effectiveness of the horizontal reference system had indicated that the inconvenience of operation with the reference was considerable. It is pertinent to note, therefore, that testing at the Ottawa Road Test was generally accomplished without the horizontal reference system in operation.

The instrument produces a continuous analog of the slope of the pavement (Fig. 3, 4) in two wheel paths which correspond to the tread of an automobile. The analog tapes are fed into an automatic electronic tape reader which measures the ordinate of the chart at intervals equivalent to 1 ft on the pavement.

As previously stated, the profilometer data on the AASHO Road Test were analyzed without using the output of the horizontal reference system. The profile characteristics were reduced to a single statistic by use of the equation:

$$\overline{SV} = \frac{\Sigma Y^2 - \frac{1}{n} (\Sigma Y)^2}{\frac{1}{n} (\Sigma Y)^2}$$

where: Y is the difference between elevations 1 ft apart, and n is the number of readings.

Slope variance  $\overline{SV}$  as given by the equation is the statistical variation of slope at 1 ft intervals referenced to the mean slope of an entire test pavement. The slope variance statistic is indicative of pavement roughness, but does not consider long wave lengths of the pavement.

### EVALUATION TESTS

The testing schedule at the AASHO Road Test limited the availability of the profilometer and operating crew to a period not exceeding 5 days, including travel time. Permission was obtained from the Commander, Chanute Air Force Base, Rantoul, Illinois, to conduct the evaluation tests on pavements at that installation during the period 26-30 October 1959.

### Procedure

Eight test tracks were established on portland cement concrete pavements on the NW end of the NW-SE runway and on adjoining taxiway A. Two of the tracks were 400 ft long, four were 800 ft long, one was 1300 ft long, and one curved track approximately 268 ft in length was established along a painted traffic line. The locations of the test tracks are shown on Figure 5 and will hereinafter be referred to by the track numbers shown on Figure 5. With the exception of the curved track, the courses were established along longitudinal joints to permit the driver to line up along the joint. This resulted in passage of the left pair of slope wheels approximately 3 in. from the joint, and passage of the right pair of slope wheels approximately in the middle of the slabs, which were 12.5 ft wide.

Measurements of elevation accurate to about  $\pm$ . 002 ft were made along both wheel paths of the profilometer using a precise level and stadio rod with target. Level readings were taken at intervals ranging from 1 ft to 100 ft, with the larger portion of the data obtained in the left wheel path of the profilometer.

As previously stated, the AASHO profilometer contains an inertial system for continuous horizontal reference and two slope wheels which measure abrupt changes in profile. Three types of measurement were made with the profilometer. Profiles were run using both measurement systems and with each system operating alone to determine which of the systems had the greatest effect on the results.

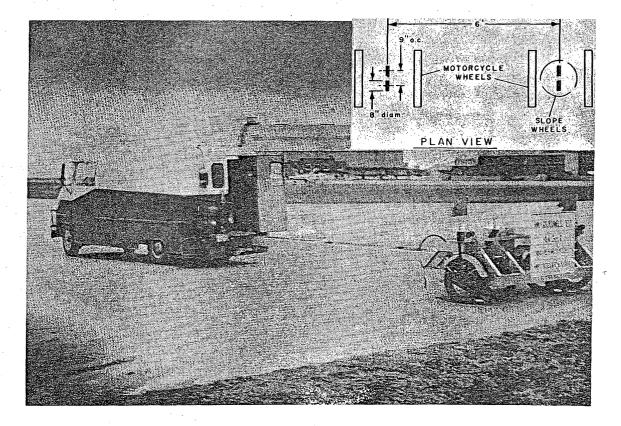


Figure 1. AASHO profilometer in operation.

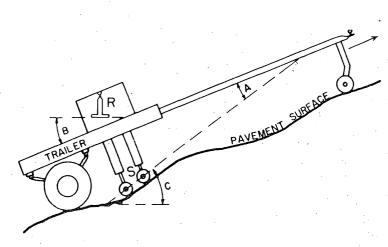


Figure 2. Schematic diagram of profilometer.

The profilometer was towed over each of the eight tracks a minimum of three times and at least one run was made on each track with both systems in operation. Two runs were made on tracks 5 and 6 using the horizontal reference only and several tests were made on each track with only the slope wheels in operation.

		·	C	Cest ]	rac	k		
Measurement system operating	1	2	3	4	5	6	7	8
Horizontal reference and slope wheels	1	1	1	1.	3	. 2	1	2
Slope wheels only	2 .	2	2	3	4	2	2	2
Horizontal reference only	0	0	0	0	2	2	0	0

### Table I. Profilometer test runs.

The analog charts produced by the profilometer were later read electronically in the Road Test laboratories. This information was fed into a digital computer which summarized the slope data in units of feet per foot; elevations were expressed by making a continuous summation of the slope data. Since the method adopted at the Road Test for representing pavement profile is based upon mean slope of the test track, as shown by the equation previously given, it was then necessary to recalculate the data to relate these elevations to the level elevations at specific locations along the test tracks. This operation may have introduced some error; however, the amount is not known.

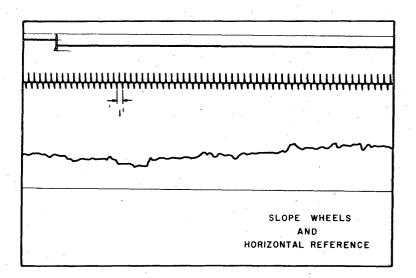
#### Results

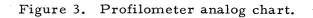
The comparative elevations obtained by profilometer and level for the various test tracks and wheel paths are shown on Figures Al to Al6 (App A) and are summarized on Tables BI to BXVI (App B). The following analysis of the profilometer capabilities is made on a qualitative basis by comparing the general profiles obtained by each method of measurement to the level data.

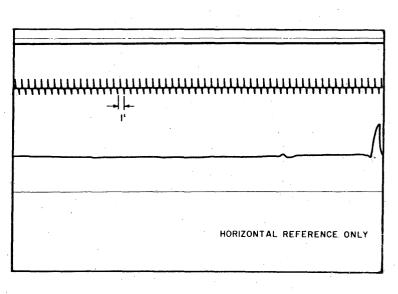
From the test results it is evident that it is necessary to use the horizontal reference system, since data produced by the slope wheels alone did not compare favorably with the level data. This would be expected since these wheels measure slopes relative to the frame of the device itself. Test runs with only the horizontal reference system in operation gave better results, but again the profiles were in general different from those obtained by leveling.

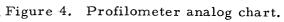
The best results were obtained when the slope wheels and horizontal reference systems were both operating. The results of these runs are summarized in Table II: Profilometer results are considered to be entirely inadequate only for track 8. It is significant to note that track 8 was a horizontal curve which may have introduced error into the data produced by the profilometer.

With both measurement systems in operation, the general shape of profiles produced by the profilometer on tracks 1 through 7 compared favorably with those obtained by precise leveling techniques. The profilometer comparison to the true profile was considered excellent on track 7, where the profiles were almost identical, and good on track 3. However, numerical values of elevation produced by the profilometer on tracks 1, 2, 4, 5 and 6 were not in good agreement with the precise level values. Observation of Figure Al suggests that errors may accumulate in the horizontal reference system. It will be noted that the slope of the profile obtained from profilometer run 5-HR is essentially the same as the level profile, but that an accumulative error apparently occurred in the first 40 ft of test run. These data further suggest that if the profilometer could be re-referenced at intervals to level check points, profiles produced by the two methods would be essentially the same. The same observation can be made for all the other test runs except those on track 8.









Track	Wheel path	Max diff between level and prof <u>data (ft)</u>	General rating of profilometer <u>data</u>	<u>Remarks</u>
1	Left	0.2	Fair	Approximate profile reproduced, accumulative errors present
1	Right	1.1	Fair	Approximate profile reproduced, accumulative errors present
2	Left	0.7	Fair	Approximate profile reproduced, accumulative errors present
2	Right	0.5	Fair	Approximate profile reproduced, accumulative errors present
3	Left	0.2	Good	Approximate profile reproduced, accumulative errors present
3	Right	0.2	Good	Approximate profile reproduced, accumulative errors present
. 4	Left	1.0	Fair	Approximate profile reproduced, accumulative errors present
4	Right	0.8	Fair	Approximate profile reproduced, accumulative errors present
· 5	Left	3.5*	Fair	Runs 1 and 2 good, run 3 poor
5	Right	2.5*	Fair	Runs 1 and 2 good, run 3 poor
6.	Left	1.0	Fair	Approximate profile reproduced
6	Right	1.0	Fair	Approximate profile reproduced
7	Left	0.1	Excellent	Approximate profile reproduced
7	Right	0.3	Good	Approximate profile reproduced
8	Left	1.3	Very poor	Did not reproduce slope of profile
8	Right	1.1	Very poor	Did not reproduce slope of profile

Table II. Summary of profilometer runs with horizontal reference and slope wheels in operation.

\*Run No. 3

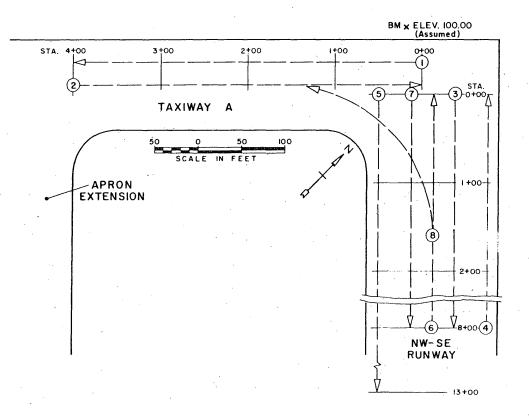
## CONCLUSIONS

It is apparent that the accuracy of the profilometer is to a large extent dependent on the accuracy of the horizontal reference system.

Results of these tests indicate that differences between level and profilometer data are the result of accumulated errors in the horizontal reference system; however, the reason for the errors did not become apparent during the course of this study. There appears to be little doubt that use of a precise gyroscope would eliminate most of the accumulated errors introduced by the present reference system.

#### **RECOMMENDATIONS**

The AASHO profilometer is sound in principle, and it is recommended that this type of instrument be adopted if fabrication of a profilometer for use on airfield pavements is undertaken by the Government. However, further development of the horizontal reference system is necessary, and development of a system incorporating precise gyroscopes is recommended. The data obtained in this study indicate that such an instrument will reproduce profiles, and will have wide application for use on airfield pavements.



Eigure 5. Location of test tracks, Chanute AFB. Tracks established along longitudinal joints. Left wheel path approximately 3 in. from joint. Right wheel path 6 ft to right in direction of travel.

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## LEGEND

HR Horizontal Reference and slope wheels operating

NHR Horizontal Reference N of Operating, slope wheels only

HRO Horizontal Reference Operating, slope wheels not operating Number designates profilometer run.

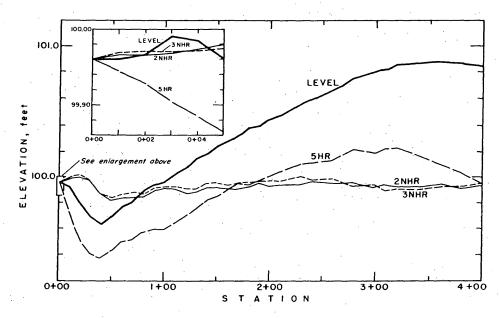
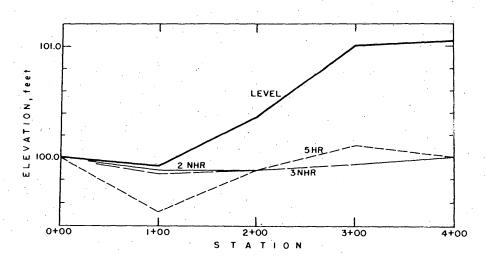
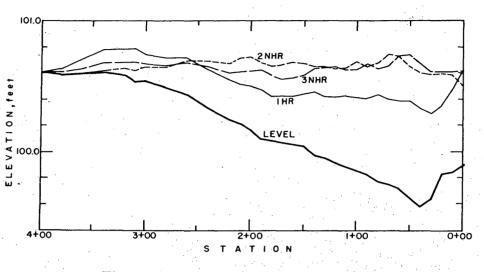
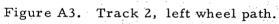


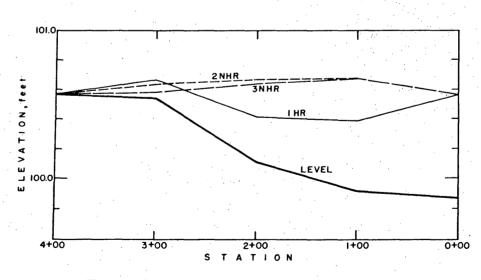
Figure Al. Track 1, left wheel path.

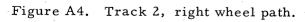






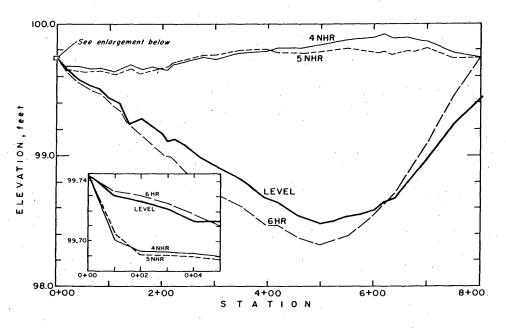


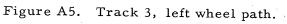


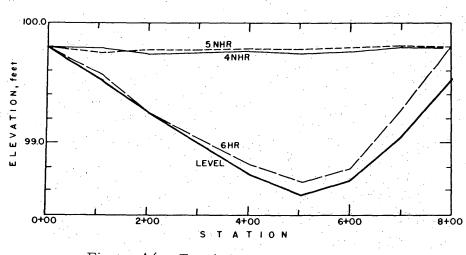


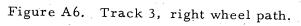
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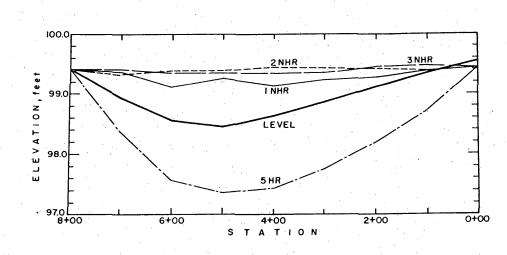


Figure A7. Track 4, left wheel path.

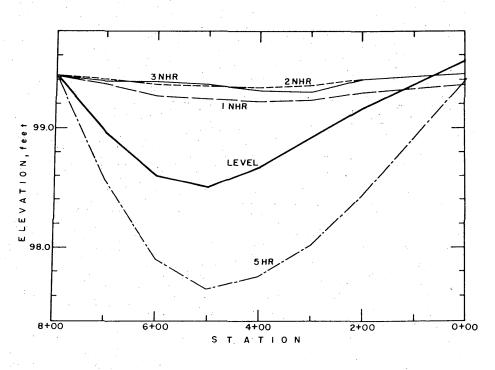
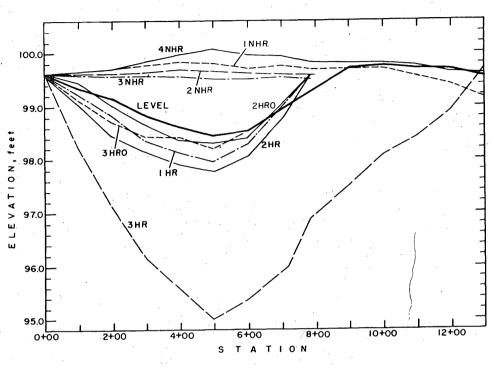
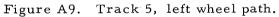
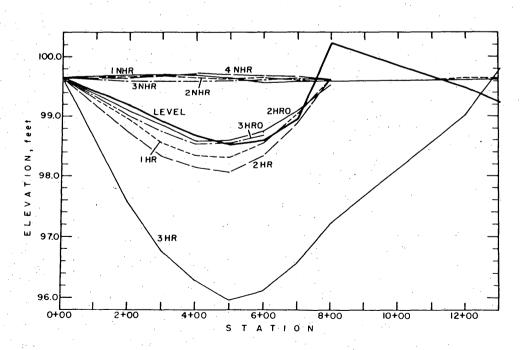
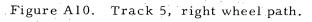


Figure A8. Track 4, right wheel path.









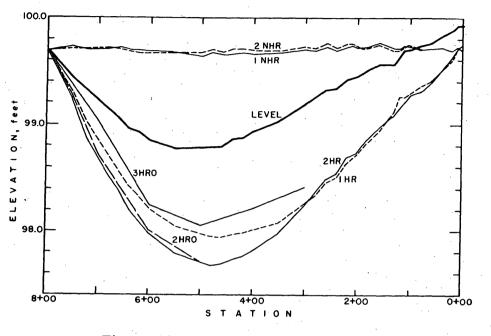
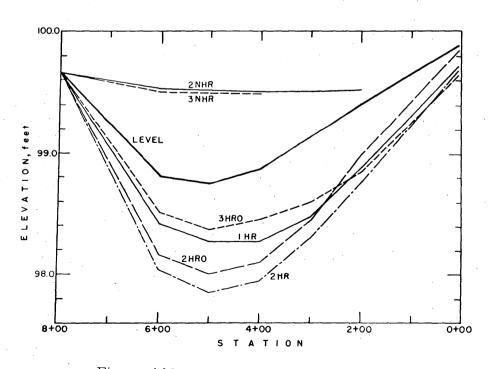
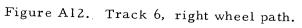


Figure All. Track 6, left wheel path.

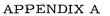


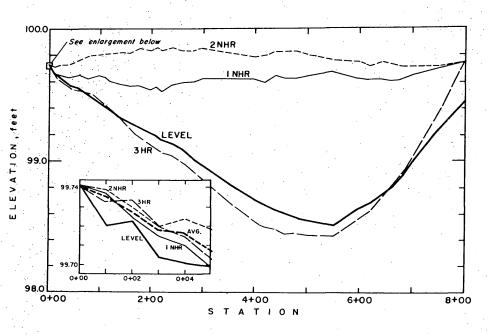


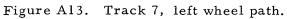
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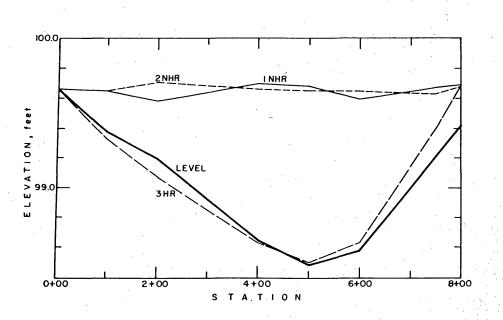
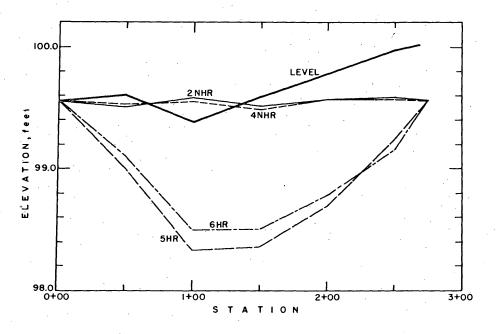
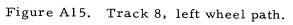
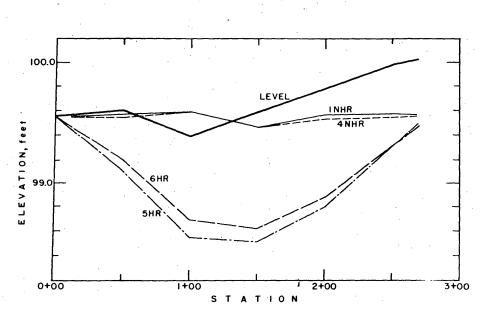
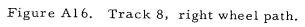


Figure Al4. Track 7, right wheel path.









APPENDIX B. PRECISE LEVEL AND PROFILOMETER ELEVATIONS 17 LEGEND

HR Horizontal Reference and slope wheels operating

NHR Horizontal Reference Not Operating, slope wheels only

HRO Horizontal Reference Operating, slope wheels not operating

Number designates profilometer run.

Table BI. Track 1, left wheel path.

Table BII. Track 1, right wheel path.

Tabl	Table BI. Track 1, left wheel path.								
		Pr	ofilometer						
Station	Level	5-HR	2-NHR	3-NHR					
0/00	99.961	99.961	99.961	99.961					
01 02	99.961 99.966	99.946 99.928	99.966 99.966	99.968 99.970					
.03	99.990	99.904	99.968	99.969					
04	99.984	99.884	99.972	99.971					
05	99.962	99.863	99.978	99.974					
06	99.970	99.843	99.905	99.979					
07	<b>99-9</b> 58	99.822	99.992	99.984					
08	99.944	99.802	100.000	99.990					
09 10	99.939 99.928	99.772 99.743	100.004 100.008	99.996 99.997					
10 15	99.920 99.849	99.61b	100.003	99.995					
20	99.800	99.531	100.017	99.999					
25	99.750	99.473	100.003	99.986					
- 30	99.699	99.411	99.962	99.970					
35	99.649	99-375	99.932	99.921					
40	99.638	99.305	99.071 00.808	99.064					
45	99.658 99.696	99.404 99.439	99.848 99.841	99.839 99.026					
50 60	99.898 99.765	99.500	99.864	99.839					
70	99.817	99.522	99.801	99.849					
80	99.685	99.584	99.076	99.852					
90	99.931	99.604	99.924	99.599					
1 <del>/</del> 00	99.963	99.608	99 <b>.</b> 938	99.922					
01	99.963	99.611	99•937 99•939	99.925 99.929					
02 03	99.965 99.969	99.619 99.622	99.939 99.943	99.925 99.925					
04	99 <b>.</b> 974	<b>99.61</b> 8	99.946	99.923					
05	99.980	99.618	99.950	99.919					
10	100.002	99.650	99. <b>93</b> 0	99.910					
15	99.983	99.675	<b>99.92</b> 1	99.894					
20	100.075	99.705	99.917 99.919	99.878 99.895					
30 40	100.136 100.175 100.232	99.768 99.823	99.919	99 <b>.</b> 914					
50	100.232	99.856	99.960	99.913					
60	100.277	99.910	99.949	99.913					
70	100.324	99.960	<b>99.9</b> 68	<b>99.9</b> 12					
80 20	100.362 100.400	99.960	99.952 99.971	99 <b>.</b> 930 99 <b>.</b> 960					
90 2 <b>/</b> 00	100.446	99.973 100.013	99.968	99.945					
01	100.457	100.018	99.962	99.945					
02	100.457 100.456	100.022	99.981	99.946					
03	100.462	100.031	99.976	99.945					
04	100.465	100.036	99.975	99.944					
05	100.464 100.486	100.044	99•977 99•981	99.943 99.954					
10 20	100.527	100.007	99.997	99.958					
30	100.572	100.116	100.006	99.954					
· 40	100.603	100.127	99.994	99.979					
60	100.679	100.143	99.995	99.968					
60 - /20	100.764	100.216	99.942	99.962 99.935					
3 <b>/</b> 00 01	100.817 100.819	100.196 100.199	99.942 99.941	99.935					
01	100.825	100.203	99.940	99.935					
03	100.827	100.204	99.941	99.935					
04	100.825	100.209	99.942	99.939					
05	100.824	100.216	99.921	99.936					
10	100.835	100.223	99.909	99•945 99•939					
20 . 40	100.868 100.872	100.220 100.175	99.911 99.919	99.939 99.934					
60	100.872	100.101	99.932	99.948					
<u> ხ</u> ე .	100.871	100.035	99.939	99.920					
4/00	100.849	99.959	99.955	99.946					

	·	Profilometer				
Station	Level	5-HR	2-NHR	3-NHR		
0,400	100.006	100.006	100.006	100.006		
10	99.929	99.839	100.051	100.033		
20	99.806	99.628	100.066	100.041		
30	99.691	99.449	100.015	99.985		
40	99.631	. 99.333	99.919	99.880		
50	99.696	99.366	99.916	99.672		
60	99.751	99.415	99.910	99.856		
70	• 99.801	99.431	99.686	99.837		
80	99.866	99.485	99.916	99.871		
90	99.897	99.511	99.920	99.879		
1/00	99.931	99.524	99.903	<b>99.</b> 868		
10	99.797	99.571	.99.697	99.869		
20	100.038	99.620	99.907	99.871		
.30	100.094	99.669	99.918	99.885		
40	100.124	99.704	99.907	99.881		
50	100.159	99.732	99.899	99.871		
60	100.218	99.791	99.901	99.882		
70	100.258	99.832	99.903	99.894		
80	100.312	99.846	99.915	99.904		
90	100.331	99.881	99.900	99.894		
2/00	100.368	99.893	99.899	99.900		
20	100.696	99.950	99.904	99.904		
40	100.781	99.952	99.926	99.922		
60	100.850	100.061	99.919	99.932		
80	100.929	100.093	.99.939	99.943		
3,400	101.003	100.116	99.957	99.948		
20	101.047	100.144	99.973	99.965		
40	101.057	100.122	99.972	99.959		
60	101.061	100.095	99.986	99.975		
80	101.054	100.057	99.967	99.958		
4,600	101.044	100.008	100.001	100.002		

APPENDIX B

#### Table BIII. Track 2, left wheel path.

#### Table BIV. Track 2, right wheel path.

·		Prot	ilometer	
Station	Level	1-HR	2 - NHR	3-NHR
4,400	100.608	100.608	100.608	100.608
3,480	100.584	100.632	100.600	100.590
- (0	100.593	100.701	100.595	100.603
40	100.608	100.781	100.618	100.642
20	100.585	100.784	100.635	100.637
10	100.531	100.787	100.614	100.655
05	100.537	100.771	100.623	100.618
3,400	100.537	100.742	100.645	100.624
2/90	100.489	100.716	100.642	100.608
60	100.435	100.715	100.693	100.638
40	100.329	100.627	100.690	100.635
20	100.246	100.549	100.677	100.585
10	100.212	100.516	100.713	100.601
05	100.205	100.510	100.712	100.604
04	100.204	100.508	100.715	100.611
03	100.194	100.513	100.715	100.613
02	100.182	100.513	100.715	100.616
01	100.180	100.509	100.731	100.620
2,400	100.171	100.503	100.724	100.615
1/95	100.145	100.493	100.693	100.627
90	100.103	100.473	100.681	100.624
85	100.098	100.457	100.684	100.593
80	100.087	100.422	100.653	100.582
70	100.071	100.428	100.664	100-553
1,60	100.058	100.425	100.683	100.565
50	100.038	100.442	100.675	100.587
40	99.977	100.459	1,00.652	100.636
30	<b>99</b> •953	100.423	100.653	100.638
20	99.919	100.416	100.637	100.647
10	99.884	100.429	100.641	100.625
1/00	99.853	100.416	100.687	100.623
99	99.858	100.416	100.667	100.623
98	.99.853	100.416	100.664	100.629
97	99.852	100.416	100.660	100.636
96	99.852	100.416	100.660	100.642
95	99.855	100.413	100.651	100.671
90 85	99.823	100.407	100.647	100.650
80	99.792 00.775	100.429	100.679	100.636
70	99.775 99.752	100.500	100.748	100.658
60	99.712 99.718	100.390	100.727	100.732
50	99.648	100.387	100.650	100.739
40	99.582	100.330	100.603	100.669
30	99.638	100.289	100.588	100.608
20	99.826	100.349	100.593	100.591
10	99.839	100.477	100.587	100.605
0,400	99.889	100.608	100.506	100.607

		F	rofilomete	r
Station	Level	1-HR	2-NHR	3-MHR
· · ·				
4,600	100.560	100.560	100.560	100.560
3,480	100.566	100.626	100.585	100.585
60	100.567	100.656	100.579	100.570
40	100.563	100.685	100.593	100.572
20	100.540	100.707	100.640	100.599
3,400	100.541	100.663	100.635	100.582
2 <b>/</b> 90	100.489	100.627	100.612	100.558
80	100.437	100.644	100.627	100.567
60	100.438	100.624	100.683	100.623
40	100.256	100.492	100.643	100.573
20	100.168	100.430	100.624	100.604
2,400	100.111	100.411	100.672	100.635
1/90	100.037	100.367	100.634	100.608
80	100.045	100.381	100.639	100.603
70	100.018	100.383	100.614	100.604
60	100.017	100.395	100.658	100.662
50 ·	99.988	100.401	100.682	100.667
40	99.917	100.351	100.636	100.631
30	99.900	100.368	100.654	100.652
20	99.901	100.390	100.657	100.648
10	99.863	100.382	100.657	100.642
-1/00	99.918	100.389	100.678	100.673
90	99.813	100.371	100.670	100.655
80	99.785	100.354	100.661	100.665
70	99.752	100.338	100.686	100.692
60	99.696	100.297	100.708	100.706
50	99.648	100.260	100.704	100.675
40.	99.574	100.206	100.600	100.581
30	99.604	100.249	100.539	100.538
20	99.697	100.362	100.535	100.521
10	99.802	100.471	100.546	100.534
0,400	99.870	100.559	100.561	100.562

Table	BV.	Track	3.	left wheel	path.	
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		· · · · · · · · · · · · · · · · · · ·		
			rofilomet	
Station	Level	6-HR	4-NHR	5-NHR
0,400	99.744	99.744	99.744	99.744
01	99.730	99•733	99.701	99.704
02	99.726	99.730	99.693	99.691
03	99.721	99.725	99.693	99.691
. 04	99.713	99.718	99.692	99.690
05	99.713	99.710	99.690	99.688
10	99.693	99.686	99.684	99.677
20	99.642	99.633	99.672	99.654
40	99.588	99.564	99.673	99.646
60	99.544	99.516	99.657	99.642
80	99.503	99.473	99.659	99.648
1/00	99.434	99.405	99.646	99.632
05	99.418	99,387	99.641	99.624
10	99.410	99.374	99.638	99.619
20	99-393	99.334	99.656	99.638
40	99.232	99.232	99.681	99.661
60	99.283	99.162	99.659	99.617
80	99.221	99.095	99.679	.99.645
2/00	99.161	99.016	99.652	.99.662
05.	99.141	99.003	99.655	99.668
10	99.114	99.992	99.658	99.673
20	99.123	98.969	99.693	99.707
40	99.079	98.897	99.711	99.731
75	98.982	98.792	99.753	<b>99.7</b> 61
3,400	98.925	98.718	99.737	99.766 00.766
01	98.922	98.720	99•738	99.766 99.770
02	98.924	98.718	99•742 99•744	99•110 99•774
03 04	98.923	98.719 98.721	99.748	99.777
	98.925 98.923	90.721 98.725	99.753	99.784
05 50	90.925 98.819	98.611	99.785	99.802
4,400	98.674	98.472	99.792	99.806
4 <b>7</b> 00 20	90.074 90.041	98.462	99.812	99.788
60	98.542	98.374	99.825	99.785
5,400	98.488	98.323	99.847	99.798
01	98.489	98.323	99.846	99.798
02	98.486	98.322	99.848	99.799
03	98.485	98.326	99.846	99.798
04	98.489	98.325	99.851	99.801
05	98.487	98.325	99.851	99.780
50	98.543	98.396	99.880	99.811
6,400	98.589	98.546	99.903	99.798
20	98.646	98.637	99.912	99.791
40	98.692	98.721	99.890	99.777
60	98.776	98.844	99.896	99.793
80	98.869	98,966	99.874	99.790
7,400	98.963	99.082	99.867	99.813
01	98.963	99.085	99.864	<b>99.</b> 812
02	98.965	99.091	99.864	99.812
03	98.967	99.095	99.864	99.811
04	98.972	99,100	99.861	99.808
05	98.974	99.102	99.859	99.806
50	99.228	99.447	99.787	99.737
8,400	99.420	99•739	99•741	99.737
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## Table BVI. Track 3, right wheel path.

·		Profilometer				
Station	Level	6-HR	4-NHR	5-NHR		
0,400 1,410 2,400 4,400 5,405 6,400 7,400 8,400	99.804 99.517 99.254 98.735 98.563 98.678 99.040 99.502	99.804 99.565 99.258 98.821 98.674 98.780 99.266 99.805	99.804 99.798 99.751 99.770 99.758 99.772 99.802 99.802	99.804 99.767 99.779 99.798 99.789 99.802 99.802 99.807 99.804		

Table BVII. Track 4, left wheel path.

		Р	rofilomete	r	
Station	Level	5-HR	1-NHR	2 - NHR	3-NHR
0.400	00,100	99.508	99.408	99.408	99.408
8,400	99.408				99.396
7,600	98.953	98.376	99.362	99.341	
6,400	98.564	97.560	99.101	99.361	99.355
5,400	98.450	97.354	99.262	99 <b>.</b> 389	99.362
4,400	98.620	97.429	99.136	99.440	99.342
3,400	98.872	97.763	99.227	99.425	99.356
2,400	99.104	98.196	99.272	99.423	99.458
1,400	99.337	98.713	99.151	99.372	99.4 <b>69</b>
0,405	99.492	99.339	99.416	99.394	99.409
04	99.501	99.350	99.412	99.395	99.410
03	99.504	99.359	99.407	99.392	99.413
02	99.510	99.373	99.407	99.394	99.417
01	99.512	99.388	1.1	99.399	99.410
0,400	99.516	99.406		99.404	99.412

Table BVIII.Track 4, right wheel path.

	1. A. A.	Profilometer					
Station	Level	5-HR	1-NHR	2-NHR	3-NHR		
8/00 7/00 6/00 5/00 4/00 3/00 2/00 0/00	99.449 98.965 98.606 98.506 98.674 98.919 99.167 99.567	99.449 98.568 97.902 97.653 97.763 98.057 98.437 99.387	99.449 99.383 99.273 99.251 99.234 99.242 99.306 99.375	99.449 99.415 99.377 99.367 99.344 99.361 99.419 99.454	99.449 99.408 99.389 99.370 99.334 99.315 99.409 99.461		

APPENDIX B

#### Table BIX. Track 5, left wheel path.

		Profilometer								
Station	Level	l-HR	2-HR	3-HR	1-NHR	2-NER	3-NHR	4-NHR	2-HRO	3-HRO
0,400	99.624	99.624	99.624	99.624	99.624	99.624	99.624	99.624	99.624	99.624
1,400	99.387	99.282	99.056	99.227	99.681	99.635	99.608	99.651	99.270	99.152
2700	99.141	98.858	98.575	97.085	99.755	99.657	99.627	99.772	99.000	98.878
3,400	98.853	98.389	98.141	96.131	99.802	99.678	99.652	99.868	98.676	98.625
4/00	98.614	98.118	97.911	95.578	99.889	99.732	99.628	99.989	98.469	98.492
5,400	98.453	97.991	97.780	95.196	99,858	99.713	99.579	100.040	98.435	98.416
6,400	96.528	98.303	98.069	95.406	99.760	99.691	99.585	99.999	98.578	98.600
7/00.	98.910	98.928	98.782	95.991	99.791	99.677	99.638	99.968	99.014	99.024
8,400	99.406	99.629	99.625	96.868	99.733	99.639	99.567	99.866	99.631	99.630
9,400	99.736			97.541	99.739			99.845		
10,400	99.780		· · ·	98.012	99.790			99.835		
12/00	99.431			98.936	99.701	2.5.5		99.694		
13/00	99.244			99.759	99.623		1	99.634		

Table BX.. Track 5, right wheel path.

		Profilometer								
Station	Level	1-HR	2-HR	3-HR	1-NHR	2-NHR	3-NHR.	4-NHR	2-HRO	3-HRO
0/00 2/00 3/00 4/00 5/00 6/00 7/00 8/00 12/00 13/00	99.650 99.184 98.911 98.671 98.506 98.580 98.951 100.254 99.244	99.650 98.953 98.547 98.343 98.311 98.544 99.043 99.654	99.650 98.738 98.330 98.139 98.061 98.341 98.896 99.655	99.650 97.529 96.747 96.277 95.958 96.108 96.555 97.204 99.029 99.759	99.650 99.691 99.701 99.694 99.649 99.649 99.612 99.612 99.608 99.634 99.633	99.650 99.672 99.692 99.688 99.635 99.653 99.653 99.625 99.591 <b>9</b> 9.641 <b>99.64</b> 1 <b>99.64</b> 1	99.650 99.624 99.614 99.611 99.625 99.640 99.645 99.645 99.647	99.650 99.680 99.700 99.718 99.705 99.688 99.682 99.634	99.650 99.114 98.829 98.678 98.618 98.715 99.131 99.642	99.650 99.015 98.767 98.653 98.579 98.738 99.136 99.653

## APPENDIX B

#### Table BXI. Track 6, left wheel path.

	· · ·	·		· · · · · · · · · · · · · · · · · · ·				
		L	· · · · ·		rofilomet		· · · · · · · · · · · ·	T
Station	Level	1-HIR	2 - HR	1-NHR	2-NHR	2-HRO	3-HRO	Average*
8,400	99.696	99.696	99.696	99.696	99.696	99.696	99.696	<u> </u>
7/50	99.432	99.295	99.240	99.730	99.712			99.494
25	99.335	99.064	98.988	99.717	99.695		1. S. 1. 1. 1. 1.	99.367
24	99.330	99.050	99.968	99.700	99 704			.99.360
23	99.326	99.034	98.937	. 99.704	99.702	1		99.344
22	99.325	99.023	95.909	99.702	99.702			99.334 99.321
21	99.313	99.011	98.873	99.702	99.699		99.009	99.317
20	99.309	99.003	98.859	99.696	99.693	96.037	99.009	99.167
6,480	99.146	98.711	96.525	99.719	99.715			99.099
60	99.058	96.566	99.390	99.715	99.724			99.009
40	98.958	98.424	98.214	99.694 99.672	99,703 99,707			90.949
20	90.921	98,330 98,215	98.006 97.977	99.676	99.686	97.922	: 96.310	95.600
6/00	90.050	98.064	97.510	99.660	99.662	71.722		98.799
5/55	96.774	98.059	97.806	99.659	99.660			98.796
54 53	90.771 98.777	90.009	97.000	99.657	99.660			98.795
52	.98.773	98.059	97.792	99.650	99.662		114 A.A.A.A.A.A.A.A.A.A.A.A.A.A.A.A.A.A.A.	90.795
51.	90.776	90.060	97.790	99.660	99.664	1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 -		90.796
50	90.773	90.054	97.801	99.662	99.667		e ti	95.796
5,600	90.706	97.901	97.716	99.645	99.667	97.719	98.139	90.752
4,480	98.804	97.951	97.660	<b>99.6</b> 03	99.707			98.755
60	90.005	97.945	91.691	99.659	99.682			90.744
40	90.865	97.960	97.730	39.662	99.714			96.76
20	98.882	97.985	97.761	99.677	99.716			98.765
4,400	90.939	98.013	97.612	99.663	99.690	97.051	98.225	90.799
3/50	99.039	98.005	97.977	99.677	99.694			90.055
05	99.201	95.268	98.233	99.713	99.740			99.909
04	99.194	96.267	90.250	99.717	99.744			98.994
03	99.190	96.265	90.245	99.717	99.740			98.993
02	99.190	93.266	90.243	99.711	99-739			96.990
01	99.196	98.266	90.245	99.710	99.737			98.990 99.01
3/00	<b>99.19</b> 6	96.267	96.246	99.708	99.736	98.266	96.403	99.01
2/80	99.255	98-345	98.357	99.696	99.725			99.11
60	99.329	98.463	98.409	99•735	99.767			99.11
40	99.341	98.503	98.540	99.694	99.721 99.762			99.20
20	99.433	98.644	98.690	99.733	99.764			99.228
10	99.443	96.681	90.719 98.747	99•747 99•729	99.784	98.720	96.676	99.23
2/00	99.457	98.725 98.843	96.870	99.734	99.724	<i>J</i> 01120		99.29
1/80 60	99.521 99.567	98.043 98.935	98.971	99.772	99.758		h	99.359
30	99.566	90.935 99.130	99.093	99.722	99.695			99.410
.20	99.500 99.644	99.264	99.159	99.715	99.694			99.458
. 10	99.703	99.252	99.228	99.741	99.733			99.468
1,400	99.707	99.289	99.274	99.737	99.743	99.271	99.070	99.51
0,480	99.743	99.358	99.313	99.706	99.720			99.525
60	99.769	99.401	99.309	99.715	99.720	1		99.556
40	99.827	99.505	99.496	99.714	99.724			99.610
20	99.682	99.628	99.610	99.690	99.698		} · · ·	99,651
10	99.929	99.712	99.709	99.726	99.724			99.720
05	99.925	99.733	99.736	99.720	99.716	1 <del>.</del>		99.826
04	99.935	99.737	99.738	99.717	99.712			99.72
03	99.932	99.741	99.745	99.716	99.709		t ter	99.728
02	99.928	99.745	99.748	99.711	99.706		1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	99.720
01	99.924	99.746	99.753	99.707	99.700			99.729
0/00	99.932	99.756	99.756	99.702	99.692	99.910	99.701	99.72

\*Excluding runs 2-HRO and 3-HRO

## Table BXII. Track 6, right wheel path.

		Profilometer						
Station	Level	1-HR	2 <b>- HR</b>	2-NHR	3-NHR	2-HRO	3-HRO	
8/00 6/00 5/00 4/00 3/01 2/00 0/05	99.668 98.829 98.754 98.802 99.150 99.420 99.906	99.668 98.438 95.278 98.276 98.476 98.864 99.744	99.668 98.065 97.855 97.955 98.305 98.765 99.724	99.668 99.672 99.671 99.648 99.650 99.690 99.668	99.668 99.664 99.652 99.636 99.656 99.677 99.653	99.668 98.181 95.019 98.116 95.452 98.896 99.576	99.668 99.526 98.378 95.459 95.604 95.859 99.660	

Table BXIII. Track 7, left wheel path.

## Table BXV. Track 8, left wheel path.

		<u> </u>	Profilomet	er
Station	Level	3-HR	1-NHR	2-NHR
0,000	99.741	99.741	99.741	99.741
01	99.720	99.733	99.737	99.739
02	99.722	99.734	99.725	99.730
03	99.704	99.720	99.715	99.720
04	99.701	99.715	99.710	.99.724
05	99.699	99.703	99.699	99.719
10	99.666	99.660	99.666	99.716
20	99.634	99.617	99.650	99.722
40	99.571	99.562	99.634	99.736
60	99.544	99 <b>•539</b>	99.644	99 <b>.762</b>
80	99.494	99.508	99.625	99.790
1/00	99.445	99.453	99.642	99.803
10	99.412	99.416	99.633	99.603
20	99.385	99 <b>.</b> 368	99.607	99.803
40 60	99.331	99.324	99.588 99.562	99.813 99.624
60 80	99.295	99.246	99.565	99.855
2,400	99.246 99.209	99.176 99.111	99.505 99.547	99.846
10	99.209 99.192	99.097	99.562	99.861
20	99.192 99.163	99.064	99.529	99.844
40	<b>99.1</b> 37	99.043	99.574	99,860
60	99.095	98.997	99.592	99.342
80	99.022	98.939	99.602	99.848
3,400	98.973	98.869	99.626	99.853
01	98.964	98.861	99.627	99.849
02	98.959	95.856	99.625	99.845
03	98.957	98.848	99.615	99.840
04	98.955	98.848	99.617	99.841
05	98.957	96.849	99.619	99.828
50	98.831	98.701	99.622	99.829
- 4,600	98.713	98.550	99.624	99.799
20	98.673	98.508	99.609	99.801
40	98.631	96.484	99.650	99.820
60	98.600	96.455	99.635	99.630
80	98.573	98.452	99.636 99.646	99.031 99.811
5/00	98.554	98.441 98.443	99.640 99.646	99.807 99.807
01 02	98.553	98.440	99.642	99.816
02	98.555 98.549	96.440	99.647	99.815
03	90.549 98.552	96.440 96.440	99.648	99.810
04	98.555	98.438	99.646	99.806
50	98.513	96.430	99.678	99.773
6,600	98.644	98.560	99.625	99.757
20	98.680	98.626	99.610	99.729
40	98.743	98.713	99.612	99.749
60	98.793	98 <b>.790</b>	99.601	99.729
80	98.885	98.885	99.612	99.714
7/00	98.995	99.017	99.647	99.718
01	98,999	<b>99.0</b> 18	99.647	99.725
02 ·	99.010	99.032	99.644	99.725
03	99.022	95.041	99.647	99.728
04	99.027	99.053	99.650	99.730
05	99.033	99.065	99.656	99.731
50	99.230	99.352	99.698 99.743	99.711 99.741
8 <b>/0</b> 0	99.440	99.744	77.1.3	33.141

			Profilometer				
	Station	Level	5-HR	6-HR	2-NHR	4-NHR	
	0,400	99.559	99.559	99.559	99.559	99.559	
	10	99.567	99.428	99.465	. 99.532	99.551	
	20	99.605	. 99.330	99.360	99-534	99.559	
	30	99.593	99.219	99.284	99.522	99.543	
	50	99.608	90.998	99.103	99.510	99.522	
	70	99.535	98.724	98.664	99.554	99.536	
	90	99.431	98.439	98.600	99.540	99.516	
	1/00	99.386	98.327	98.495	99.584	99.556	
1	10	99.341	98.197	98.374	99.540	99.510	
	30	99.479	98.217	98.377	99.494	99.462	
	50	99.598	98.357	98.499	99.516	99.492	
	70	99.706	98.485	98.614	99.527	99.520	
	90	99.743	98.620	98.716	99.570	99.553	
	2/00	99.785	96.687	98.780	99.568	99.567	
	10	99.827	90.775	98.865	<b>99.</b> 594	99.576	
	30	99.903	96.961	98.958	99.550	99.539	
	50	99.981	99.241	99.153	99.584	99.579	
	67.5	100.023	99.456	99.360	99.563	99.560	
	70		99.484	99.490	99.563	99.561	
	75	•	99.560	99.560	99.559		

## Table BXVI. Track $\delta$ , right wheel path.

			Profil	ometer	
Station	Level	5-HR	6-HR	1-NHR	4-NHR
				00.550	00 550
0,600	99.559	99.559	99-559	99.559	99.559
10	99.567	99.450	99.470	99.540	99.536
20	99.605	99.357	99.407	99.561	99.551
30	99.593	99.268	99.315	99.540	99.521
50	99.608	99.100	99.196	99.573	99.554
70	99.535	98.908	99.043	99.639	99.633
90	99.431	96.636	96.772	99.584	99.579
1/10	99.341	90.403	95.618	99.605	99-595
30	99.479	98.404	98.527	99.457	99.440
50	99.598	98.510	98.619	99.470	99.468
70	99.706	98.643	98.732	99.533	99.513
90	99.743	98.740	98.825	99.575	99.542
2/10	99.827	98.862	98.928	99.565	99.535
30	99.903	99.053	99.078	99.524	99.510
50	99.981	99.313	99.308	99.573	99:547
67.5	100.023	99.489	99.476	99.565	99.556

## Table BXIV. Track 7, right wheel path.

		Profilometer					
Station	Level	3-HR	1-NHR	2-NHR			
0,100 1,400 2,400 4,400 5,400 6,400 7,450 6,400	99.661 99.379 99.192 98.644 98.484 98.576 99.205 99.414	99.661 99.330 99.076 98.632 98.496 98.630 99.397 99.673	99.661 99.653 99.565 99.700 99.601 99.594 99.669 99.669	99.661 99.652 99.705 99.663 99.653 99.646 99.627 99.671			